

Location Map

Project: Marsh Run II Redevelopment

Address:11816 Wayzata Blvd







April 11, 2023

Bria Raines CC: Loren Gordon City of Minnetonka 14600 Minnetonka Boulevard Minnetonka, MN 55345

Re: Marsh Run II Redevelopment

Dear Ms. Raines,

Doran RE Partners, LLC submitted a full entitlement plan set on February 24, 2023 including a Master Development, Site Building Plan Review, and Rezoning application(s). The applications are related to the proposed 197-unit apartment project located at 11816 Wayzata Blvd.

City staff received a Traffic Study from SRF on March 24, 2023, which resulted in recommendations to make an adjustment to the site plan that was previously submitted. The recommendation was to shift the proposed western drive entrance 100' east of the existing site entrance. This was due to the need for safe left-turning maneuvers, and meet the recommended AASHTO gap time of 7.5 seconds from when vehicles become visible on the main sight line to when they cross the proposed access location. The previous proposed access drive would have a gap time of 6.75 seconds. With the new proposed western site entrance, the project should meet or exceed the recommended gap time of at least 7.5 seconds and instead be closer to 8-8.5 seconds.

Moving the western site entrance approximately 150 feet from the previously proposed entrance had cascading impacts to the previously submitted site plan. This is due to grades on project site – grades fall from east to west along Wayzata Blvd, but entering the site fall from west to east. Site and building plan configurations were adjusted to accommodate the appropriate and/or desired maximum slopes of the site drive and surface parking. A full list of the site plan and south elevation changes from the original submission in February include:

- Overall finish site grade adjusted near building entry/new site entry to allow for proper slopes into the site and cross slope through the surface parking/circulation area.
- The new lower grade required a rework of the front entry. Shifting the entry door out to accommodate stairs and accessible pathway to catch the grade.
- The Parking entrance into L1 shifted to east wing due to new site entry location for easier circulation and building access.



- Given the L1 garage door is no longer on the western portion of the building, the black masonry was swapped to be consistent with the brown masonry surrounding this portion of the building. Additional windows were also added to activate this portion of the building frontage in lieu of the garage door.
- Additional parking stalls added where previous L1 parking entrance was. This brings the parking count
 up from 304 to 306 parking stalls. Full parking counts are detailed on the new cover sheet.
- Accessible stalls on surface parking shifted east to have easiest access to the accessible pathway at the main building entry.
- Move in pad extended north approximately 24' for easier internal move in and closer proximity of electrical room to exterior transformer.

Please reach out if there are any questions when reviewing the new site plans or south building elevation.

Thank you,

Jacquel Hajder

Exhibit A – Legal Description

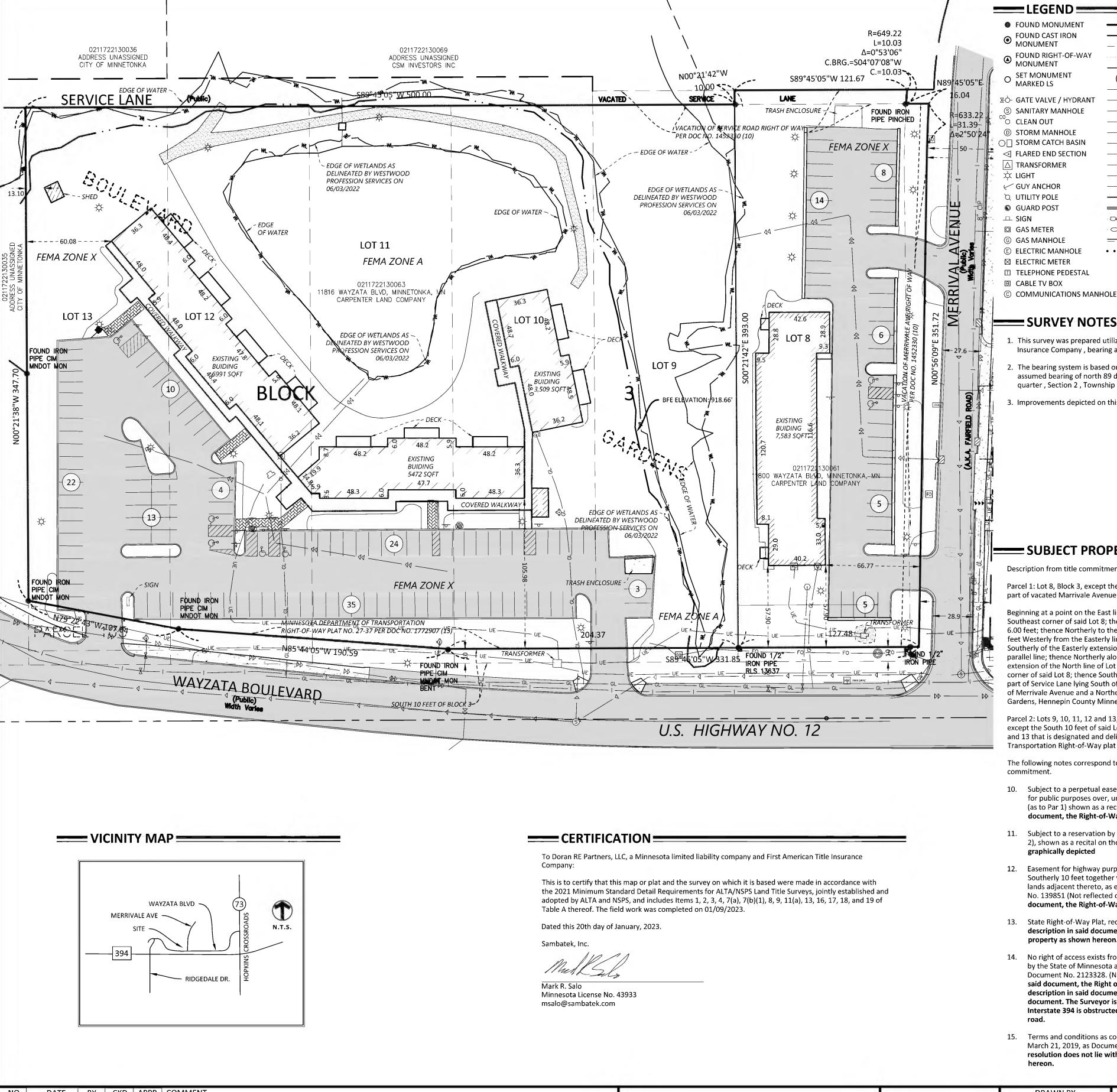
Par 1: Lot 8, Block 3, except the South 10 feet taken for widening Superior Boulevard; and That part of vacated Marrivale Ave. described as follows: beginning at a point on the East line of Lot 8, Block 3, in said plat distant 10.00 feet North of the Southeast corner of said Lot 8; thence; East, parallel with the South line of said Lot 8, a distance of 6.00 feet; thence Northerly to the point of intersection with a line which runs parallel with and 50.00 feet Westerly from the Easterly line of said Avenue, said point of intersection being 31.52 feet Southerly of the Easterly extension of the North line of said Lot 8, as measured along the last said parallel line; thence Northerly along said parallel line, a distance of 31.52 feet ot said Easterly extension of the North line of Lot 8; thence West along said Easterly extension, to the Northeast corner of said Lot 8; thence Southerly, along said East line of Lot 8, to said point of beginning; That part of Service Lane lying South of the center line thereof and between the Westerly right-of-way line of Merrivale Ave. and a Northerly extension of the Westerly line of Lot 8, Block 3, "Boulevard Gardens, Hennepin Co. Minn."

Par 2: Lots 9, 10, 11, 12 and 13, Block 3, "Boulevard Gardens, Hennepin Co. Minn.", except the South 10 feet of said Lots 9, 10, 11, 12 and 13 and except that part of said Lots 11, 12 and 13 that is designated and delineated as Parcel 10C on the Minnesota Department of Transportation Right-of-Way plat No 27-37.

Subject to a perpetual easement in favor of the City of Minnetonka, its successors and/or assigns for public purposes over, under and across Merrivale Avenue as shown in Document No 1452330; (as to Par 1)

Subject to a reservation by the State of Minnesota of minerals and mineral rights; (as to Lot 9 in Par 2)

PID 02-117-22-13-0063



TREE LINE

CONCRETE CURB

---- BUILDING CANOPY

BITUMINOUS SURFACE

CONCRETE SURFACE

DECIDUOUS TREE

CONIFEROUS TREE

SPOT ELEVATION

CONTOUR

SOIL BORING

STALL COUNT

REGULAR PARKING

TRAFFIC MARKERS

//// BUILDING LINE

- ---- EASEMENT LINE BOUNDARY LINE - - SETBACK LINE - RIGHT-OF-WAY LINE — Δ — RESTRICTED ACCESS
- FOUND CAST IRON MONUMENT UNDERLYING / ADJACENT LOT FOUND RIGHT-OF-WAY TIE LINE MONUMENT — – – SECTION LINE **SET MONUMENT** (100.00)DEED DISTANCE
- MARKED LS —— I —— WATERMAIN **⊠**O- GATE VALVE / HYDRANT SANITARY SEWER SANITARY MANHOLE — → STORM SEWER CLEAN OUT —— UE —— UNDERGROUND ELECTRIC
- ∪T UNDERGROUND TELEPHONE ⑤ STORM MANHOLE ☐ STORM CATCH BASIN ---- UG ---- UNDERGROUND GAS — OE — OVERHEAD ELECTRICAL WIRE TRANSFORMER ——o—— CHAIN LINK FENCE
- 💢 LIGHT WOOD FENCE ——×—— WIRE FENCE GUY ANCHOR — WL — WET LAND RETAINING WALL
- Q UTILITY POLE GUARD POST
- DOCODO BLOCK RETAINING WALL STONE RETAINING WALL **© GAS MANHOLE** = POND / WATER LINE © ELECTRIC MANHOLE • • • • • • FEMA FLOOD ZONE LINE
- □ TELEPHONE PEDESTAL B CABLE TV BOX
- SURVEY NOTES =
- 1. This survey was prepared utilizing Title Commitment No. NCS-1148042-MPLS by First American Title Insurance Company, bearing an effective date of 09/02/2022.
- 2. The bearing system is based on the Hennipin County coordinate system, NAD83 (1986 Adjust), with an assumed bearing of north 89 degrees 45 minutes five seconds east for the South line of the Northeast quarter, Section 2, Township 117, Range 22.
- 3. Improvements depicted on this survey are a combination of data collected by Sambatek and by others.

SUBJECT PROPERTY =

Description from title commitment:

Parcel 1: Lot 8, Block 3, except the South 10 feet taken for widening Superior Boulevard; and That part of vacated Marrivale Avenue described as follows:

Beginning at a point on the East line of Lot 8, Block 3, in said plat distant 10.00 feet North of the Southeast corner of said Lot 8; thence; East, parallel with the South line of said Lot 8, a distance of 6.00 feet; thence Northerly to the point of intersection with a line which runs parallel with and 50.00 feet Westerly from the Easterly line of said Avenue, said point of intersection being 31.52 feet Southerly of the Easterly extension of the North line of said Lot 8, as measured along the last said parallel line; thence Northerly along said parallel line, a distance of 31.52 feet of said Easterly extension of the North line of Lot 8; thence West along said Easterly extension, to the Northeast corner of said Lot 8; thence Southerly, along said East line of Lot 8, to said point of beginning; That part of Service Lane lying South of the center line thereof and between the Westerly right-of-way line of Merrivale Avenue and a Northerly extension of the Westerly line of Lot 8, Block 3, "Boulevard Gardens, Hennepin County Minnesota."

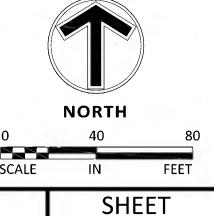
Parcel 2: Lots 9, 10, 11, 12 and 13, Block 3, "Boulevard Gardens, Hennepin County Minnesota.", except the South 10 feet of said Lots 9, 10, 11, 12 and 13 and except that part of said Lots 11, 12 and 13 that is designated and delineated as Parcel 10C on the Minnesota Department of Transportation Right-of-Way plat No 27-37.

The following notes correspond to the reference numbers listed in Schedule B, Section 2 of the title commitment.

- 10. Subject to a perpetual easement in favor of the City of Minnetonka, its successors and/or assigns for public purposes over, under and across Merrivale Avenue as shown in Document No 1452330; (as to Par 1) shown as a recital on the Certificate of Title. According to the description in said document, the Right-of-Way lies within the surveyed property as shown hereon.
- 11. Subject to a reservation by the State of Minnesota of minerals and mineral rights; (as to Lot 9 in Par 2), shown as a recital on the Certificate of Title. The document is blanket in nature and are not graphically depicted
- 12. Easement for highway purposes (Trunk Highway No. 12) acquired by State of Minnesota over Southerly 10 feet together with the right of construct and maintain temporary snow fences on lands adjacent thereto, as evidenced by Final Certificate, recorded January 14, 1938, as Document No. 139851 (Not reflected on the Certificate of Title). According to the description in said document, the Right-of-Way lies adjacent to the surveyed property as shown hereon.
- 13. State Right-of-Way Plat, recorded November 6, 1986, as Document No. 1772907. According to the description in said document, the Right-of-Way is the southern boundary of the surveyed property as shown hereon.
- 14. No right of access exists from premises to Interstate Highway No. 394. Right of access was acquired by the State of Minnesota as evidenced by Final Certificate, recorded September 12, 1990 as Document No. 2123328. (Not reflected on the Certificate of Title) According to the description in said document, the Right of Access adjoins the surveyed property as shown hereon. Based on the description in said document, the right of access to Parcel 10-C was not specifically taken by said document. The Surveyor is not depicting any access restrictions on the survey. Direct access to Interstate 394 is obstructed by a chainlink fence on the south side of Wayzata Boulevard frontage
- 15. Terms and conditions as contained in Planning Commission Resolution No. 2019-06, recorded March 21, 2019, as Document No. T05601870. According to the description in said document, the resolution does not lie within or benefit the surveyed property and is not graphically depicted

TABLE A" NOTES

- 1. The survey shows property corner monuments or witness to the corner that were found during the field work, as well as property corner monuments or witness to the corner set by the surveyor at locations where there did not appear to be any evidence of an existing monument.
- 2. The address of the surveyed property is shown on the graphical portion of the survey.
- 3. The surveyed property lies within Flood Plain Zone X 'Areas determined to be outside the 0.2% annual chance flood plain' and Zone A, as depicted by scaled map location and graphic plotting according to FEMA, FIRM Map No. 27053C0331F dated 11/04/2016.
- 4. The gross land area of the surveyed property is 5.260 Acres or 229,125 Square Feet.
- 7a. The buildings and exterior dimensions of the outside wall at ground level are shown on the survey, which may or may not be the foundation wall.
- 7b1. The square footage of the buildings is are shown on the survey square feet, measured at ground
- 8. Visible substantial features observed in the process of conducting the fieldwork are shown hereon.
- 9. The parking areas and striping on the surveyed property are shown. There are 7 striped handicap parking stalls, and there are 149 striped regular parking stalls for a total of 146 striped parking stalls.
- 11. Evidence of underground utilities existing on or serving the surveyed property is shown per the a) Plans and/or reports were provided by the client.
- 13. The names of adjoining land owners according to the current county tax records as of 01/16/2023 are shown on the survey.
- 16. There is no evidence of recent earth moving work, building construction or building additions observed in the process of conducting the fieldwork for this survey.
- 17. No changes in street right of ways are proposed per CITY OF MINNETONKA website. There is no observable evidence of recent street or sidewalk construction or repair.
- 18. Plottable off site easements and servitudes disclosed in the provided title documents and/or observed during the field work that appear to benefit and/or affect the subject property are shown
- 19. Evidence of professional liability insurance obtained by the surveyor will be furnished upon request.



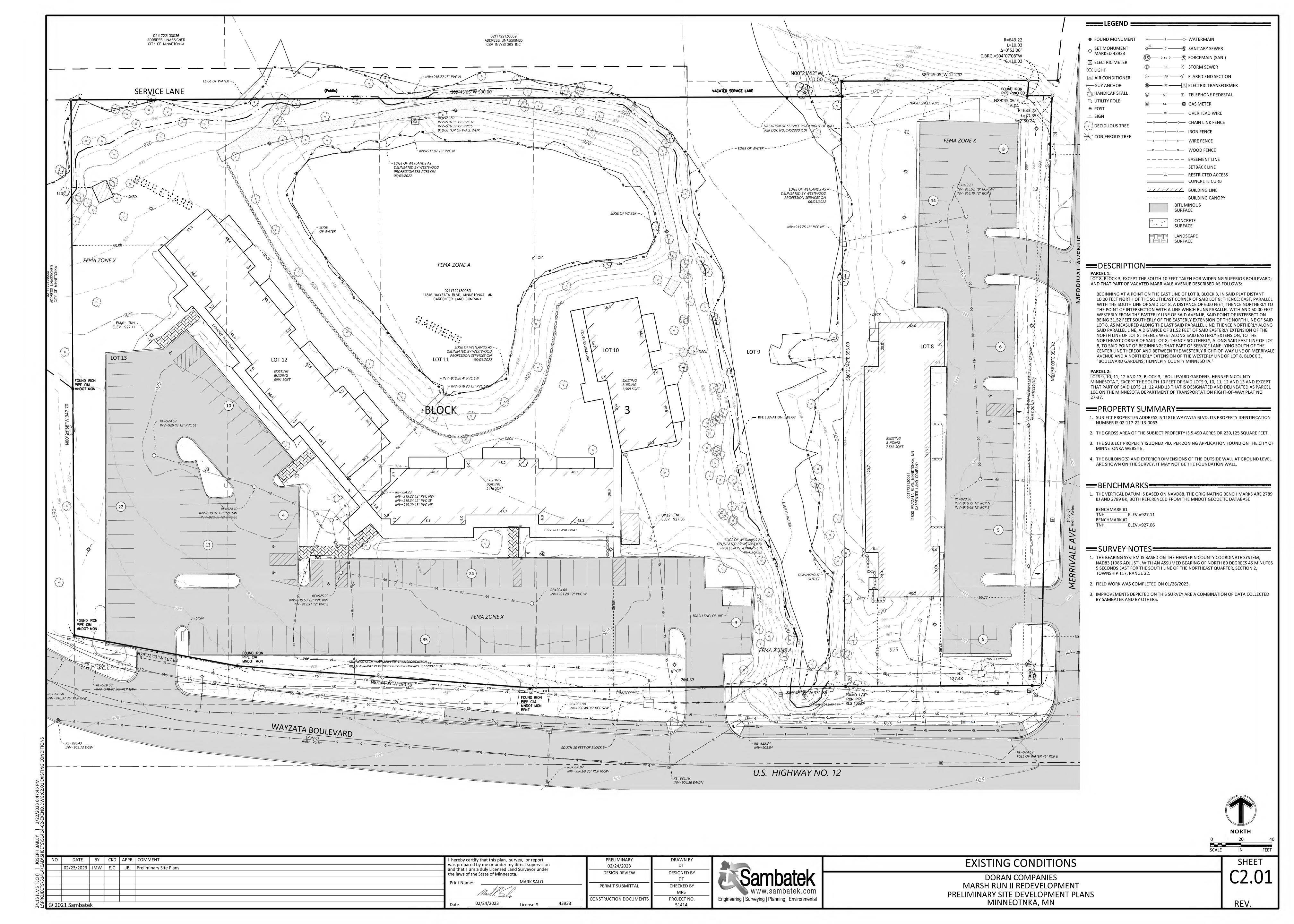
DATE BY CKD APPR COMMENT CDJ **DESIGNED BY CHECKED BY** JN PROJECT NO. 🛭 2021 Sambatek

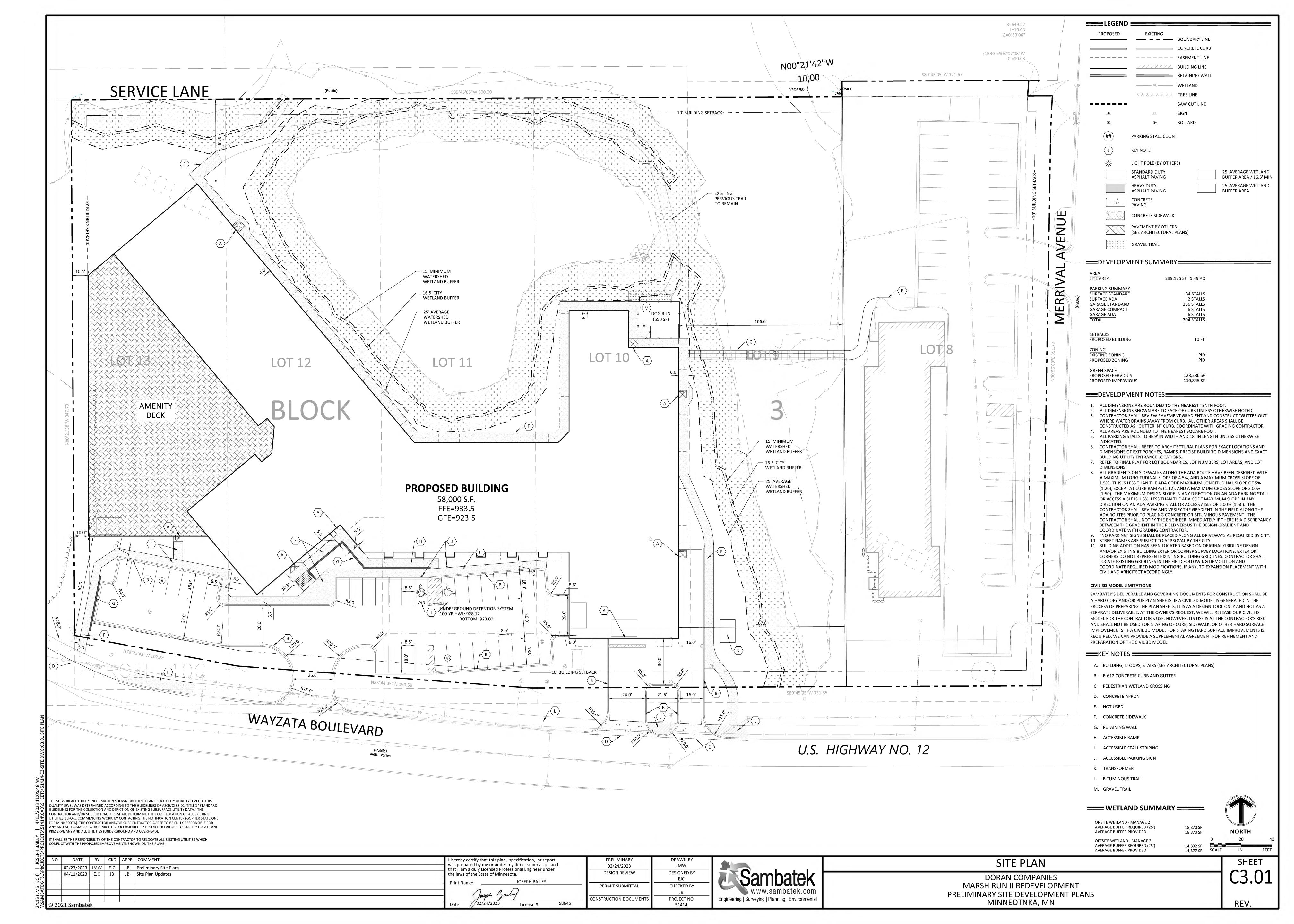
Engineering | Surveying | Planning | Environmenta

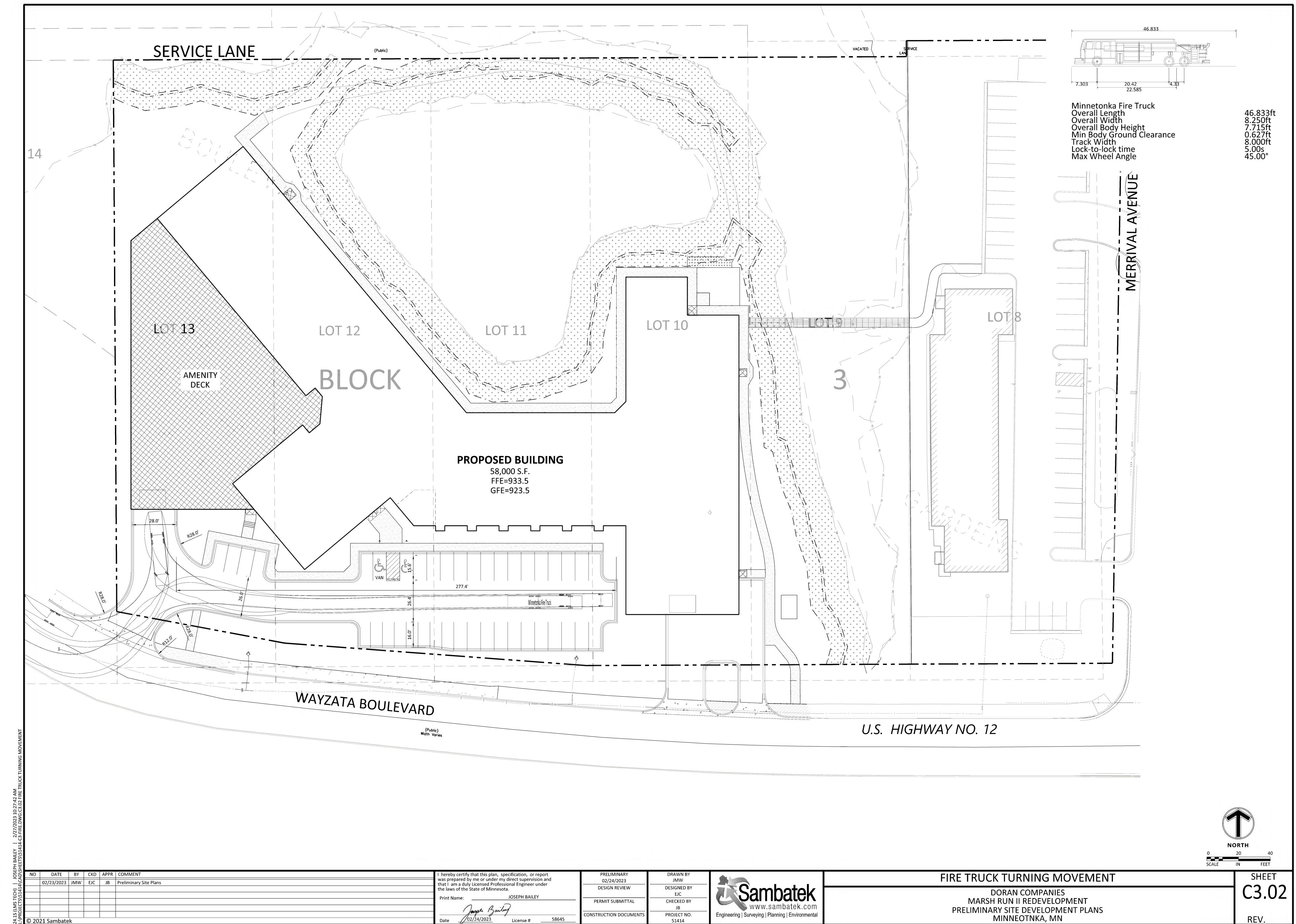
ALTA/NSPS Land Title Survey DORAN RE PARNERS, LLC

MARSH RUN II 11900 WAYZATA BLVD MINNETONKA, MN

OF 1 REV. A



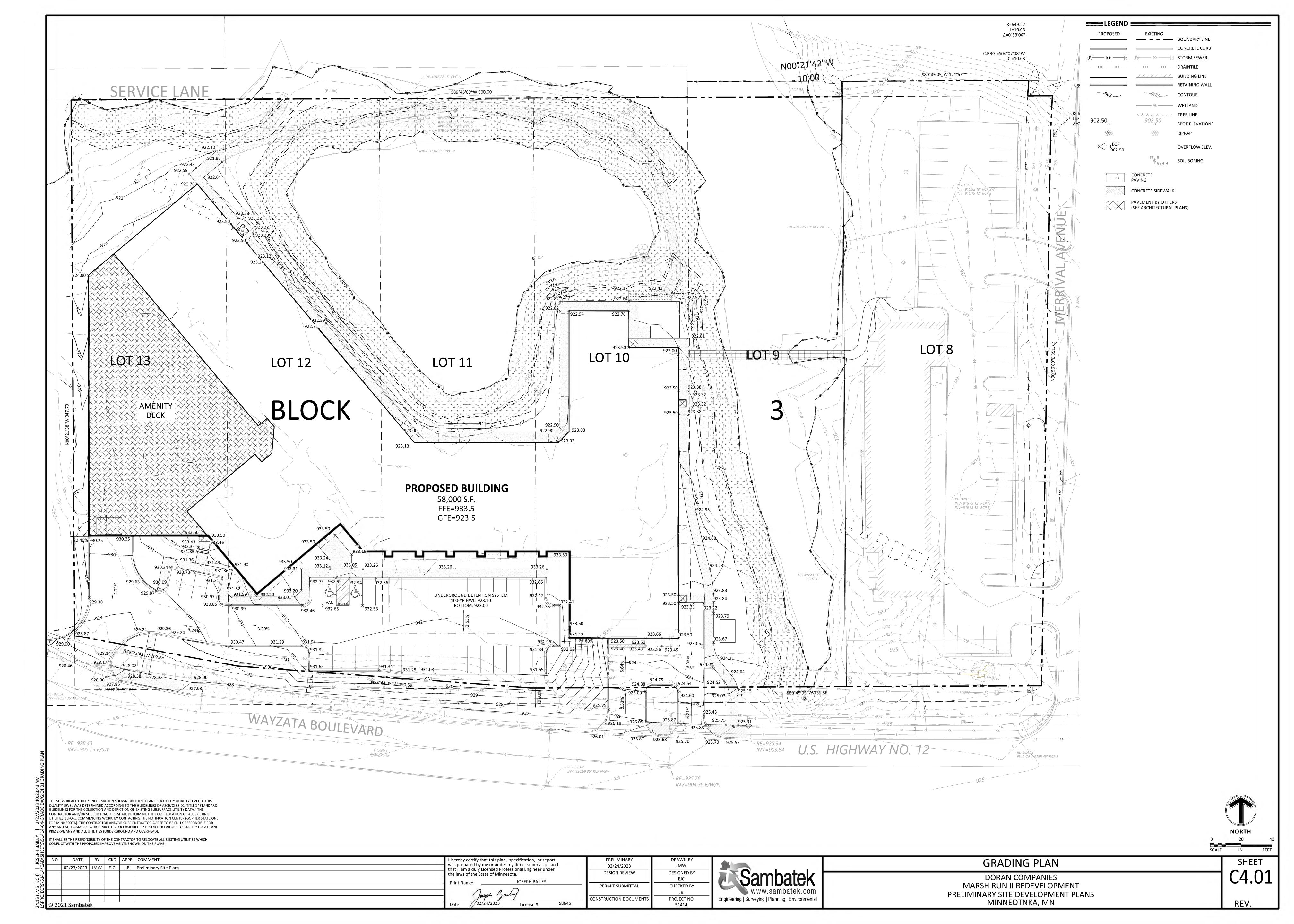




CONSTRUCTION DOCUMENTS

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PROJECT NO. 51414



GRADING NOTES

- 1. PROPOSED CONTOURS ARE TO FINISHED SURFACE ELEVATION. SPOT ELEVATIONS ALONG PROPOSED CURB DENOTE GUTTER GRADE.
- 2. CONTRACTOR SHALL REVIEW PAVEMENT GRADIENT AND CONSTRUCT "GUTTER OUT" WHERE WATER DRAINS AWAY FROM CURB. ALL OTHER AREAS SHALL BE CONSTRUCTED AS "GUTTER IN" CURB.
- 3. ALL GRADIENT ON SIDEWALKS ALONG THE ADA ROUTE SHALL HAVE A MAXIMUM LONGITUDINAL SLOPE OF 5% (1:20), EXCEPT AT CURB RAMPS (1:12), AND A MAXIMUM CROSS SLOPE OF 2.00% (1:50). MAXIMUM SLOPE IN ANY DIRECTION ON AN ADA PARKING STALL OR ACCESS AISLE SHALL BE IN 2.00% (1:50). CONTRACTOR SHALL REVIEW AND VERIFY THE GRADIENT IN THE FIELD ALONG THE ADA ROUTES PRIOR TO PLACING CONCRETE OR BITUMINOUS. CONTRACTOR SHALL NOTIFY THE ENGINEER IMMEDIATELY IF THERE IS A DISCREPANCY BETWEEN THE GRADIENT IN THE FIELD VERSUS THE DESIGN GRADIENT. COORDINATE ALL WORK WITH PAVING CONTRACTOR.
- 4. CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO AVOID PROPERTY DAMAGE TO ADJACENT PROPERTIES DURING THE CONSTRUCTION PHASES OF THIS PROJECT. CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR ANY DAMAGES TO THE ADJACENT PROPERTIES OCCURRING DURING THE CONSTRUCTION PHASES OF THIS PROJECT.
- 5. SAFETY NOTICE TO CONTRACTORS: IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS ON THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS. THE DUTY OF THE ENGINEER OR THE DEVELOPER TO CONDUCT CONSTRUCTION REVIEW OF THE CONTRACTOR'S PERFORMANCE IS NOT INTENDED TO INCLUDE REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES IN, ON OR NEAR THE CONSTRUCTION SITE.
- 6. CONTRACTOR SHALL COMPLETE THE SITE GRADING CONSTRUCTION IN ACCORDANCE WITH THE REQUIREMENTS OF THE OWNER'S SOILS ENGINEER. ALL SOIL TESTING SHALL BE COMPLETED BY THE OWNER'S SOILS ENGINEER. CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING ALL REQUIRED SOIL TESTS AND INSPECTIONS WITH THE SOILS ENGINEER.

A GEOTECHNICAL ENGINEERING SOILS REPORT HAS BEEN COMPLETED BY:

COMPANY: BRAUN INTERTEC

ADDRESS: 1101 HAMPSHIRE AVE S, MINNEAPOLIS, MN 55438

PHONE: 952-995-2238

DATE: 02/23/2023

CONTRACTOR SHALL OBTAIN A COPY OF THE SOILS REPORT.

- 7. CONTRACTOR SHALL COMPLETE DEWATERING AS REQUIRED TO COMPLETE THE SITE GRADING CONSTRUCTION.
- 8. PRIOR TO PLACEMENT OF THE AGGREGATE BASE, A TEST ROLL SHALL BE PERFORMED ON THE STREET AND PARKING AREA SUBGRADE. CONTRACTOR SHALL PROVIDE A LOADED TANDEM AXLE TRUCK WITH A GROSS WEIGHT OF 25 TONS. THE TEST ROLLING SHALL BE AT THE DIRECTION OF THE SOILS ENGINEER AND SHALL BE COMPLETED IN AREAS AS DIRECTED BY THE SOILS ENGINEER. CORRECTION OF THE SUBGRADE SOILS SHALL BE COMPLETED IN ACCORDANCE WITH THE REQUIREMENTS OF THE SOILS ENGINEER.
- 9. REPLACE ALL SUBGRADE SOIL DISTURBED DURING THE CONSTRUCTION THAT HAVE BECOME UNSUITABLE AND WILL NOT PASS A TEST ROLL. REMOVE UNSUITABLE SOIL FROM THE SITE AND IMPORT SUITABLE SOIL AT NO ADDITIONAL COST TO THE OWNER.
- 10. CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING AND MAINTAINING VEHICULAR AND PEDESTRIAN TRAFFIC CONTROL DEVICES SUCH AS BARRICADES, WARNING SIGNS, DIRECTIONAL SIGNS, FLAGMEN AND LIGHTS TO CONTROL THE MOVEMENT OF TRAFFIC WHERE NECESSARY. TRAFFIC CONTROL DEVICES SHALL CONFORM TO APPROPRIATE MINNESOTA DEPARTMENT OF TRANSPORTATION STANDARDS.
- 11. EXISTING TREES AND OTHER NATURAL VEGETATION WITHIN THE PROJECT AND/OR ADJACENT TO THE PROJECT ARE OF PRIME CONCERN TO THE CONTRACTOR'S OPERATIONS AND SHALL BE A RESTRICTED AREA. CONTRACTOR SHALL PROTECT TREES TO REMAIN AT ALL TIMES. EQUIPMENT SHALL NOT NEEDLESSLY BE OPERATED UNDER NEARBY TREES AND EXTREME CAUTION SHALL BE EXERCISED WHEN WORKING ADJACENT TO TREES. SHOULD ANY PORTION OF THE TREE BRANCHES REQUIRE REMOVAL TO PERMIT OPERATION OF THE CONTRACTOR'S EQUIPMENT. CONTRACTOR SHALL OBTAIN THE SERVICES OF A PROFESSIONAL TREE TRIMMING SERVICE TO TRIM THE TREES PRIOR TO THE BEGINNING OF OPERATION. SHOULD CONTRACTOR'S OPERATIONS RESULT IN THE BREAKING OF ANY LIMBS, THE BROKEN LIMBS SHOULD BE REMOVED IMMEDIATELY AND CUTS SHALL BE PROPERLY PROTECTED TO MINIMIZE ANY LASTING DAMAGE TO THE TREE. NO TREES SHALL BE REMOVED WITHOUT AUTHORIZATION BY THE ENGINEER. COSTS FOR TRIMMING SERVICES SHALL BE CONSIDERED INCIDENTAL TO THE GRADING CONSTRUCTION AND NO SPECIAL PAYMENT WILL BE MADE.
 - a. RESTRICTED AREAS SHALL INCLUDE ALL DESIGNATED TREED AREAS OUTSIDE OF THE DESIGNATED CONSTRUCTION ZONE. ALL VEGETATION WITHIN THE RESTRICTED AREAS SHALL REMAIN.
 - b. CONTRACTOR SHALL RESTRICT ALL GRADING AND CONSTRUCTION ACTIVITIES TO AREAS DESIGNATED ON THE PLANS. ACTIVITIES WITHIN THE CONSTRUCTION MAY BE RESTRICTED TO A NARROWER WIDTH IN THE FIELD TO SAVE ADDITIONAL TREES AS DIRECTED BY THE OWNER.
 - c. ACTIVITIES PROHIBITED OUTSIDE OF THE CONSTRUCTION BOUNDARIES WOULD INCLUDE, BUT NOT BE LIMITED TO: SOIL AND OTHER MATERIAL STOCKPILING, EQUIPMENT OR MACHINERY STORAGE, DRIVING OF ANY VEHICLE, LEAKAGE OR SPILLAGE OF ANY "WASHOUT" OR OTHER TOXIC MATERIAL. THE COLLECTION OF OTHER DEBRIS AND SOIL STOCKPILING WILL BE IN AN AREA DETERMINED ON-SITE BY THE ENGINEER.
 - d. ALL RESTRICTED AREAS SHALL BE FENCED OFF WITH BRIGHT ORANGE POLYETHYLENE SAFETY NETTING AND STEEL STAKES AS SHOWN ON THE TREE PROTECTION DETAIL. AT NO TIME SHALL THIS FENCING BE REMOVED OR ACTIVITY OF ANY KIND TAKE PLACE WITHIN IT. FINAL PLACEMENT OF ALL PROTECTIVE FENCING SHALL BE COMPLETE BEFORE ANY WORK COMMENCES ON-SITE.
 - e. BEFORE COMMENCING WITH ANY EXCAVATION CONTRACTOR SHALL COMPLETE ALL PREPARATORY WORK REGARDING TREE REMOVAL, ROOT PRUNING, TREE PRUNING AND STUMP REMOVAL TO THE SATISFACTION OF THE OWNER.
 - f. PREPARATORY WORK SHALL INCLUDE THE FOLLOWING AND SHALL BE COMPLETED UNDER THE DIRECT SUPERVISION OF THE OWNER'S REPRESENTATIVE:
 - i. TREE REMOVAL: CONTRACTOR SHALL FELL THE TREES. AT NO TIME SHALL TREES BE BULLDOZED OUT, BUT SHALL BE CUT DOWN AND STUMPS REMOVED SEPARATELY. PRIOR TO THE FELLING OF ALL TREES, PROPER REMOVAL OF A PORTION OR ALL OF THE CANOPY SHALL BE COMPLETED SO THAT TREES IN THE RESTRICTED AREAS SHALL NOT BE INJURED IN THE PROCESS.
 - ii. ROOT PRUNING: BEFORE ANY STUMPS ARE TO BE REMOVED, ALL ROOTS

- SHALL BE SEVERED FROM ROOTS IN THE RESTRICTED AREAS BY SAW CUTTING WITH A VERMEER DESIGNED FOR ROOT PRUNING, BY HAND, OR WITH A CHAINSAW. TREE ROOTS PROJECTING INTO THE CONSTRUCTION ZONE SHALL BE EXPOSED PRIOR TO ROOT PRUNING WITH SMALL MACHINERY, I.E.... BOBCAT.
- iii.STUMP REMOVAL: AT SUCH TIME THAT ROOTS HAVE BEEN PROPERLY SEVERED, STUMPS MAY BE REMOVED. WHERE REMOVAL OF CERTAIN STUMPS COULD CAUSE DAMAGE TO EXISTING PROTECTED TREES, TREE STUMPS SHALL BE GROUND OUT. ALL STUMP REMOVAL SHALL BE UNDER THE DIRECT SUPERVISION OF THE OWNER'S REPRESENTATIVE.
- iv.TREE PRUNING: PROPER PRUNING OF TREES IN THE RESTRICTED ZONE SHALL BE DIRECTED BY AND SUPERVISION AT ALL TIMES BY THE OWNER'S REPRESENTATIVE.
- g. AN OWNER'S REPRESENTATIVE WILL BE AVAILABLE AT ALL TIMES DURING THE PREPARATORY AND CONSTRUCTION PERIOD.
- h. MULCH RATHER THAN SEED OR SOD WILL BE USED AT THE BASE OF QUALITY TREES TO A PERIMETER DETERMINED BY THE OWNER'S REPRESENTATIVE. AREAS TO BE SEEDED FOR EROSION CONTROL PURPOSES WITHIN THE CONSTRUCTION ZONE ARE TO BE DETERMINED BY THE OWNER'S REPRESENTATIVE. NATURAL GROUND COVER WILL BE MAINTAINED WHEREVER POSSIBLE.
- i. THE USE OF RETAINING WALLS NEAR TREES, IN ADDITION TO THOSE REQUIRED ON THE PLANS SHALL BE DETERMINED IN THE FIELD, BASED ON TREE LOCATIONS AND TOPOGRAPHY.
- 12. EXCAVATE TOPSOIL FROM AREAS TO BE FURTHER EXCAVATED OR REGRADED AND STOCKPILE IN AREAS DESIGNATED ON THE SITE. CONTRACTOR SHALL SALVAGE ENOUGH TOPSOIL FOR RESPREADING ON THE SITE AS SPECIFIED. EXCESS TOPSOIL SHALL BE PLACED IN EMBANKMENT AREAS, OUTSIDE OF BUILDING PADS, ROADWAYS AND PARKING AREAS. CONTRACTOR SHALL SUBCUT CUT AREAS, WHERE TURF IS TO BE ESTABLISHED, TO A DEPTH OF 6 INCHES. RESPREAD TOPSOIL IN AREAS WHERE TURF IS TO BE ESTABLISHED TO A MINIMUM DEPTH OF 6 INCHES.
- 13. TRENCH BORROW CONSTRUCTION: IF ALLOWED BY THE OWNER, CONTRACTOR SHALL COMPLETE "TRENCH BORROW" EXCAVATION IN AREAS DIRECTED BY THE ENGINEER IN ORDER TO OBTAIN STRUCTURAL MATERIAL. TREES SHALL NOT BE REMOVED OR DAMAGED AS A RESULT OF THE EXCAVATION, UNLESS APPROVED BY THE ENGINEER. THE EXCAVATION SHALL COMMENCE A MINIMUM OF 10 FEET FROM THE LIMIT OF THE BUILDING PAD. THE EXCAVATION FROM THIS LIMIT SHALL EXTEND AT A MINIMUM SLOPE OF 1 FOOT HORIZONTAL TO 1 FOOT VERTICAL (1:1) DOWNWARD AND OUTWARD FROM THE FINISHED SURFACE GRADE ELEVATION. THE TRENCH BORROW EXCAVATION SHALL BE BACKFILLED TO THE PROPOSED FINISHED GRADE ELEVATION, AND SHALL BE COMPACTED IN ACCORDANCE WITH REQUIREMENTS OF THE QUALITY COMPACTION METHOD AS OUTLINED IN MN/DOT SPECIFICATION 2105.3F2. SNOW FENCE SHALL BE FURNISHED AND PLACED ALONG THE PERIMETER OF THE TRENCH BORROW AREA WHERE THE SLOPES EXCEED 2 FOOT HORIZONTAL TO 1 FOOT VERTICAL (2:1).
- 14. FINISHED GRADING SHALL BE COMPLETED, CONTRACTOR SHALL UNIFORMLY GRADE AREAS WITHIN LIMITS OF GRADING, INCLUDING ADJACENT TRANSITION AREAS. PROVIDE A SMOOTH FINISHED SURFACE WITHIN SPECIFIED TOLERANCES, WITH UNIFORM LEVELS OR SLOPES BETWEEN POINTS WHERE ELEVATIONS ARE SHOWN, OR BETWEEN SUCH POINTS AND EXISTING GRADES. AREAS THAT HAVE BEEN FINISHED GRADED SHALL BE PROTECTED FROM SUBSEQUENT CONSTRUCTION OPERATIONS, TRAFFIC AND EROSION. REPAIR ALL AREAS THAT HAVE BECOME RUTTED, ERODED OR HAS SETTLED BELOW THE CORRECT GRADE. ALL AREAS DISTURBED BY THE CONTRACTOR'S OPERATIONS SHALL BE RESTORED TO EQUAL OR BETTER THAN ORIGINAL CONDITION OR TO THE REQUIREMENTS OF THE NEW WORK.
- 15. TOLERANCES
 - a. THE RESIDENTIAL BUILDING SUBGRADE FINISHED SURFACE ELEVATION SHALL NOT VARY BY MORE THAN 0.30 FOOT ABOVE, OR 0.30 FOOT BELOW, THE PRESCRIBED ELEVATION AT ANY POINT WHERE MEASUREMENT IS MADE.
 - b. THE COMMERCIAL BUILDING SUBGRADE FINISHED SURFACE ELEVATION SHALL NOT VARY BY MORE THAN 0.10 FOOT ABOVE, OR 0.10 FOOT BELOW, THE PRESCRIBED ELEVATION AT ANY POINT WHERE MEASUREMENT IS MADE.
 - c. THE STREET OR PARKING AREA SUBGRADE FINISHED SURFACE ELEVATION SHALL NOT VARY BY MORE THAN 0.05 FOOT ABOVE, OR 0.10 FOOT BELOW, THE PRESCRIBED ELEVATION OF ANY POINT WHERE MEASUREMENT IS MADE.
 - d. AREAS WHICH ARE TO RECEIVE TOPSOIL SHALL BE GRADED TO WITHIN 0.30 FOOT ABOVE OR BELOW THE REQUIRED ELEVATION, UNLESS DIRECTED OTHERWISE BY THE ENGINEER.
 - e. TOPSOIL SHALL BE GRADED TO PLUS OR MINUS 1/2 INCH OF THE SPECIFIED THICKNESS.
- 16. AFTER THE SITE GRADING IS COMPLETED, IF EXCESS OR SHORTAGE OF SOIL MATERIAL EXISTS, CONTRACTOR SHALL TRANSPORT ALL EXCESS SOIL MATERIAL OFF THE SITE TO AN AREA SELECTED BY THE CONTRACTOR, OR IMPORT SUITABLE MATERIAL TO THE SITE.
- 17. CONTRACTOR SHALL DETERMINE THE LOCATION OF ANY HAUL ROADS THAT MAY BE REQUIRED TO COMPLETE THE SITE GRADING CONSTRUCTION AND SHALL INDICATE HAUL ROADS ON EROSION AND SEDIMENT CONTROL "SITE MAP". CONTRACTOR SHALL COMPLY WITH THE REQUIREMENTS OF THE GOVERNING AUTHORITY OF EACH ROADWAY. CONTRACTOR SHALL POST WHATEVER SECURITY AND COMPLY WITH ALL CONDITIONS WHICH ARE REQUIRED BY EACH GOVERNING AUTHORITY OF EACH ROADWAY.
- 18. DISTURBED AREAS WITHIN WETLAND MITIGATION SITE AND ANY DISTURBED AREAS WITHIN THE WETLAND SHALL BE RESTORED WITH 6 TO 12 INCHES OF ORGANIC SOILS, PREFERABLY SOILS THAT WERE PREVIOUSLY REMOVED FROM WETLAND AREAS. SEEDING IN THE WETLAND MITIGATION AREAS ABOVE THE NORMAL WATER LEVEL SHALL BE MN STATE SEED MIX 34-271, WET MEADOW SOUTH AND WEST, OR APPROVED EQUAL. FOR STATE SEED MIXES, OATS AND WINTER WHEAT SHOULD BE SELECTED BASED ON THE TIME OF YEAR THAT THE MIX IS BEING USED. OATS SHOULD BE INCLUDED IN MIXES IF BEING USED BETWEEN OCTOBER 15TH AND AUGUST 1ST. WINTER WHEAT SHOULD BE USED BETWEEN AUGUST 1ST AND OCTOBER 15TH. THE SEEDING RATE IS THE SAME FOR OATS AND WINTER WHEAT. MIX 34-271 SHOULD BE APPLIED AT 12 POUNDS PER ACRE. SEED SHALL BE WATERED UNTIL A HEALTHY STAND OF VEGETATION IS OBTAINED.
- 19. FILL PLACED WITHIN THE BUILDING PAD AREAS SHALL BE IN CONFORMANCE WITH HUD/FHA PROCEDURES AND DATA SHEET 79G.

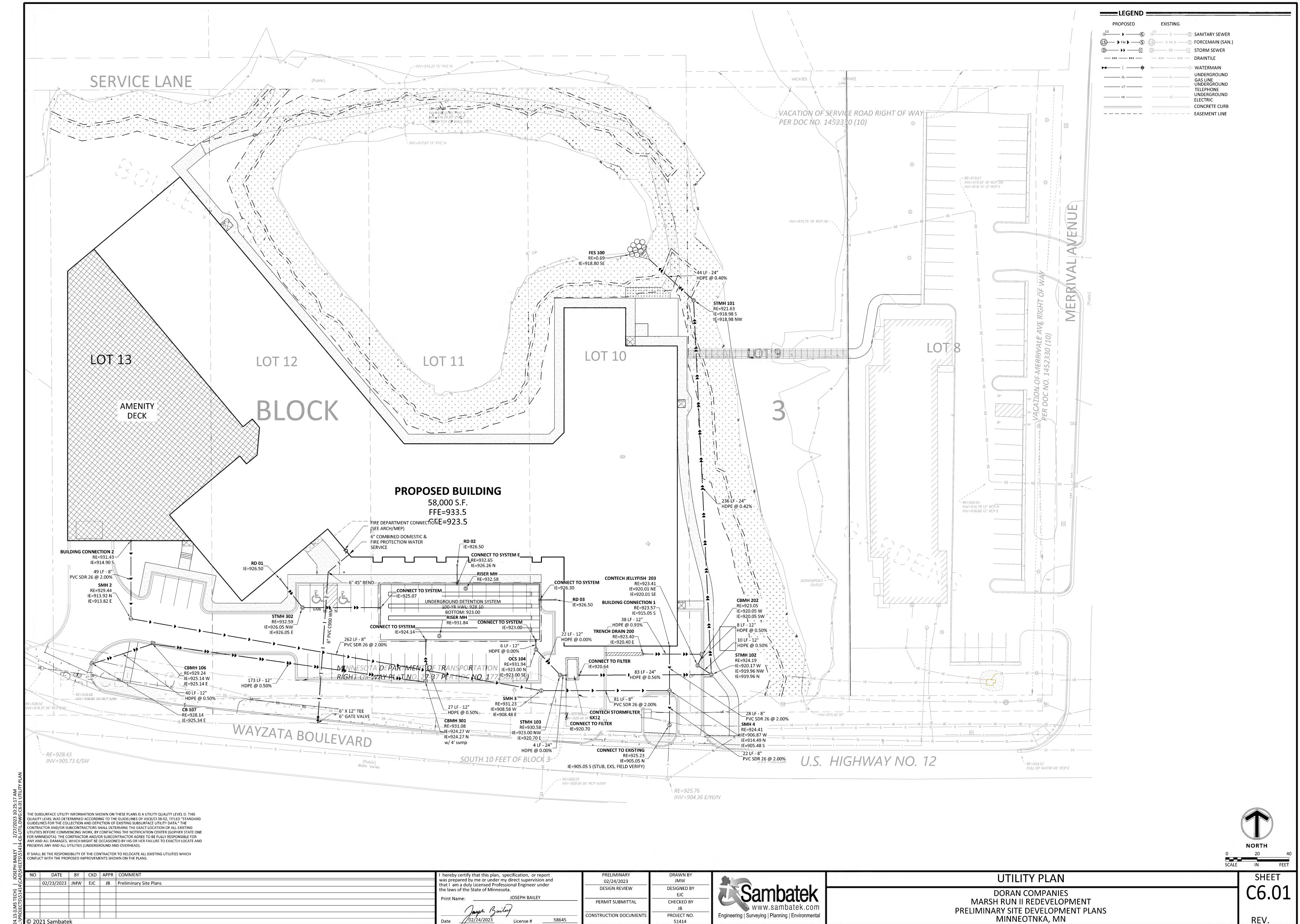
CIVIL 3D MODEL LIMITATIONS

SAMBATEK'S DELIVERABLE AND GOVERNING DOCUMENTS FOR CONSTRUCTION SHALL BE A HARD COPY AND/OR PDF PLAN SHEETS. IF A CIVIL 3D MODEL IS GENERATED IN THE PROCESS OF PREPARING THE PLAN SHEETS, IT IS AS A DESIGN

TOOL ONLY AND NOT AS A SEPARATE DELIVERABLE. AT THE OWNER'S REQUEST, WE WILL RELEASE OUR CIVIL 3D MODEL FOR THE CONTRACTOR'S USE. HOWEVER, ITS USE IS AT THE CONTRACTOR'S RISK AND SHALL NOT BE USED FOR STAKING OF CURB, SIDEWALK, OR OTHER HARD SURFACE IMPROVEMENTS. IF A CIVIL 3D MODEL FOR STAKING HARD SURFACE IMPROVEMENTS IS REQUIRED, WE CAN PROVIDE A SUPPLEMENTAL AGREEMENT FOR REFINEMENT AND PREPARATION OF THE CIVIL 3D MODEL.

REV. DATE

DATE BY CKD APPR COMMENT **SHEET** hereby certify that this plan, specification, or report **GRADING NOTES** was prepared by me or under my direct supervision and JMW 02/24/2023 02/23/2023 | JMW | EJC | JB | Preliminary Site Plans that I am a duly Licensed Professional Engineer under **DESIGN REVIEW DESIGNED BY** the laws of the State of Minnesota. **DORAN COMPANIES** EJC JOSEPH BAILEY MARSH RUN II REDEVELOPMENT CHECKED BY PERMIT SUBMITTAL PRELIMINARY SITE DEVELOPMENT PLANS CONSTRUCTION DOCUMENTS Engineering | Surveying | Planning | Environmenta PROJECT NO. MINNEOTNKA, MN 02/24/2023 D 2021 Sambatek License # 51414



CONSTRUCTION DOCUMENTS

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PROJECT NO. 51414

Engineering | Surveying | Planning | Environmental

——UTILITY CONSTRUCTION NOTES ——————

HEALTH REQUIREMENTS.

- THE UTILITY IMPROVEMENTS FOR THIS PROJECT SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE "STANDARD UTILITIES SPECIFICATIONS" AS PUBLISHED BY THE CITY ENGINEERS ASSOCIATION OF MINNESOTA (CEAM), EXCEPT AS MODIFIED HEREIN. CONTRACTOR SHALL OBTAIN A COPY OF THESE SPECIFICATIONS.

 ALL UTILITIES SHALL BE CONSTRUCTED IN ACCORDANCE WITH ALL LOCAL, STATE AND FEDERAL REQUIRMENTS, INCLUDING BUT NOT LIMITED TO CITY, DEPARTMENT OF LABOR AND INDUSTRY AND MINNESOTA DEPARTMENT OF
 - b. CONTRACTOR SHALL NOT OPEN, TURN OFF, INTERFERE WITH, OR ATTACH ANY PIPE OR HOSE TO OR TAP WATERMAIN BELONGING TO THE CITY UNLESS DULY AUTHORIZED TO DO SO BY THE CITY. ANY ADVERSE CONSEQUENCES OF ANY SCHEDULED OR UNSCHEDULED DISRUPTIONS OF SERVICE TO THE PUBLIC ARE THE LIABILITY OF CONTRACTOR.
 - c. A MINIMUM VERTICAL SEPARATION OF 18 INCHES, AND HORIZONTAL SEPARATION OF 10-FEET, BETWEEN OUTSIDE PIPE AND/OR STRUCTURE WALLS, IS REQUIRED AT ALL WATERMAIN AND SEWER MAIN (BUILDING, STORM AND SANITARY) CROSSINGS.
- 2. ALL MATERIALS SHALL BE AS SPECIFIED IN CEAM SPECIFICATIONS EXCEPT AS MODIFIED HEREIN.
 - a. ALL MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE CITY.
 - b. ALL SANITARY SEWER TO BE PVC SDR-35, UNLESS NOTED OTHERWISE.
 - i. ALL SANITARY SEWER SERVICES TO BUILDING SHALL BE PVC SCH 40 CONFORMING TO ASTM D2665.
 - c. ALL WATERMAIN TO BE DUCTILE IRON CLASS 52, or PVC C-900, UNLESS NOTED OTHERWISE.
 - i. ALL WATERMAIN TO HAVE 7.5-FEET OF COVER OVER TOP OF WATERMAIN.
 - ii. PROVIDE THRUST BLOCKING AND MECHANICAL JOINT RESTRAINTS ON ALL WATERMAIN JOINTS PER CITY STANDARDS.
 - iii.WHERE A SEWER LINE CROSSES A WATER SERVICE, THE WATER SERVICE SHALL NOT CONTAIN ANY JOINTS OR CONNECTIONS WITHIN 10 FEET OF THE CROSSING.
 - d. ALL STORM SEWER PIPE TO BE SMOOTH INTERIOR DUAL WALL HDPE PIPE WITH WATERTIGHT GASKETS, UNLESS NOTED OTHERWISE.
 - i. ALL STORM SEWER PIPE FOR ROOF DRAIN SERVICES TO BUILDING SHALL BE PVC SCH 40 CONFORMING TO ASTM D2665.
 e. RIP RAP SHALL BE Mn/DOT CLASS
- 3. COORDINATE ALL BUILDING SERVICE CONNECTION LOCATIONS AND INVERT ELEVATIONS WITH MECHANICAL CONTRACTOR PRIOR TO CONSTRUCTION.
- 4. ALL BUILDING SERVICE CONNECTIONS (STORM, SANITARY, WATER) WITH FIVE FEET OR LESS COVER ARE TO BE INSULATED FROM BUILDING TO POINT WHERE 5-FEET OF COVER IS ACHIEVED.
- 5. CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO AVOID PROPERTY DAMAGE TO ADJACENT PROPERTIES DURING THE CONSTRUCTION PHASES OF THIS PROJECT. CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR ANY DAMAGES TO THE ADJACENT PROPERTIES OCCURRING DURING THE CONSTRUCTION PHASES OF THIS PROJECT.
- 6. SAFETY NOTICE TO CONTRACTORS: IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS ON THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS. THE DUTY OF THE ENGINEER OR THE DEVELOPER TO CONDUCT CONSTRUCTION REVIEW OF CONTRACTOR'S PERFORMANCE IS NOT INTENDED TO INCLUDE REVIEW OF THE ADEQUACY OF CONTRACTOR'S SAFETY MEASURES IN, ON OR NEAR THE CONSTRUCTION SITE.
- 7. ALL AREAS OUTSIDE THE PROPERTY BOUNDARIES THAT ARE DISTURBED BY UTILITY CONSTRUCTION SHALL BE RESTORED IN KIND. SODDED AREAS SHALL BE RESTORED WITH 6 INCHES OF TOPSOIL PLACED BENEATH THE SOD.
- 8. CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING AND MAINTAINING TRAFFIC CONTROL DEVICES SUCH AS BARRICADES, WARNING SIGNS, DIRECTIONAL SIGNS, FLAGMEN AND LIGHTS TO CONTROL THE MOVEMENT OF TRAFFIC WHERE NECESSARY. TRAFFIC CONTROL DEVICES SHALL CONFORM TO APPROPRIATE MINNESOTA DEPARTMENT OF TRANSPORTATION STANDARDS.
- 9. ALL SOILS TESTING SHALL BE COMPLETED BY AN INDEPENDENT SOILS ENGINEER. EXCAVATION FOR THE PURPOSE OF REMOVING UNSTABLE OR UNSUITABLE SOILS SHALL BE COMPLETED AS REQUIRED BY THE SOILS ENGINEER. THE UTILITY BACKFILL CONSTRUCTION SHALL COMPLY WITH THE REQUIREMENTS OF THE SOILS ENGINEER. CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING ALL REQUIRED SOILS TESTS AND SOIL INSPECTIONS WITH THE SOILS ENGINEER. A GEOTECHNICAL ENGINEERING REPORT HAS BEEN COMPLETED BY: COMPANY: BRAUN INTERTEC
- ADDRESS: 11001 HAMPSHIRE AVE S, MINNEAPOLIS, MN 55438

PHONE: 952-995-2238

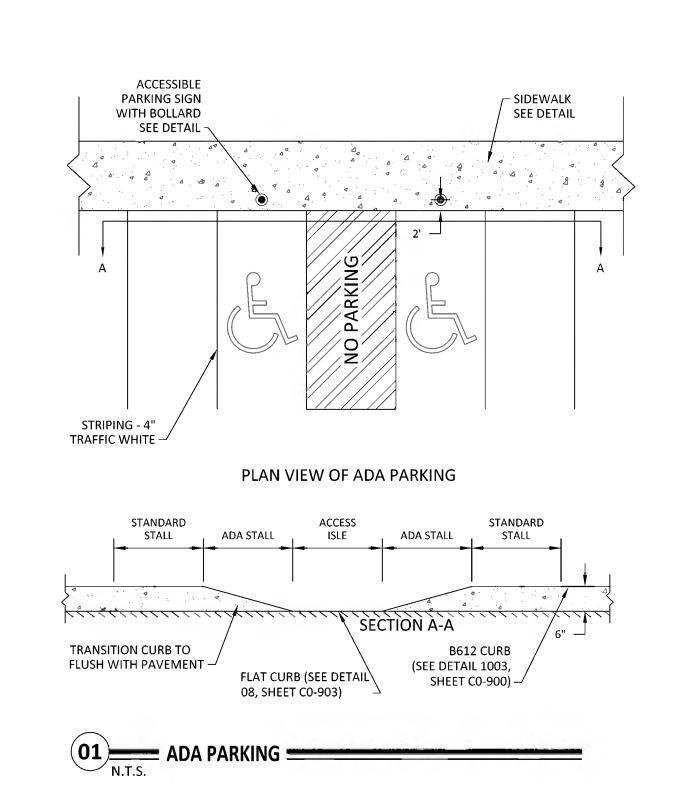
DATED: 02/23/2023

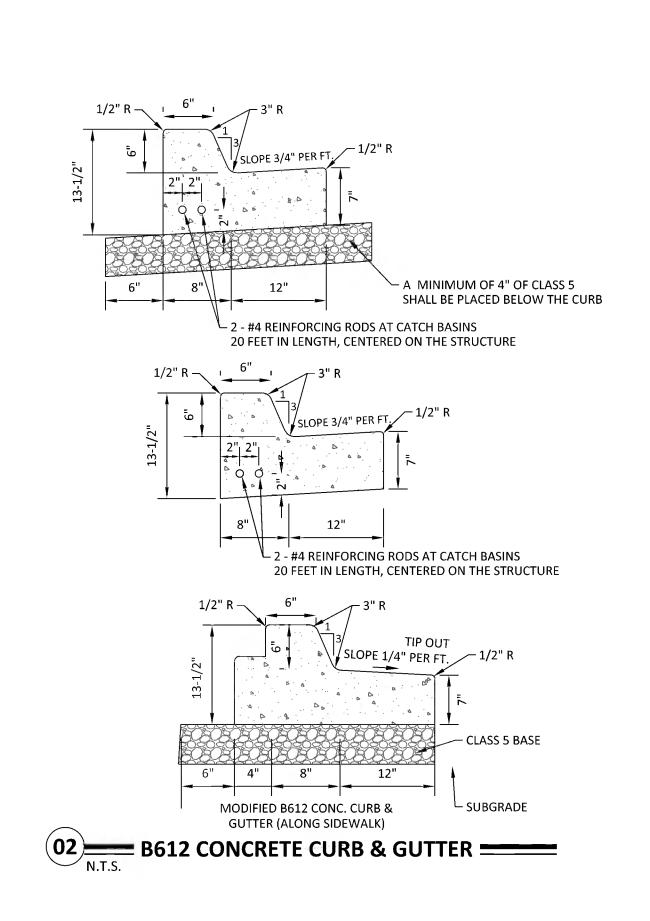
CONTRACTOR SHALL OBTAIN A COPY OF THIS SOILS REPORT.

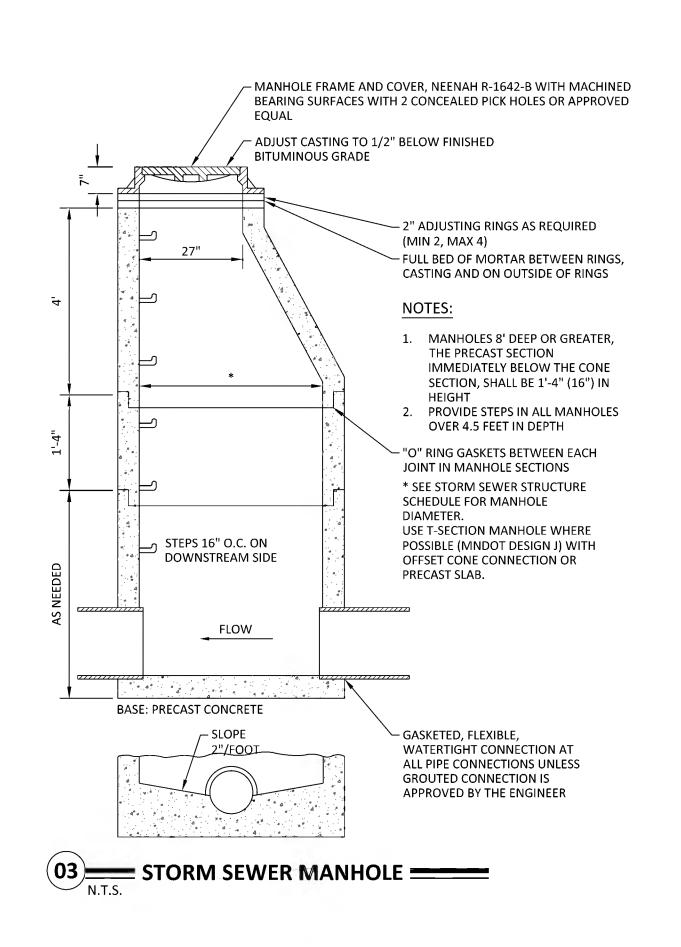
- 10. CONTRACTOR SHALL SUBMIT 2 COPIES OF SHOP DRAWINGS FOR MANHOLE AND CATCH BASIN STRUCTURES TO _______. CONTRACTOR SHALL ALLOW 5 WORKING DAYS FOR SHOP DRAWING REVIEW.
- 11. CONTRACTOR AND MATERIAL SUPPLIER SHALL DETERMINE THE MINIMUM DIAMETER REQUIRED FOR EACH STORM SEWER STRUCTURE. THE UNDERGROUND STORMWATER SYSTEM SHOWN ON THE UTILITY PLAN AND THE DETAIL SHEETS IS FOR INFORMATIONAL PURPOSES ONLY AND DEPICTS THE MINIMUM STORAGE REQUIREMENTS AND THE SYSTEM ELEVATIONS. THE CONTRACTOR (WITH THEIR SUPPLIER OR DESIGNER) SHALL SUBMIT DESIGN DRAWINGS TO THE ENGINEER FOR REVIEW AND APPROVAL PRIOR TO CONSTRUCTION. THE DESIGN DRAWINGS SHALL DEPICT THE FINAL LAYOUT AND DETAILS FOR CONSTRUCTION. THE DRAWINGS SHALL BE CERTIFIED BY A LICENSED ENGINEER FOR THE STATE IN WHICH THE PROJECT IS CONSTRUCTED. THE SUBMITTAL SHALL INCLUDE ALL NECESSARY PRODUCT INFORMATION, DESIGN CALCULATIONS AND BEDDING REQUIREMENTS FOR THE PROPOSED STORMWATER SYSTEM. FOLLOWING CONSTRUCTION, THE CERTIFYING ENGINEER SHALL SUBMIT A LETTER TO THE OWNER AND ENGINEER INDICATING THEY OBSERVED THE INSTALLATION AND THE INSTALLATION OF THE STORMWATER SYSTEM WAS IN CONFORMANCE WITH THE CERTIFIED DRAWINGS.

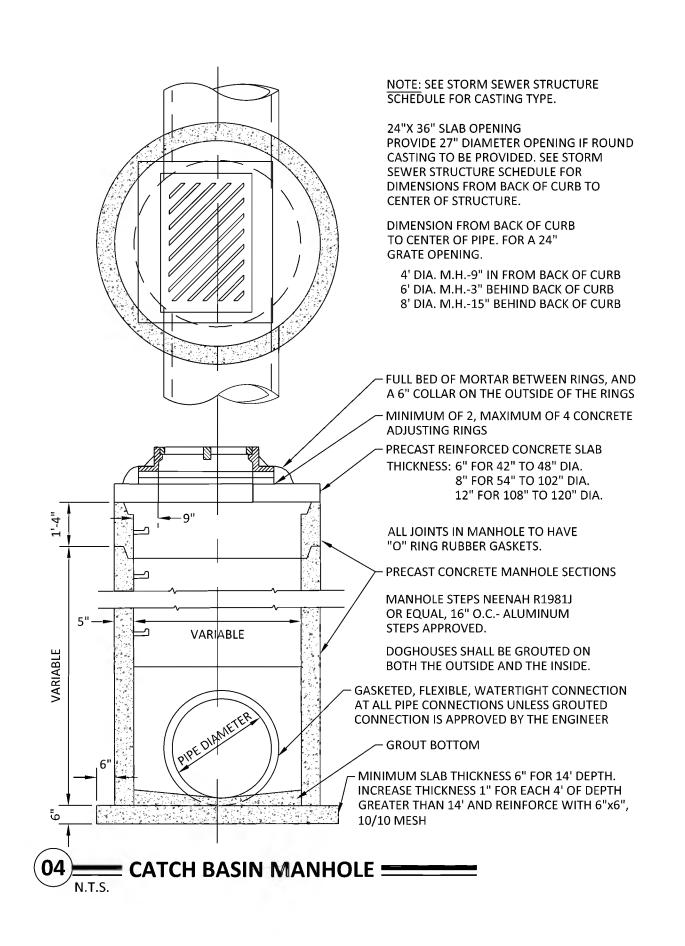
DATE BY CKD APPR COMMENT **UTILITY NOTES** hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and 02/24/2023 02/23/2023 | JMW | EJC | JB | Preliminary Site Plans that I am a duly Licensed Professional Engineer under C6.02 DESIGN REVIEW **DESIGNED BY** the laws of the State of Minnesota. **DORAN COMPANIES** MARSH RUN II REDEVELOPMENT PERMIT SUBMITTAL CHECKED BY PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN Engineering | Surveying | Planning | Environmenta CONSTRUCTION DOCUMENTS PROJECT NO. 🕽 2021 Sambatek 51414

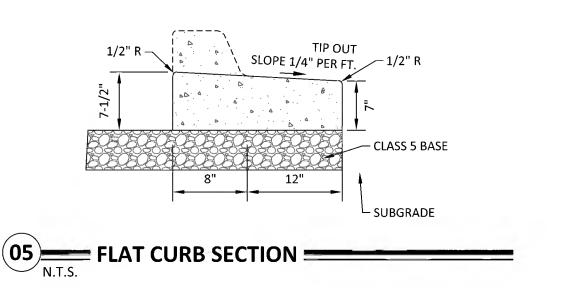
ECH) | JOSEPH BAILEY | 2/27/2023 10:25:17 AM \51414\CAD\SHEETS\51414-C6-UTIL.DWG:C6.02 UTILITY NOTES

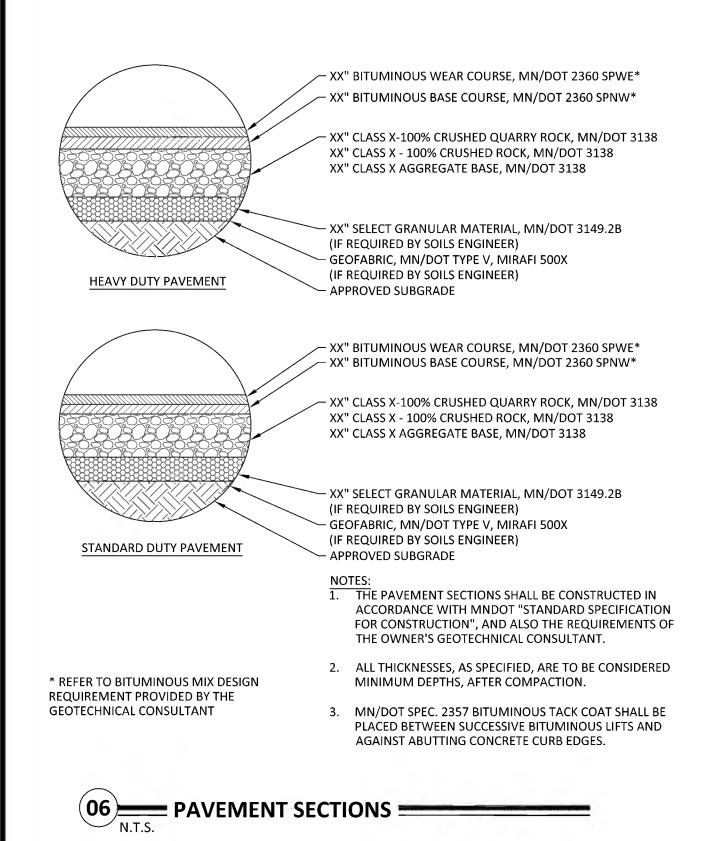


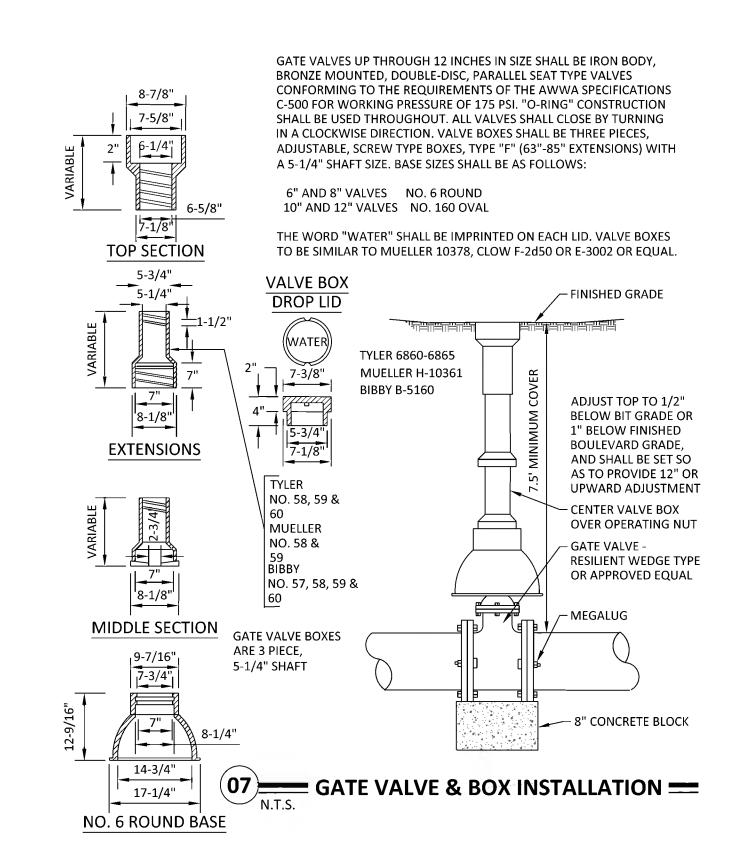


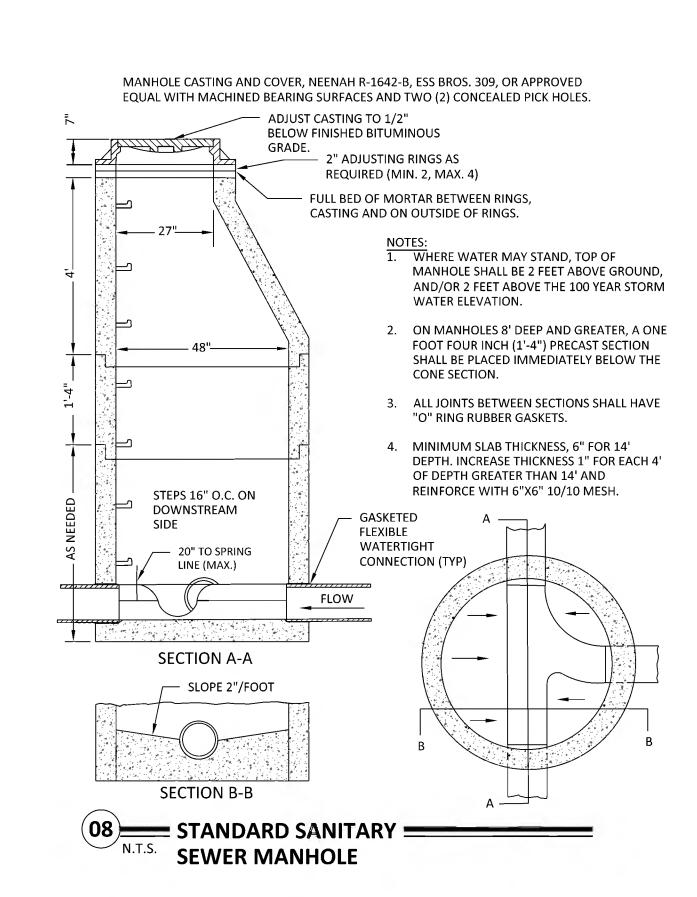


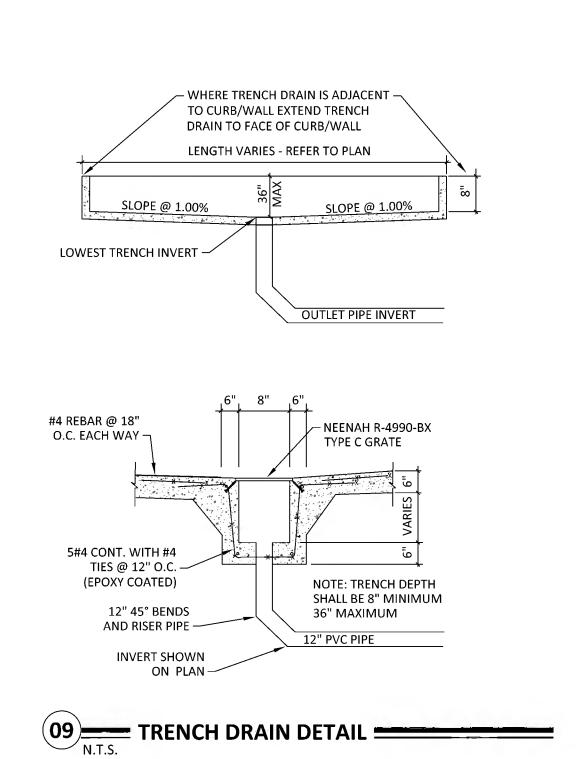




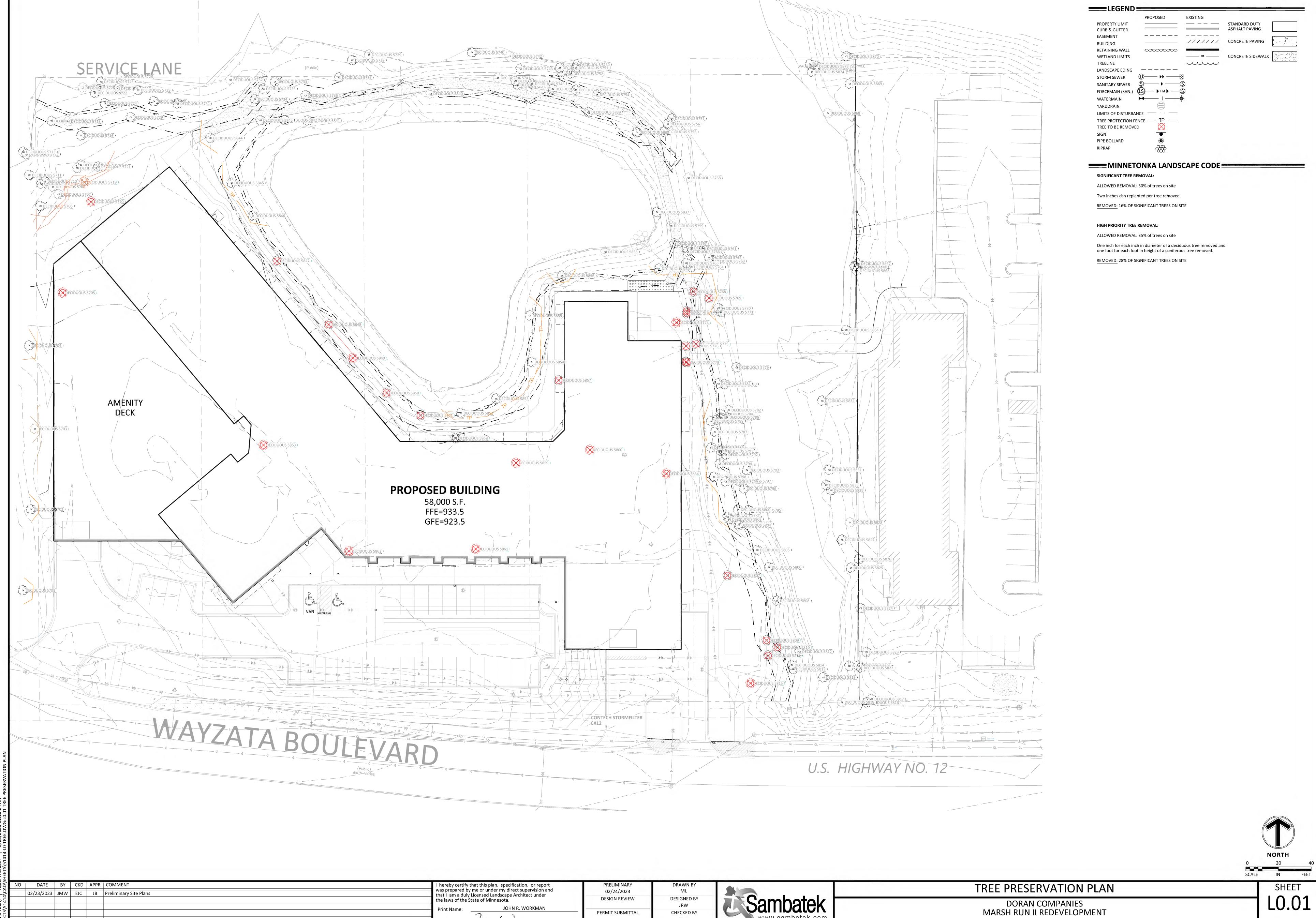








| NO DATE BY CKD APPR COMMENT 02/23/2023 JMW EJC JB Preliminary Site Plans | I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that Lam a duly licensed Professional Engineer under | PRELIMINARY 02/24/2023 | DRAWN BY JMW | | DETAILS | SHEET |
|---|--|--------------------------------|------------------------------|--|--|-------|
| S/2141/2 S/2141/2 | the laws of the State of Minnesota. Print Name: JOSEPH BAILEY | DESIGN REVIEW PERMIT SUBMITTAL | DESIGNED BY EJC CHECKED BY | Sambatek | DORAN COMPANIES MARSH RUN II REDEVELOPMENT | C9.01 |
| PROJECT | Jayen Bailey | CONSTRUCTION DOCUMENTS | JB PROJECT NO. | www.sambatek.com Engineering Surveying Planning Environmental | PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN | DEM |
| Tide © 2021 Sambatek | Date | | 51414 | | IVIIININEO I INKA, IVIIN | REV. |



JRW

CHECKED BY

JRW

PROJECT NO. 51414

Engineering | Surveying | Planning | Environmental

PERMIT SUBMITTAL

CONSTRUCTION DOCUMENTS

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PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN

| A-Tag | DBH | B-Species | Status |
|--------------|-----|--|--------------------|
| 5701 | 12 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 702 | 16 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5703 | 16 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5704 | 20 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5705 | 23 | Green Ash (Fraxinus pennsylvaica) | Remove |
| 5706 | 7 | Box Elder (Acer negundo) | Preserve |
| 5707 | 29 | Eastern Cottonwood (Populus deltoides) Eastern Cottonwood (Populus deltoides) | Preserve |
| 5708 | 13 | Box Elder (Acer negundo) | Preserve |
| 5709 | 4 | Box Elder (Acer negundo) | Preserve |
| 5710 5711 | 8 | Box Elder (Acer negundo) | Preserve |
| 5712 | 44 | Black Willow (Salix nigra) | Preserve |
| 5713 | 5 | Box Elder (Acer negundo) | Preserve |
| 5714 | 9 | Box Elder (Acer negundo) | Preserve |
| 5715 | 11 | Box Elder (Acer negundo) | Preserve |
| 5716 | 23 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5717 | 17 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5718 | 13 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5719 | 31 | Eastern Cottonwood (Populus deltoides) | Remove |
| 5720 | 4 | Eastern Cottonwood (Populus deltoides) | Remove |
| 5721 | 4 | Box Elder (Acer negundo) | Preserve |
| 5722 | 5 | Box Elder (Acer negundo) | Preserve |
| 5723 | 9 | Box Elder (Acer negundo) | Preserve |
| 5724 | 8 | Box Elder (Acer negundo) | Preserve |
| 5725 | 14 | Black Willow (Salix nigra) | Preserve |
| 5726 | 9 | Box Elder (Acer negundo) | Preserve |
| 5727 | 10 | Box Elder (Acer negundo) | Preserve |
| 5728 | 10 | Box Elder (Acer negundo) | Preserve |
| 5729 | 6 | Box Elder (Acer negundo) | Preserve |
| 5730 | 15 | Box Elder (Acer negundo) | Preserve |
| 5731 | 9 | Box Elder (Acer negundo) | Preserve |
| 5732 | 4 | Box Elder (Acer negundo) | Preserve |
| 5733 | 34 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5734 | 21 | Eastern Cottonwood (Populus deltoides) Eastern Cottonwood (Populus deltoides) | Preserve |
| 5735 | 16 | Black Willow (Salix nigra) | Preserve |
| 5736 5737 | 42 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5738 | 24 | Black Willow (Salix nigra) | Preserve |
| 5739 | 23 | Black Willow (Salix nigra) | Preserve |
| 5740 | 26 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5741 | 19 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5742 | 13 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5743 | 14 | Black Willow (Salix nigra) | Preserve |
| 5744 | 13 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5745 | 11 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5746 | 15 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5747 | 17 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5748 | 12 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5749 | 7 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5750 | 5 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5751 | 15 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5752 | 14 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5753 | 15 | Black Willow (Salix nigra) | Preserve |
| 5754 | 19 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 755 | 27 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 756 | 6 | American Elm (Ulmus americana) | Preserve |
| 5757 | 5 | American Elm (Ulmus americana) | Preserve |
| 5758 | 16 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5759 | 26 | Quaking Aspen (Populus tremuloides) | Preserve |
| 5760 | 25 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5761 | 11 | Box Elder (Acer negundo) | Preserve |
| 5762 | 8 | Box Elder (Acer negundo) | Preserve |
| 5763 | 9 | Box Elder (Acer negundo) Eastern Cottonwood (Populus deltoides) | Preserve |
| 5764 | 12 | Quaking Aspen (Populus tremuloides) | Preserve |
| 5765 | 15 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | Preserve |
| 5766 5767 | 5 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | Preserve |
| 5767 5768 | 23 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | Preserve Remove |
| 5769 | 12 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | Remove |
| 5769 5770 | 13 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | Preserve |
| 5770 5771 | 5 | Quaking Aspen (Populus tremuloides) Quaking Aspen (Populus tremuloides) | |
| 5772 | 4 | Box Elder (Acer negundo) | Preserve Remove |
| 5773 | 9 | Box Elder (Acer negundo) | Remove |
| 5774 | 12 | Box Elder (Acer negundo) | Remove |
| 5775 | 8 | Green Ash (Fraxinus pennsylvaica) | Remove |
| 5776 | 9 | Box Elder (Acer negundo) | Remove |
| | 8 | Box Elder (Acer negundo) | |
| 5777 | O | acr tropulary | Remove |

| 5779 | 8 | Box Elder (Acer negundo) | Preserve |
|--------------|--------|--|----------------------|
| 5780 | 33 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5781 | 5 | Box Elder (Acer negundo) | Preserve |
| 5782 | 5 | Box Elder (Acer negundo) | Preserve |
| 5783 | 6 | Box Elder (Acer negundo) | Preserve |
| 5784 | 10 | Black Willow (Salix nigra) | Preserve |
| 5785 | 4 | Box Elder (Acer negundo) | Preserve |
| 5786 | 26 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5787 | 8 | Box Elder (Acer negundo) | Preserve |
| 5788 | 25 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5789 5790 | 15 | Eastern Cottonwood (Populus deltoides) Eastern Cottonwood (Populus deltoides) | Preserve |
| 5791 | 9 | Box Elder (Acer negundo) | Preserve Preserve |
| 5792 | 23 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5793 | 4 | Box Elder (Acer negundo) | Preserve |
| 5794 | 28 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5795 | 5 | Box Elder (Acer negundo) | Preserve |
| 5796 | 5 | Box Elder (Acer negundo) | Preserve |
| 5797 | 41 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5798 | 6 | Siberian Elm (Ulmus pumila) | Preserve |
| 5799 | 20 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5800 | 5 | Box Elder (Acer negundo) | Preserve |
| 5801 | 6 | Box Elder (Acer negundo) | Preserve |
| 5802 | 5 | Box Elder (Acer negundo) | Preserve |
| 5803 | 8 | Box Elder (Acer negundo) Box Elder (Acer negundo) | Preserve |
| 5804 5805 | 11 | Box Elder (Acer negundo) | Preserve |
| 5806 | 5 | Box Elder (Acer negundo) | Preserve |
| 5807 | 19 | Green Ash (Fraxinus pennsylvaica) | Remove |
| 5808 | 22 | Box Elder (Acer negundo) | Preserve |
| 5809 | 8 | Green Ash (Fraxinus pennsylvaica) | Remove |
| 5810 | 4 | Box Elder (Acer negundo) | Remove |
| 5811 | 9 | Siberian Elm (Ulmus pumila) | Remove |
| 5812 | 34 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5813 | 4 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5814 | 10 | Box Elder (Acer negundo) | Preserve |
| 5815 | 5 | Box Elder (Acer negundo) | Remove |
| 5816 5817 | 5 | Green Ash (Fraxinus pennsylvaica) Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5818 | 5 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5819 | 4 | Box Elder (Acer negundo) | Preserve |
| 5820 | 6 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5821 | 8 | Siberian Elm (Ulmus pumila) | Preserve |
| 5822 | 22 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5823 | 32 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5824 | 14 | Box Elder (Acer negundo) | Preserve |
| 5825 | 8 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5826 | 9 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5827 | 8 | Green Ash (Fraxinus pennsylvaica) Box Elder (Acer negundo) | Preserve |
| 5828 5829 | 9 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5830 | 5 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5831 | 14 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5832 | 13 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5833 | 9 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5834 | 12 | River Birch (Betula nigra) | Remove |
| 5835 | 5 | Black Walnut (Juglans nigra) | Preserve |
| 5836 | 8 | Box Elder (Acer negundo) | Remove |
| 5837 | 6 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5838 | 13 | Quaking Aspen (Populus tremuloides) Box Elder (Acer negundo) | Preserve |
| 5839 | 14 | Box Elder (Acer negundo) | Preserve |
| 5840 5841 | 4 | Box Elder (Acer negundo) | Preserve |
| 5842 | 5 | Box Elder (Acer negundo) | Preserve |
| 5843 | 7 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5844 | 21 | Honey Locust (Gladitsia triacanthos) | Preserve |
| 5845 | 22 | Honey Locust (Gladitsia triacanthos) | Preserve |
| 5846 | 22 | Honey Locust (Gladitsia triacanthos) | Preserve |
| 5847 | 26 | Honey Locust (Gladitsia triacanthos) | Remove |
| 5848 | 28 | Honey Locust (Gladitsia triacanthos) | Remove |
| 5849 | 27 | Honey Locust (Gladitsia triacanthos) | Remove |
| 5850 | 23 | Honey Locust (Gladitsia triacanthos) | Remove |
| 5851 | 16 | Honey Locust (Gladitsia triacanthos) Honey Locust (Gladitsia triacanthos) | Remove |
| 5852 5853 | 23 | Honey Locust (Gladitsia triacanthos) | Preserve Preserve |
| 5854 | 21 | Honey Locust (Gladitsia triacanthos) | Preserve |
| 5855 | 19 | Honey Locust (Gladitsia triacanthos) | Preserve |
| | i I | Honov Locust (Gladitsia triasanthos) | |

Preserve

Preserve

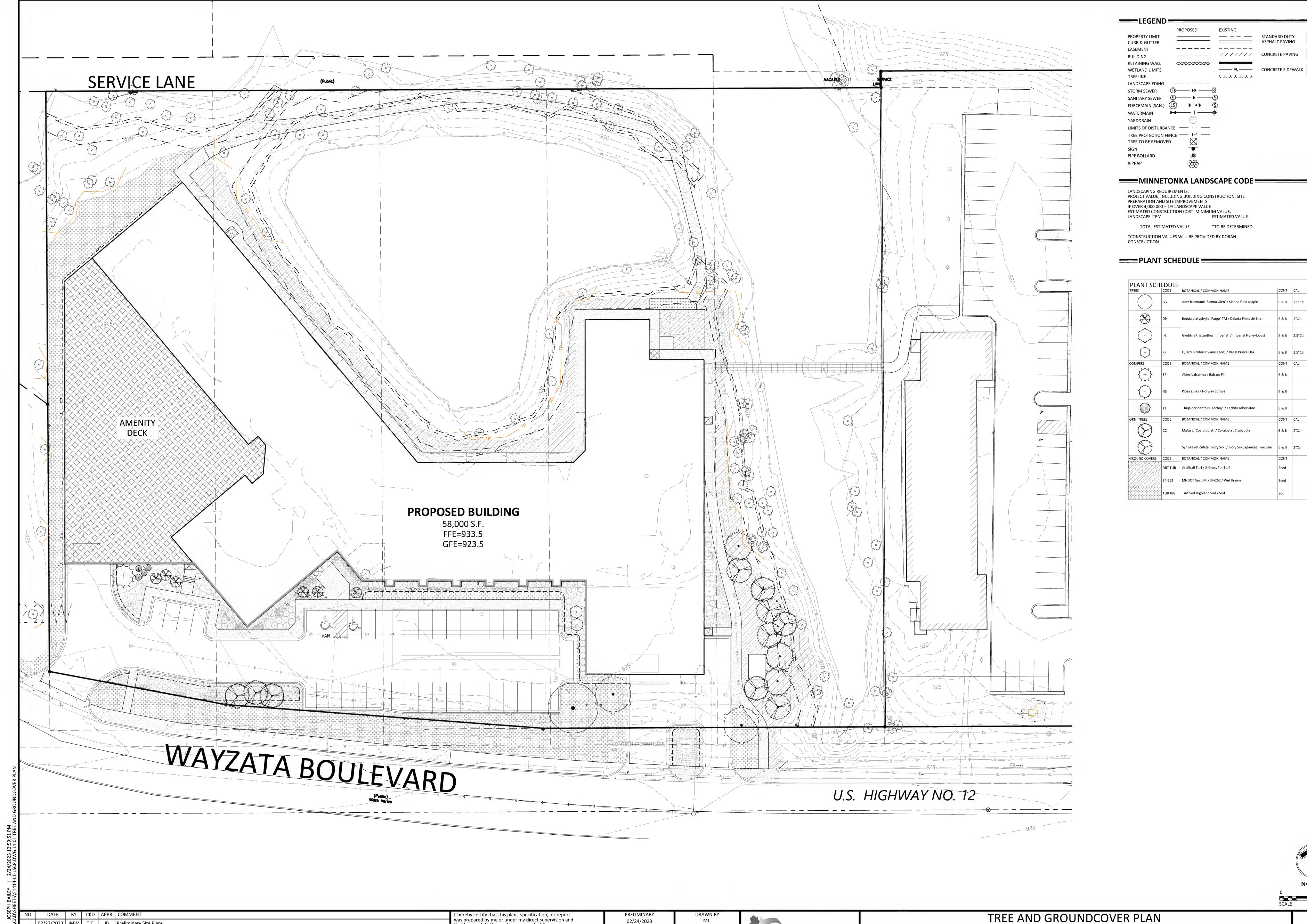
Remove

Honey Locust (Gladitsia triacanthos)

Paper Birch (Betula papyrifera)

| 5858 | 16 | River Birch (Betula nigra) | Remove |
|------|----|--|----------|
| 5859 | 8 | Paper Birch (Betula papyrifera) | Remove |
| 5860 | 11 | Paper Birch (Betula papyrifera) | Remove |
| 5861 | 12 | River Birch (Betula nigra) | Remove |
| 5862 | 28 | Green Ash (Fraxinus pennsylvaica) | Remove |
| 5863 | 22 | River Birch (Betula nigra) | Remove |
| 5864 | 7 | Box Elder (Acer negundo) | Preserve |
| 5865 | 36 | Eastern Cottonwood (Populus deltoides) | Preserve |
| 5866 | 8 | American Elm (Ulmus americana) | Preserve |
| 5867 | 6 | Box Elder (Acer negundo) | Preserve |
| 5868 | 7 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5869 | 10 | Box Elder (Acer negundo) | Preserve |
| 5870 | 18 | Box Elder (Acer negundo) | Preserve |
| 5871 | 14 | Box Elder (Acer negundo) | Preserve |
| 5872 | 6 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5873 | 7 | Green Ash (Fraxinus pennsylvaica) | Preserve |
| 5874 | 5 | Green Ash (Fraxinus pennsylvaica) | Preserve |

| SHEETS SH | | | | | | |
|--|---|---------------------------|----------------------|--|---|-------|
| NO DATE BY CKD APPR COMMENT 02/23/2023 JMW EJC JB Preliminary Site Plans | I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly licensed Landscape Architect under | PRELIMINARY 02/24/2023 | DRAWN BY ML | | TREE INVENTORY | SHEET |
| (\\21414\) | the laws of the State of Minnesota. Print Name: JOHN R. WORKMAN | DESIGN REVIEW | DESIGNED BY JRW | Sambatek | DORAN COMPANIES | L0.02 |
| O C C C C C C C C C C C C C C C C C C C | John () Joskman | PERMIT SUBMITTAL | CHECKED BY JRW | www.sambatek.com | MARSH RUN II REDEVELOPMENT PRELIMINARY SITE DEVELOPMENT PLANS | |
| ST № | Date 02/24/2023 License # 59119 | CONSTRUCTION DOCUMENTS | PROJECT NO. 51414 | Engineering Surveying Planning Environmental | MINNEOTNKA, MN | REV. |



I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly Licensed Landscape Architect under the laws of the State of Minnesota. 02/24/2023 **DESIGNED BY DESIGN REVIEW** JRW PERMIT SUBMITTAL CHECKED BY JRW CONSTRUCTION DOCUMENTS PROJECT NO.

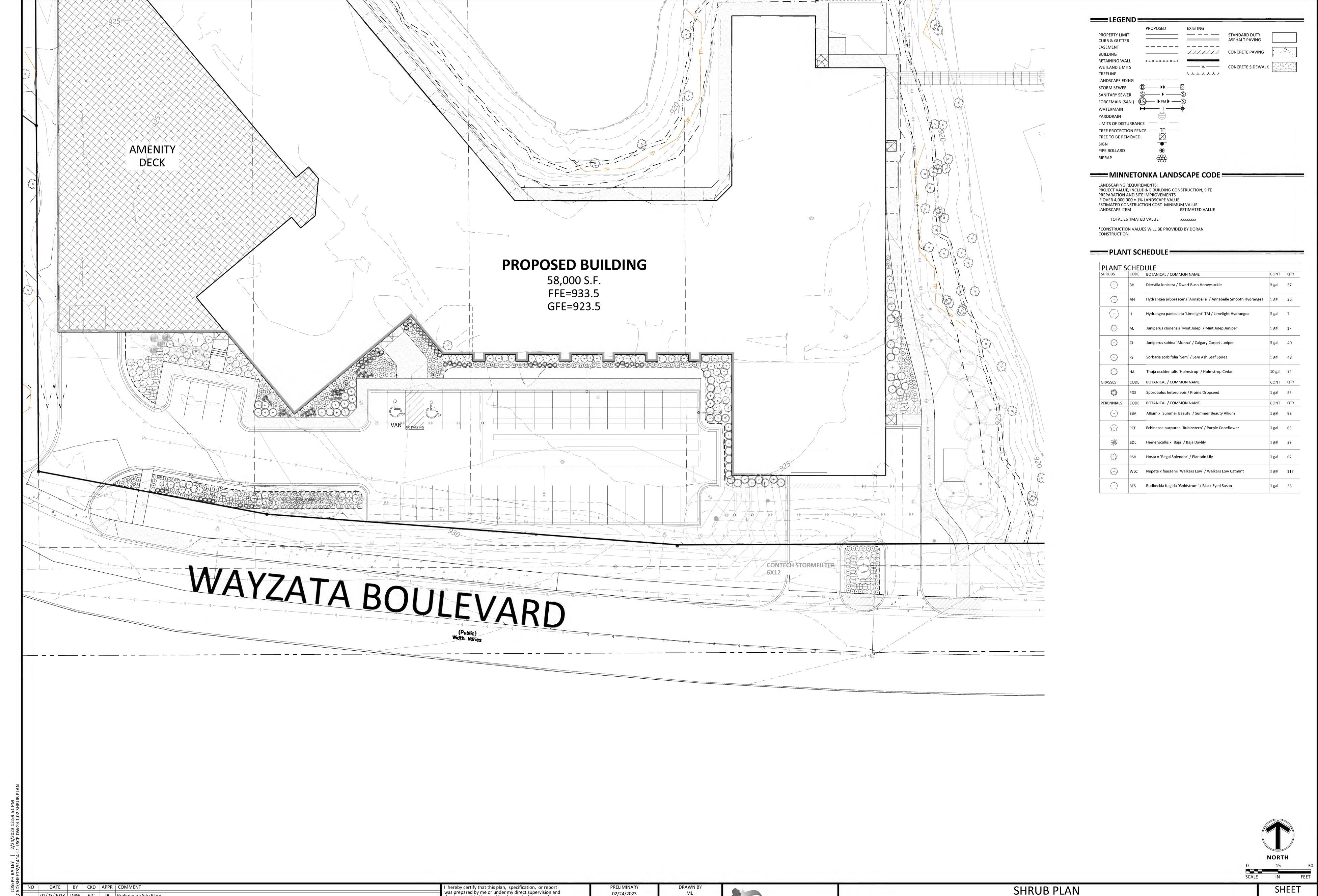
02/23/2023 JMW EJC JB Preliminary Site Plans

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51414

SHEET PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN



was prepared by me or under my direct supervision and

that I am a duly Licensed Landscape Architect under the laws of the State of Minnesota.

02/23/2023 | JMW | EJC | JB | Preliminary Site Plans

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02/24/2023

DESIGN REVIEW

PERMIT SUBMITTAL

CONSTRUCTION DOCUMENTS

DESIGNED BY

JRW

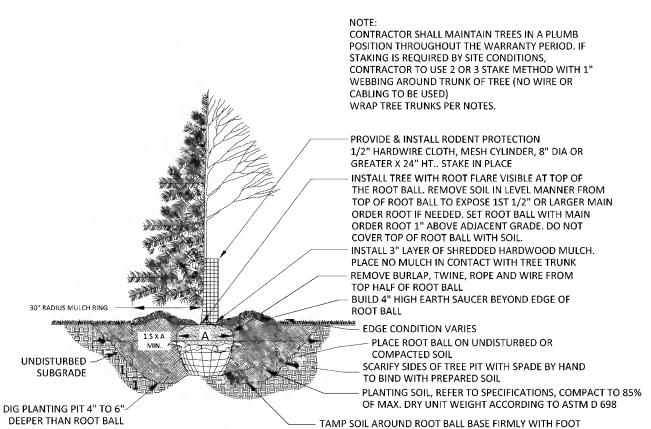
CHECKED BY

JRW

PROJECT NO. 51414

Engineering | Surveying | Planning | Environmental

DORAN COMPANIES MARSH RUN II REDEVELOPMENT PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN



PRESSURE SO THAT ROOT BALL DOES NOT SHIFT

PREPARE SOIL FOR - INSTALL 3" LAYER OF MULCH, DO NOT PLACE IN THE ENTIRE BED CONTACT W/ SHRUB STEM - APPLY PRE-EMERGENT HERBICIDE - EDGE CONDITION VARIES EDGER, REFER TO PLAN AND SPECIFICATION - LOOSEN ROOTS OF CONTAINER GROWN PLANTS - EXCAVATE PLANT BED MIN. 4" DEEPER THAN - SCARIFY SIDES AND BOTTOM OF PLANTING BED PLANTING SOIL. REFER TO SPECIFICATIONS UNDISTURBED SUBGRADE

P-02

P-04

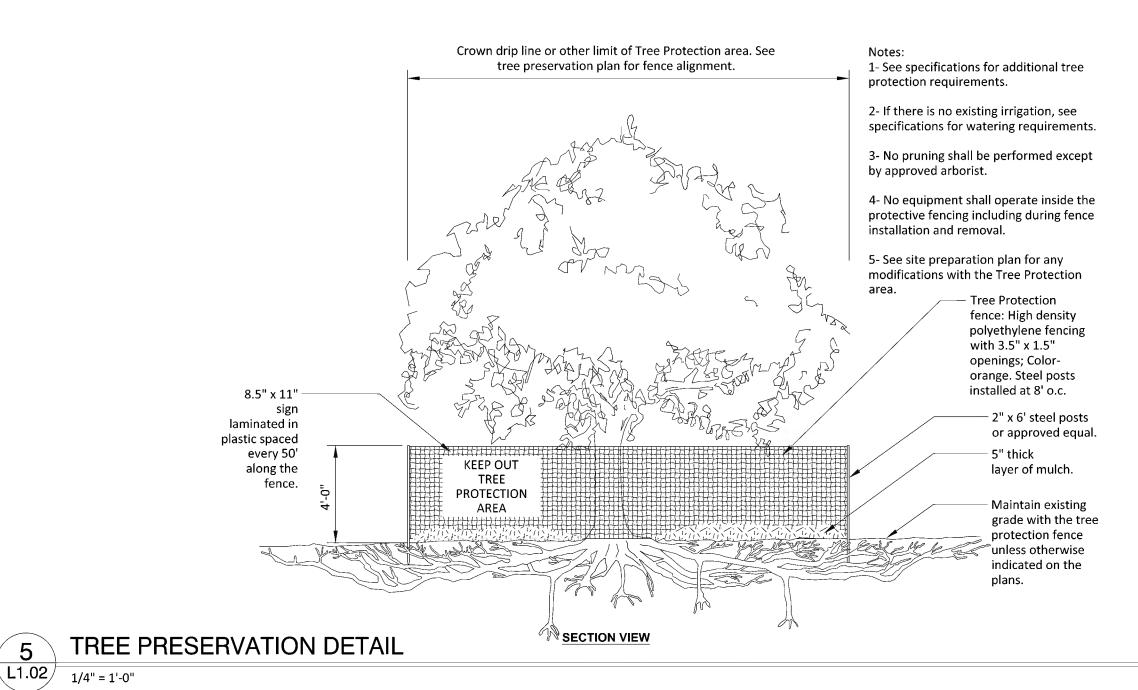
REFER TO EXTERIOR PLANTING SPECIFICATION PREPARE SOIL FOR THE ENTIRE BED - INSTALL 3" LAYER OF MULCH. DO NOT - EDGE CONDITION VARIES EDGER, REFER TO PLAN AND SPECIFICATION LOOSEN ROOTS OF CONTAINER GROWN PLANTS PLANTING SOIL, REFER TO SPECIFICATIONS

- UNDISTURBED SUBGRADE

- SCARIFY SIDES AND BOTTOM OF PLANTING BED WITH SPADE

MULCH/DECORATIVE ROCK PER PLAN AND LANDSCAPE NOTES $\frac{3}{6}$ " THICK STEEL EDGER (BLACK) W/ STAKE FINISHED GRADE AND EDGE CONDITION VARIES - SEE PLAN

PERENNIAL PLANTING DETAIL



DATE BY CKD APPR COMMENT hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and 02/23/2023 | JMW | EJC | JB | Preliminary Site Plans that I am a duly Licensed Landscape Architect under the laws of the State of Minnesota.) 2021 Sambatek

02/24/2023 **DESIGN REVIEW** PERMIT SUBMITTAL CONSTRUCTION DOCUMENTS **DESIGNED BY** JRW CHECKED BY JRW PROJECT NO.

51414

Engineering | Surveying | Planning | Environmenta

NOVEMBER 1), UNLESS OTHERWISE SPECIFIED. THE GUARANTEE SHALL COVER THE FULL COST OF NATIVE SEED MIX NOTES:

ESTABLISHMENT AND YEAR ONE: MOW THREE(3) TIMES FIRST YEAR ON 30-DAY INTERVALS TO A HEIGHT BETWEEN FIVE AND EIGHT INCHES. DO NOT USE FERTILIZERS. SPOT TREAT INVASIVE

WOODY PLANTS OR HAND WEED INDIVIDUAL NOXIOUS WEEDS. YEAR TWO: PERFORM ONE MOWING BETWEEN MID-JUNE AND MID-AUGUST. SPOT SPRAY

22. SEASONS/TIME OF PLANTING AND SEEDING: NOTE: THE CONTRACTOR MAY ELECT TO PLANT IN WEEDS AS NEEDED WHERE THEY ARE ESPECIALLY DOMINATE. 3. YEAR THREE (AND BEYOND): CUT ONE TIME PER YEAR AS A CLEAN UP PROCEDURE (EITHER IN EARLY MAY OR LATE NOVEMBER). PRESCRIBED BURNS MAY BE USED AS WELL IN PLACE OF

MOWING. CHECK LOCAL REGULATIONS AND PERMIT PROCEDURES.

21. CONTRACTOR SHALL NOTIFY THE LANDSCAPE ARCHITECT AT LEAST 3 DAYS PRIOR TO PLANNED DELIVERY. THE CONTRACTOR SHALL NOTIFY THE LANDSCAPE ARCHITECT AT LEAST 24 HOURS IN

22.6. NATIVE MIX SEEDING: 4/15 - 7/20; 9/20-10/20 23. MAINTENANCE SHALL BEGIN IMMEDIATELY AFTER EACH PORTION OF THE WORK IS IN PLACE. PLANT MATERIAL SHALL BE PROTECTED AND MAINTAINED UNTIL THE INSTALLATION OF THE PLANTS IS COMPLETE, INSPECTION HAS BEEN MADE, AND PLANTINGS ARE ACCEPTED EXCLUSIVE OF THE GUARANTEE. MAINTENANCE SHALL INCLUDE WATERING, CULTIVATING, MULCHING, REMOVAL OF DEAD MATERIALS, RE-SETTING PLANTS TO PROPER GRADE AND KEEPING PLANTS IN A PLUMB POSITION. AFTER ACCEPTANCE, THE OWNER SHALL ASSUME MAINTENANCE

RESPONSIBILITIES. HOWEVER, THE CONTRACTOR SHALL CONTINUE TO BE RESPONSIBLE FOR

4/1 - 6/1; 9/21 - 11/1

4/1 - 6/1; 9/21 - 11/1

4/1 - 6/1; 9/21-11/1

4/1 - 5/1; 9/21 - 11/1

4/1 - 6/1; 7/20 - 9/20

8. THE PLAN TAKES PRECEDENCE OVER THE LANDSCAPE LEGEND IF DISCREPANCIES EXIST. KEEPING THE TREES PLUMB THROUGHOUT THE GUARANTEE PERIOD. QUANTITIES SHOWN IN THE PLANTING SCHEDULE ARE FOR THE CONTRACTOR'S CONVENIENCE. 24. ANY PLANT MATERIAL WHICH DIES, TURNS BROWN, OR DEFOLIATES (PRIOR TO TOTAL ACCEPTANCE OF THE WORK) SHALL BE PROMPTLY REMOVED FROM THE SITE AND REPLACED WITH 9. THE SPECIFICATIONS TAKE PRECEDENCE OVER THE PLANTING NOTES AND GENERAL NOTES. MATERIAL OF THE SAME SPECIES, QUANTITY, AND SIZE AND MEETING ALL LANDSCAPE LEGEND

REPLACEMENT INCLUDING LABOR AND PLANTS.

ADVANCE OF BEGINNING PLANT INSTALLATION.

OFF-SEASONS ENTIRELY AT HIS/HER RISK.

22.1. POTTED PLANTS:

22.2. DECIDUOUS /B&B:

22.4. EVERGREEN B&B:

22.5. TURF/LAWN SEEDING:

22.3. EVERGREEN POTTED PLANTS:

10. EXISTING TREES AND SHRUBS TO REMAIN SHALL BE PROTECTED TO THE DRIP LINE FROM ALL SPECIFICATIONS. CONSTRUCTION TRAFFIC, STORAGE OF MATERIALS ETC. WITH 4' HT. ORANGE PLASTIC SAFETY 25. WATERING: MAINTAIN A WATERING SCHEDULE WHICH WILL THOROUGHLY WATER ALL PLANTS FENCING ADEQUATELY SUPPORTED BY STEEL FENCE POSTS 6' O.C. MAXIMUM SPACING. ONCE A WEEK. IN EXTREMELY HOT, DRY WEATHER, WATER MORE OFTEN AS REQUIRED BY INDICATIONS OF HEAT STRESS SUCH AS WILTING LEAVES. CHECK MOISTURE UNDER MULCH PRIOR TO WATERING TO DETERMINE NEED. CONTRACTOR SHALL MAKE THE NECESSARY

TURF NOTES:

ARRANGEMENTS FOR WATER.

TURF ESTABLISHMENT SHALL BE ACCOMPLISHED IN ACCORDANCE WITH THE PROVISIONS

MULCHING AND FERTILIZING. SEED MIXTURE NO.25-121 WILL BE PLACED AT THE RATE OF 65

6. ALL DISTURBED AREAS TO RECEIVE NATIVE SEED, ARE TO RECEIVE PLANTING SOIL, SEED, MULCH,

AND WATER UNTIL A HEALTHY STAND OF GRASS IS OBTAINED. FOR SLOPES STEEPER THAN 3:1 OR

COMPLETED IN THE IMMEDIATE AREA. OF THE MN/DOT 2105 AND 2575 EXCEPT AS MODIFIED BELOW: 2. A GRANULAR PRE-EMERGENT HERBICIDE SHALL BE APPLIED TO ALL PLANT BEDS AT THE 1. ALL AREAS TO RECEIVE SOD SHALL ALSO RECEIVE 6" OF TOPSOIL PRIOR TO MANUFACTURERS RECOMMENDED RATE PRIOR TO PLANT INSTALLATION. INSTALLING SOD. TOPSOIL SHALL BE FREE OF TREE ROOTS, STUMPS, BUILDING MATERIAL, 3. ALL PLANTING STOCK SHALL CONFORM TO THE "AMERICAN STANDARD FOR NURSERY STOCK," ANSI-Z60, LATEST EDITION, OF THE AMERICAN ASSOCIATION OF NURSERYMEN, INC. AND SHALL AND TRASH, AND SHALL BE FREE OF STONES LARGER THAN 1 1/2" INCHES IN ANY DIMENSION. CONSTITUTE MINIMUM QUALITY REQUIREMENTS FOR PLANT MATERIALS. 2. WHERE SOD ABUTS PAVED SURFACES, FINISHED GRADE OF SOD/SEED SHALL BE HELD 1" BELOW

SURFACE ELEVATION OF TRAIL, SLAB, CURB, ETC. 5. ALL PLANTS MUST BE HEALTHY, VIGOROUS MATERIAL, FREE OF PESTS AND DISEASE AND BE . SOD SHALL BE LAID PARALLEL TO THE CONTOURS AND SHALL HAVE STAGGERED JOINTS. ON CONTAINER GROWN OR BALLED AND BURLAPPED AS INDICATED IN THE LANDSCAPE LEGEND. SLOPES STEEPER THAN 3:1 OR IN DRAINAGE SWALES, SOD SHALL BE STAKED SECURELY. 6. PLANT MATERIALS TO BE INSTALLED PER PLANTING DETAILS. TURF ON ALL OTHER AREAS DISTURBED BY CONSTRUCTION SHALL BE RESTORED BY SEEDING.

7. ALL TREES MUST BE STRAIGHT TRUNKED AND FULL HEADED AND MEET ALL REQUIREMENTS 8. THE LANDSCAPE ARCHITECT RESERVES THE RIGHT TO REJECT ANY PLANTS WHICH ARE DEEMED UNSATISFACTORY BEFORE, DURING, OR AFTER INSTALLATION.

4. OVERSTORY TREES SHALL BEGIN BRANCHING NO LOWER THAN 6' ABOVE PAVED SURFACES.

1. THE CONTRACTOR SHALL INSPECT THE SITE AND BECOME FAMILIAR WITH THE EXISTING

3. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE CODES,

5. LOCATE AND VERIFY ALL UTILITIES, INCLUDING IRRIGATION LINES, WITH THE OWNER FOR

THE LANDSCAPE ARCHITECT OF ANY CONFLICTS TO FACILITATE PLANT RELOCATION.

PLANTING INSTALLATION WITH OTHER CONTRACTORS WORKING ON SITE.

11. LONG-TERM STORAGE OF MATERIALS OR SUPPLIES ON-SITE WILL NOT BE ALLOWED.

1. NO PLANTS SHALL BE INSTALLED UNTIL FINAL GRADING AND CONSTRUCTION HAS BEEN

12. CONTRACTOR SHALL REQUEST IN WRITING, A FINAL ACCEPTANCE INSPECTION.

6. THE LANDSCAPE CONTRACTOR SHALL COORDINATE THE PHASES OF CONSTRUCTION AND

7. THE CONTRACTOR SHALL REVIEW THE SITE FOR DEFICIENCIES IN SITE CONDITIONS WHICH MIGHT

NEGATIVELY AFFECT PLANT ESTABLISHMENT. SURVIVAL OR WARRANTY. UNDESIRABLE SITE

CONDITIONS SHALL BE BROUGHT TO THE ATTENTION OF THE LANDSCAPE ARCHITECT PRIOR TO

2. THE CONTRACTOR SHALL VERIFY PLAN LAYOUT AND BRING TO THE ATTENTION OF THE LANDSCAPE

ARCHITECT DISCREPANCIES WHICH MAY COMPROMISE THE DESIGN OR INTENT OF THE LAYOUT.

4. THE CONTRACTOR SHALL PROTECT EXISTING ROADS, CURBS/GUTTERS, TRAILS, TREES, LAWNS AND

PROPRIETARY UTILITIES AND GOPHER STATE ONE CALL 48 HOURS BEFORE DIGGING. CONTRACTOR

SHALL BE RESPONSIBLE FOR THE PROTECTION AND REPAIR OF ANY DAMAGES TO SAME. NOTIFY

SITE ELEMENTS DURING CONSTRUCTION. DAMAGE TO SAME SHALL BE REPAIRED AND/OR

CONDITIONS RELATING TO THE NATURE AND SCOPE OF THE WORK.

REGULATIONS, AND PERMITS GOVERNING THE WORK.

REPLACED AT NO ADDITIONAL COST TO THE OWNER.

CONTRACTOR TO VERIFY QUANTITIES SHOWN ON THE PLAN.

GENERAL NOTES:

BEGINNING OF WORK

PLANTING NOTES:

9. NO SUBSTITUTIONS OF PLANT MATERIAL SHALL BE ACCEPTED UNLESS APPROVED IN WRITING BY THE LANDSCAPE ARCHITECT. 10. ALL PLANT MATERIAL QUANTITIES, SHAPES OF BEDS AND LOCATIONS SHOWN ARE APPROXIMATE. CONTRACTOR SHALL BE RESPONSIBLE FOR COMPLETE COVERAGE OF ALL PLANTING BEDS AT SPACING SHOWN AND ADJUSTED TO CONFORM TO THE EXACT CONDITIONS OF THE SITE. THE

LANDSCAPE ARCHITECT SHALL APPROVE THE STAKING LOCATION OF ALL PLANT MATERIALS PRIOR 11. ALL PLANTING AREAS MUST BE COMPLETELY MULCHED AS SPECIFIED. 12. MULCH: DOUBLE SHREDDED HARDWOOD MULCH, CLEAN AND FREE OF NOXIOUS WEEDS OR OTHER DELETERIOUS MATERIAL, IN ALL MASS PLANTING BEDS AND FOR TREES, UNLESS INDICATED AS ROCK MULCH ON DRAWINGS. SUBMIT SAMPLE TO LANDSCAPE ARCHITECT PRIOR TO DELIVERY

TREE RINGS, AND 3" FOR PERENNIAL/GROUND COVER BEDS, UNLESS OTHERWISE DIRECTED. 13. BUILDING MAINTENANCE STRIP: WHERE NO LANDSCAPE PLANTING BEDS EXIST ADJACENT TO A BUILDING FOUNDATION, CONTRACTOR SHALL INSTALL A DECORATIVE ROCK MAINTENANCE STRIP PER PLAN. DECORATIVE ROCK SHALL BE 1"-3" DRESSER TRAP ROCK, GREY IN COLOR. 14. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL MULCHES AND PLANTING SOIL QUANTITIES TO 4. ALL TREES SHALL HAVE SYMMETRICAL OR BALANCED BRANCHING ON ALL SIDES OF THE TREE. COMPLETE THE WORK SHOWN ON THE PLAN.

ON-SITE FOR APPROVAL. DELIVER MULCH ON DAY OF INSTALLATION. USE 3" FOR SHRUB BEDS,

AND FOR EVERGREENS MOVED ANYTIME. APPLY AS PER MANUFACTURER'S INSTRUCTION. ALL EVERGREENS SHALL BE SPRAYED IN THE LATE FALL FOR WINTER PROTECTION DURING WARRANTY

16. WRAP ALL SMOOTH-BARKED DECIDUOUS TREES PLANTED IN THE FALL PRIOR TO DECEMBER 1 AND REMOVE WRAPPING AFTER MAY 1. TREE WRAPPING MATERIAL SHALL BE WHITE TWO-WALLED PLASTIC SHEETING APPLIED FROM TRUNK FLARE TO THE FIRST BRANCH. 17. ALL DECIDUOUS, PINE, AND LARCH PLANTINGS SHALL RECEIVE RODENT PROTECTION PER MNDOT

18. PLANTING SOIL FOR TREES, SHRUBS AND GROUND COVERS: FERTILE FRIABLE LOAM CONTAINING A LIBERAL AMOUNT (4% MIN.) OF HUMUS AND CAPABLE OF SUSTAINING VIGOROUS PLANT GROWTH. IT SHALL COMPLY WITH MNDOT SPECIFICATION 3877 TYPE B SELECT TOPSOIL. MIXTURE SHALL BE FREE FROM HARDPACK SUBSOIL, STONES, CHEMICALS, NOXIOUS WEEDS, ETC. SOIL MIXTURE SHALL HAVE A PH BETWEEN 6.1 AND 7.5 AND 10-0-10 FERTILIZER AT THE RATE OF 3 POUNDS PER CUBIC YARD. IN PLANTING BEDS INCORPORATE THIS MIXTURE THROUGHOUT THE ENTIRE BED IN A 6" LAYER AND ROTO-TILLING IT INTO THE TOP 12" OF SOIL AT A 1:1 RATIO.ANY PLANT STOCK NOT PLANTED

MAINTAINED IN THIS MANNER WILL BE REJECTED. 19. CONTRACTOR SHALL BE RESPONSIBLE TO VERIFY THAT EACH EXCAVATED TREE AND SHRUB PIT WILL PERCOLATE PRIOR TO INSTALLING PLANTING MEDIUM AND PLANTS. THE CONTRACTOR SHALL FILL THE BOTTOM OF SELECTED HOLES WITH SIX INCHES OF WATER AND CONFIRM THAT THIS WATER WILL PERCOLATE WITHIN A 24-HOUR PERIOD. IF THE SOIL AT A GIVEN AREA DOES NOT DRAIN PROPERLY. A PVC DRAIN OR GRAVEL SUMP SHALL BE INSTALLED OR THE PLANTING

20. ALL PLANTS SHALL BE GUARANTEED FOR TWO COMPLETE GROWING SEASONS (APRIL 1

SHALL BE RELOCATED IF DIRECTED BY THE LANDSCAPE ARCHITECT.

ON DAY OF DELIVERY SHALL BE HEELED IN AND WATERED UNTIL INSTALLATION. PLANTS NOT

ALL DISTURBED AREAS TO BE TURF SEEDED, ARE TO RECEIVE 6" TOP SOIL, SEED, MULCH, AND WATER UNTIL A HEALTHY STAND OF GRASS IS OBTAINED. FOR SLOPES STEEPER THAN 3:1 OR IN DRAINAGE SWALES INSTALL EROSION CONTROL BLANKET.

IN DRAINAGE SWALES INSTALL EROSION CONTROL BLANKET.

GENERAL TREE SPECIFICATIONS: 1. ALL STREET AND PARKING LOT TREES SHALL BE LIMBED UP TO THE FOLLOWING HEIGHTS: 1.1. 2" CAL. TREES: LOWEST BRANCH 6' HT.

1.2. 3" CAL.+ TREES: LOWEST BRANCH 7' HT. TREE CANOPY WIDTH SHALL BE RELATIVE TO HEIGHT/CALIPER OF TREE AND TYPE OF TREE. 2.1. 1" CALIPER/6-8' HT: 3-4' WIDTH MIN. 2.2. 2" CALIPER/12-14' HT: 4-5' WIDTH MIN.

2.3. 3" CALIPER/14-16' HT: 6-7' WIDTH MIN. 3. CANOPY TREES SHALL NOT HAVE CO-DOMINATE LEADERS IN LOWER HALF OF TREE CROWN.

. TREES SHALL NOT BE TIPPED PRUNED. 15. USE ANTI-DESICCANT (WILTPRUF OR APPROVED EQUAL) ON DECIDUOUS PLANTS MOVED IN LEAF

6. TREES SHALL BE FREE OF PHYSICAL DAMAGE FROM SHIPPING AND HANDLING. DAMAGED TREES SHALL BE REJECTED.

7. SUMMER DUG TREES SHALL HAVE ROOTBALL SIZE INCREASED BY 20% 8. TREES WHICH EXCEED RECOMMENDED CALIPER TO HEIGHT RELATIONSHIP SHALL BE REJECTED.

IRRIGATION NOTES:

IRRIGATION SYSTEM TO BE DESIGN/BUILD. CONTRACTOR TO SUBMIT SHOP DRAWINGS FOR APPROVAL OF SYSTEM LAYOUT PRIOR TO INSTALLATION. 2. ALL SOD TO RECEIVE SPRAY OR ROTOR IRRIGATION HEADS WITH MINIMUM DESIGN OF 1"

IRRIGATION PER WEEK. ALL PLANT BEDS TO RECEIVE DRIP LINE IRRIGATION, WITH A MINIMUM DESIGN OF .25"

. CONTRACTOR TO INSTALL A TOTAL OF 4 QUICK COUPLERS AT THE CORNERS OF THE PROPERTY. A 2.5" TYPE K SOURCE PIPE IS PROVIDED BY MECHANICAL.

LOW MAINTENANCE FESCUE NOTES: DURING GROWING SEASON NEVER MOW SHORTER THAN 3.5 INCHES, PREFERRED MAINTENANCE

IS MOW ONCE PER MONTH AT 5" HEIGHT

DO NOT USE HIGH NITROGEN FERTILIZER ON FESCUE LAWN OVERSEED THIN, BARE SPOTS IN FALL 4. ALWAYS USE SHARP BLADE WHEN MOWING TO AVOID TEARING LEAF BLADE

5. SET MOWER TO 3" FOR BAGGING AND MOWING IN LATE FALL AFTER GROWING SEASON

LANDSCAPE DETAILS AND NOTES **DORAN COMPANIES** MARSH RUN II REDEVELOPMENT PRELIMINARY SITE DEVELOPMENT PLANS MINNEOTNKA, MN

SHEET

MARSH RUN II REDEVELOPMENT

SITE & BUILDING PLANS: FEBRUARY 24, 2023

Project Description

Doran is proposing a new, high-quality, Class A luxury apartment project that will be complimentary to the Birke, in the 394 Corridor regional area. This project is precisely what the City of Minnetonka is seeking the 2040 Comprehensive Plan for the 394 Corridor regional area. This project will add life and vitality to the north side of 394, enhancing walkability, providing an additional housing option for existing residents, attracting the next generation of residents to the City, and supporting the nearby commercial uses that exist in the neighborhood today. The project will contain an affordable housing component mixed with marketrate apartments to contribute to the City's need for attainable and affordable housing. The project will provide ample and convenient visitor parking, including 36 dedicated short term and visitor stalls located in a surface lot directly in front of the building's main entrance along Wayzata Boulevard. In addition, this project will add to the City's parks and trail system, with a pedestrian bridge and walking trail loop that preserve most of the site's significant trees and landscape features. This is a unique opportunity to redevelop a 4.33 acre blighted and underutilized site to create an exceptional project that will contribute to the City's goals for affordable housing, tree preservation, and the connection of parks and trails.

The redevelopment will include razing an existing office building on the site and constructing a 197-unit apartment project, with 10% of the units affordable to households earning 60% of the area median income levels, and 10% of the units affordable to households earning 80% of the area median income levels. The building will contain a mix of alcove, 1 bed, 2 bed, and 3 bed apartments with active gathering spaces for residents and guest located on the first and second levels of the building. The project will consist of a concrete podium parking garage with approximately 268 parking stalls on two levels—one level at grade along Wayzata Boulevard and a basement level that walks out to the North side of the site. The parking garage will contain all of the resident parking for the project, with an additional 36 surface parking spaces along Wayzata Boulevard near the main entrance for short-term guest and delivery parking. Above level one the building will be wood framed construction for the apartments and an open, elevated amenity deck will have several outdoor amenities. Amenities throughout the project will include: Business center; Flex work space; Clubroom and game room; entertainment suite with rooftop patio; Game simulator; Exercise facility; Group exercise room; Outdoor pool; Outdoor spa; Grilling stations; Outdoor fire pits; Pet spa; Heated underground parking; Bocce ball, and outdoor seating. The natural site features contribute to the City and the overall amenities, with a walking trail loop along the North wetlands, a sidewalk to Wayzata Boulevard, and a pedestrian bridge trail connection to the existing park trail to the Landings and retail center to the East.

This project has significant wetlands on the North and East Sides of the property that will remain to visually buffer the existing residential area to the North and East sides of the site. The proposed project "fits", both visually and in terms of use, massing and density, and it properly addresses the goals and concerns identified by the City and residential neighbors. For the building's exterior architecture, the project is thoughtfully designed around neighborhood characteristics and concept plan feedback. From the community and City feedback during the open house and sketch review process, the exterior design seeks to be contextual, timeless, and a unique contribution to the City of Minnetonka's architecture. To lower the visual scale of the building and relate to the more traditional architecture to the North, the overall mass is broken up and articulated into 5 distinct pieces with a base, middle, and top to the building form. Historical inspiration is made modern with traditional cornice, frames, and book ends translated into clean black lines, panelized forms, and black accents. To add to the existing sense of place, the material palate will compliment the existing retail center and the Birke apartment building with a mountain shadow velour brick base, white and earth tone lap siding, and black cementitious panels and windows. To clearly call out the building entrances, black brick is used at the vehicle and pedestrian entrances; and a copper canopy on the center black brick form clearly identifies the main visitor and pedestrian entrance to the building.

In summary, this project will significantly contribute to the City's goals and neighborhood's needs with: high quality & affordable housing; a meaningful contribution to the City's parks and trails system; preserved significant trees; ample & convenient visitor parking; and a contextual & timeless architecture that's unique to the City of Minnetonka.



Project Team

Owner/Developer: Doran RE Partners, LLC 7803 Glenroy Road

Bloomington, MN 55439 Ph: 952-288-2000

Architect:
Doran Architects, LLC 7803 Glenroy Road Bloomington, MN 55439 Ph: 952-288-2000

12800 Whitewater Drive Suite 300 Minneapolis, MN 55430 PH: 763-843-0420

<u>Landscape:</u>

Minneapolis, MN 55430 PH: 763-843-0420

Sambatek

12800 Whitewater Drive Suite 300

Doran Construction Company, LLC 7803 Glenroy Road Bloomington, MN 55439 Ph: 952-288-2000

Attorney:

Doran Companies Attn: Legal Department 7803 Glenroy Road Bloomington, MN 55439 Ph: 952-288-2000

Surveyor: Sambatek

12800 Whitewater Drive Suite 300 Minneapolis, MN 55430 PH: 763-843-0420

Unit, Bed, and Parking Count

| NITS | | |
|--|---|--|
| BED BED BED LCOVE TUDIO OTAL | 113 44 9 31 0 197 UNITS | |
| <u>EDS</u> | | |
| BED BED BED LCOVE | 113 88 27 31 | |

| STUDIO TOTAL | 0 259 BEDS | |
|--|---------------|---------------------------|
| PARKING | | |
| SURFACE STANDA SURFACE COMPA SURFACE ADA SURFACE TOTAL | CT | 34 0 <u>2</u> 36 |
| LEVEL P1 STANDA LEVEL P1 COMPAG LEVEL P1 ADA LEVEL P1 TOTAL | | 41 1 <u>3</u> 45 |
| LEVEL 1 STANDAR | | 15 5 |

TOTAL **304 PARKING SPACES**

Total SF Per Floor:

| 53,873 SF |
|-----------|
| 57,586 SF |
| 43,012 SF |
| 43,012 SF |
| 43,012 SF |
| 43,012 SF |
| 42,383 SF |
| |

GRAND TOTAL: 325,888 SF

Building Information:

Construction Type: 1A Podium IIIA Above Podium (w/ Automatic SprinklerSystem Per 2018 MNSBC Chapter 9)

| SHEET NUMBER | SHEET NAME |
|-----------------|-----------------------------|
| A 0.00 | TITLE SHEET |
| A 0.01 | EXISTING SITE PHOTOS |
| A 0.02 | CONTEXT SITE PLAN |
| A 0.03 | EXISTING SITE PLAN |
| A 0.04 | PROPOSED SITE PLAN |
| A 1.00 | LOWER LEVEL FLOOR PLAN |
| A 1.01 | LEVEL 1 FLOOR PLAN |
| A 1.02 | LEVEL 2 FLOOR PLAN |
| A 1.03 | LEVEL 3, 4, & 5 FLOOR PLAN |
| A 1.04 | LEVEL 6 FLOOR PLAN |
| A 2.00 | OVERALL BUILDING ELEVATIONS |
| A 2.01 | OVERALL BUILDING ELEVATIONS |
| A 3.00 | EXTERIOR RENDERING |
| A 3.01 | EXTERIOR RENDERING |
| A 3.02 | EXTERIOR RENDERING |
| A 3.03 | EXTERIOR RENDERING |
| A 3.04 | EXTERIOR RENDERING |
| A 4.00 | SHADOW STUDIES |
| | |
| C2.01 | EXISTING CONDITIONS |
| C3.01 | SITE PLAN |
| C3.02 | FIRE TRUCK TURNING MOVEMEN |
| C4.01 | GRADING PLAN |
| C4.02 | GRADING NOTES |
| C6.01 | UTILITY PLAN |
| C6.02 | UTILITY NOTES |
| C9.01 | DETAILS |
| L0.01 | TREE PRESERVATION PLAN |
| L0.02 | TREE INVENTORY |
| L1.01 | TREE AND GROUND COVER PLAN |
| L1.02 | SHRUB PLAN |
| L1.03 | LANDSCAPE DETAILS AND NOTES |
| | |
| | |

Sheet Index



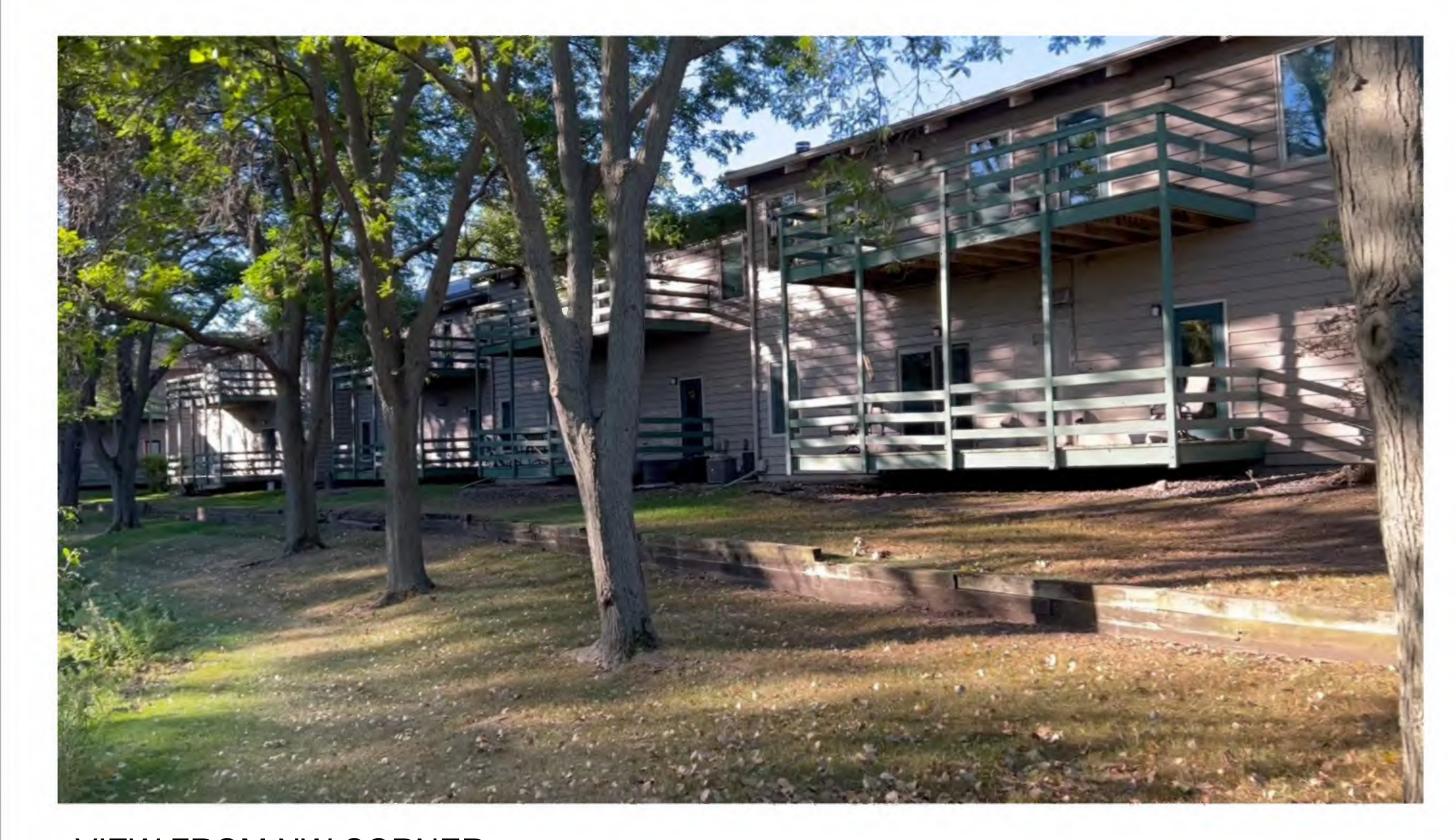
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STREET VIEW FROM SE CORNER

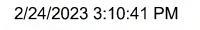




VIEW FROM NW CORNER

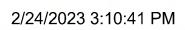


STREET VIEW FROM SW CORNER







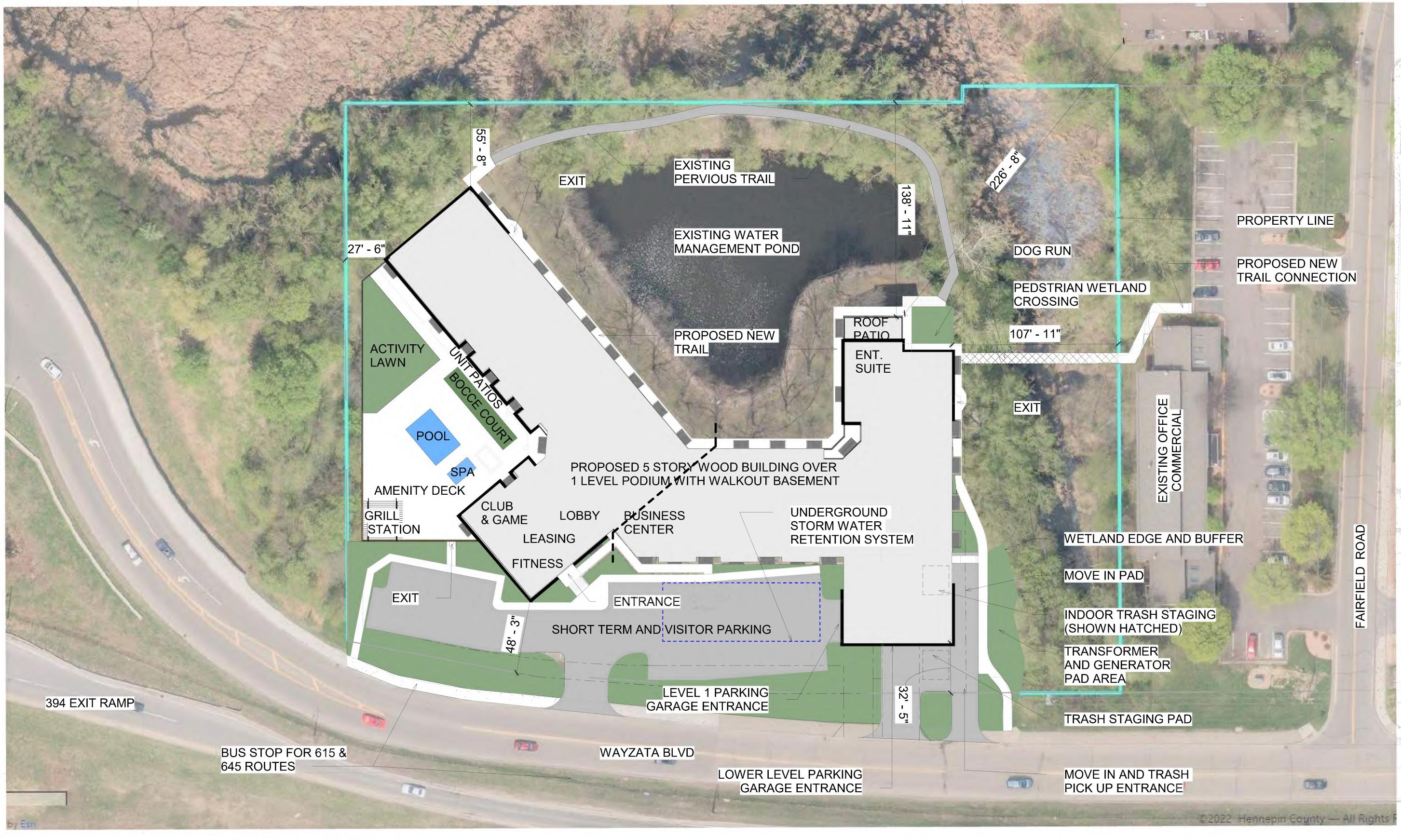


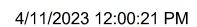




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MARSH RUN II REDEVELOPMENT

11816 Wayzata Blvd, Minnetonka

LOWER LEVEL FLOOR PLAN

A 1.00





MARSH RUN II REDEVELOPMENT

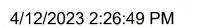
11816 Wayzata Blvd, Minnetonka

LEVEL 1 FLOOR PLAN

A 1.01

















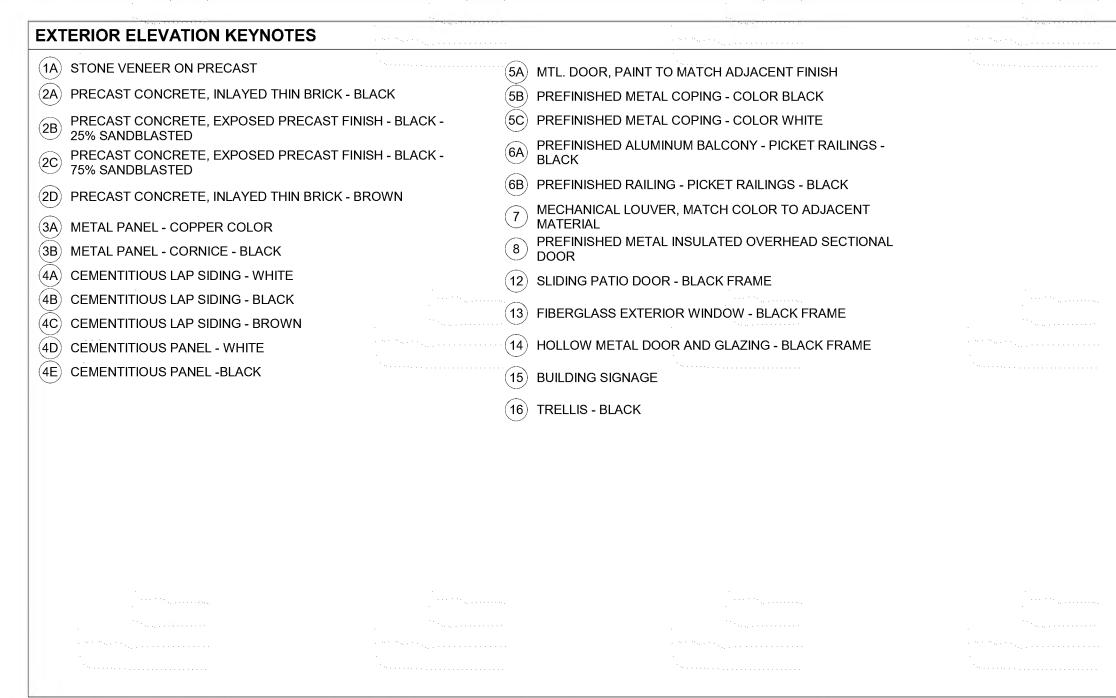














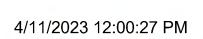




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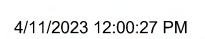




4/11/2023 12:00:27 PM









9 AM 3 PM 6 PM

























2/24/2023 3:11:02 PM





Memorandum

SRF No. 16579

To: Bria Raines, Planner

City of Minnetonka

From: Tom Sachi, PE, Project Manager

Eric Wurst, EIT, Traffic Engineer

Date: April 5, 2023

Subject: 11816 Wayzata Boulevard Traffic Summary Memorandum; Minnetonka, Minnesota

Introduction

As requested, SRF has completed a traffic study for the proposed residential development located in the City of Minnetonka. The proposed residential development is located along Wayzata Boulevard, at the site of the current Offices at Marsh Run. The following information provides a summary of the findings and recommendations offered for consideration.

Existing Conditions

Data Collection

Weekday a.m. and p.m. peak period vehicular turning movement and pedestrian/bicyclist counts were collected by SRF during the week of March 6, 2023, at the following study intersections:

- Ridgedale Drive and I-394 North On-Ramp
- Wayzata Boulevard and Fairfield Road
- Wayzata Boulevard and Market West Driveway
- Wayzata Boulevard and Market Center Driveway
- Wayzata Boulevard and Market East Driveway
- Hopkins Crossroad and Wayzata Boulevard
- Hopkins Crossroad and Fairfield Road

Proposed Development

The proposed residential development is located along Wayzata Boulevard, at the site of the existing Offices at Marsh Run, approximately 200 feet west of Fairfield Road. The existing 56,000 square foot (SF) office building located on the project site is proposed to be demolished. The proposed development is expected to construct 197 units of mid-rise multifamily housing, with 264 underground parking stalls and 40 surface parking stalls (304 total stalls). Access is expected to be provided at three (3) driveway locations along Wayzata Boulevard. A preliminary site plan for the proposed development can generally be seen in Picture 2 later in the summary. The development is anticipated to be constructed by year 2025.

Traffic Forecasts

Background Traffic Growth

To account for general background growth in the area, an annual growth rate of one-half (0.5) percent was applied to the existing peak hour traffic volumes to develop year 2025 background forecasts.

Proposed Development Trip Generation

To account for traffic impacts associated with the proposed development, a trip generation estimate for the proposed development was completed for the a.m. and p.m. peak hours and a daily basis. The estimate was developed using the *ITE Tr.p Generation Manual, 11th Edition*. Results of the trip generation estimate indicate that the proposed development is expected to generate approximately 73 a.m. peak hour, 77 p.m. peak hour, and 894 daily trips.

Intersection Capacity Analysis

An intersection capacity analysis was completed using Synchro/SimTraffic software for existing and future year 2025 build conditions. Results of the existing conditions capacity analysis indicate that all study intersections currently operate at an acceptable overall LOS B or better during the a.m. peak hour, and an acceptable overall LOS C or better during the p.m. peak hour, with the existing geometric layout and traffic controls. No significant delays or queuing issues at the study intersections were identified.

Results of the year 2025 build conditions analysis indicate that all study intersections are expected to continue to operate at an acceptable overall LOS B or better during the a.m. peak hour, and an acceptable overall LOS C or better during the p.m. peak hour, with the existing geometric layout and traffic controls. No significant delays or queuing issues were identified as part of the future analysis. Delays at the study intersections are expected to remain similar to existing conditions with increases of one (1) second or less as area development occurs (i.e., from background growth, adjacent development, and the proposed development).

Based on the year 2025 build conditions operations analysis, no geometric or traffic control changes are needed to accommodate the proposed development from an intersection capacity perspective.

Fairfield Road Traffic

Based on the trip and distribution estimates, there is a negligible amount of traffic during the a.m. peak hour and a potential that five (5) to 10 vehicles during the p.m. peak hour are using Fairfield Road as a "cut-through". This may equate to approximately 50 to 75 vehicles per day (vpd). Note, it is expected that a minimal amount of trips from the proposed development may utilize Fairfield Avenue, however, these would be local trips using the local roadway system and would not be defined as "cut -through".

Site Plan Review

A review of the proposed site plan was completed to identify any issues and recommend potential improvements for consideration with regard to sight distance, parking, access, circulation, and pedestrian facilities. In general, the following should be considered when designing internal traffic control:

- 1. Incorporate traffic controls, signing, and striping based on guidelines established in the *Manual on Un form Tre fic Control Devices* (MUTCD).
- 2. Special consideration should be made to limit any sight distance impacts from future structures, landscaping, and signing, particularly along Wayzata Boulevard.
- 3. Remove any tree and bush obstructions that prohibit sight distance, particularly for vehicles looking northwest along Wayzata Boulevard. With the rise in grade due to the on-ramp intersection, any additional tree cover can block the visibility of oncoming traffic.

Site Access Review

A detailed review of the proposed western site access was completed to determine if there is sufficient sight distance and gap times available along Wayzata Boulevard for vehicles to make safe maneuvering decisions. Based on AASHTO guidance, there is a desire for 280 to 335 feet of available intersection sight distance for a 25 to 30 mph roadway, respectively. Note, the roadway has a posted advisory travel speed of 25 mph, however, indications are that vehicles traveling along Wayzata Boulevard in the eastbound direction are traveling at higher speed.

A minimum of 155 to 200 feet is required for appropriate stopping sight distance for 25 to 30 mph travel speeds. This is the distance required for vehicles traveling along Wayzata Boulevard to ensure they can stop if a motorist entered the roadway. Lastly, in order to make safe left-turning maneuvers, AASHTO recommends vehicles exiting the proposed access points have a desired gap time of 7.5 seconds from when vehicles become visible on the main line to when they cross the proposed access location.

A detailed review of the proposed site access is shown below. Observations and gap times were collected at the proposed access location to understand if the proposed access location meets AASHTO guidance.



Picture 1 (left): Proposed Access Looking West

Available sight distance: Approximately 300 to 350 feet, depending on the height of the vehicle. Passenger cars can be partially obstructed by the guardrail.

Observed gap times: 6.75 seconds

Other notes: obstructions by vegetation would need to be removed. Drivers exiting the proposed access driveway must look to their right more than 90 degrees to observe oncoming vehicles due to the curvature of the roadway.

Given the inadequate gap time from when vehicles become visible to when they cross the proposed access, there is potential that vehicles on Wayzata Boulevard are traveling faster than 30 mph. With this observed information, the proposed access location may not be safe for exiting motorists from the proposed development who want to turn

left. While the available sight distance would be adequate for vehicles traveling at 25 mph on Wayzata Boulevard, if a low profile vehicle is traveling at 30 mph or faster, there is expected to be difficulty for vehicles at the proposed access to see oncoming traffic. Note, while the intersection sight distance may be inadequate, the stopping sight distance is expected to be sufficient for vehicles, meaning vehicles on Wayzata boulevard would be expected to be able to stop in time to prevent a crash.

In order to mitigate the available gap issue, it is recommended to relocate the western access approximately 100 feet east (center of access to center of access) of the current/existing access driveway (approximately 150 feet east of the proposed driveway). By moving the access east, observed gaps were noted to be closer to 8 to 8.5 seconds and available sight distance is approximately 390 to 400 feet depending on vehicle height, which would be acceptable for a 35 mph roadway. See below in Pictures 2 and 3. Note, stopping sight distance for a 35 mph roadway is 250 feet while intersection sight distance is 390 feet indicating that the available sight distance is sufficient to meet design standards.





Picture 2 (top): Recommended Access Relocation shown on Site Plan

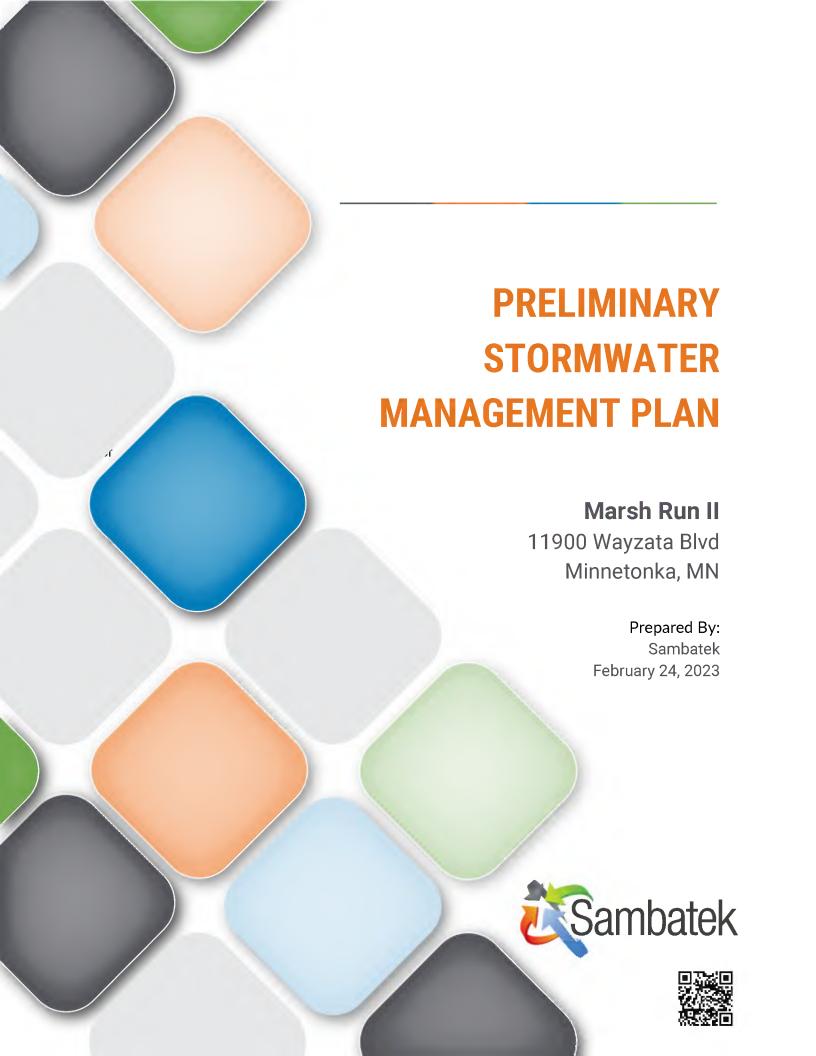
Picture 3 (bottom) Recommended Access Relocation shown on current aerial.

Summary and Conclusions

The following study conclusions and recommendations are offered for consideration:

- 1) Results of the existing intersection capacity analysis indicate that the study intersections currently all operate at an acceptable overall LOS B or better during the a.m. peak hour, and an acceptable overall LOS C or better during the p.m. peak hour, with the existing geometric layout and traffic controls. No significant side-street stop delays or queuing issues were identified with the existing geometric layout and traffic controls. No significant side-street delays or queueing issues were identified.
- 2) The proposed development consists of 197 units of mid-rise multifamily housing, with 264 underground parking stalls and 40 surface parking stalls (304 total stalls). The existing 56,000 square foot (SF) office building located on the project site is proposed to be demolished.
- 3) Access is expected to be provided at three (3) driveway locations along Wayzata Boulevard.
- 4) The proposed residential development is expected to generate approximately 73 a.m. peak hour, 77 p.m. peak hour, and 894 daily trips.
 - a. When compared to the ITE estimated expected trips for the existing office land use (assuming it is fully occupied), there is expected to be a decrease in the a.m. and p.m. peak hours of 12 and 4 site trips, respectively during the peak hours. There is expected to be an overall increase of 287 daily trips.
 - b. A comparison between the proposed development and the existing trips at the Offices at Marsh Run was completed and found that the proposed development is expected to have an increase of 49 a.m. peak hour and 52 p.m. peak hours trips as compared to today
- 5) Results of the year 2025 build capacity analyses indicate that all study intersections are expected to continue to operate at an acceptable overall LOS B or better during the a.m. peak hour, and an acceptable overall LOS C or better during the p.m. peak hour, with the existing geometric layout and traffic controls.
 - a. No significant delays or queuing issues were identified as part of the future analysis. Delays at the study intersections are expected to remain similar to existing conditions with increases of one (1) second or less as area development occurs.
 - b. No significant delays or queues are expected at the proposed access driveways along Wayzata Boulevard, with side-street delays expected to be less than 10 seconds during the a.m. and p.m. peak hours.
- 6) Based on the year 2025 build conditions operations analysis, no geometric or traffic control changes are needed to accommodate the proposed development from an intersection capacity perspective.

- 7) A review of peak hour traffic along Fairfield Road indicates that there is a negligible amount of traffic during the a.m. peak hour and a potential that five (5) to 10 vehicles during the p.m. peak hour are using Fairfield Road as a "cut-through". This may equate to approximately 50 to 75 vehicles per day (vpd). This is a decrease from year 2018 conditions. Note, a minimal amount of vehicles from the proposed development may utilize Fairfield Road, however, these are local trips using the local system and would not be "cut-through".
- 8) There is expected to be potential safety issues with the proposed western access location due to the length of available gaps from when vehicles become visible to when they cross the proposed access.
 - a. It is recommended to relocate the western access approximately 100 feet east (center of access to center of access) of the current/existing access driveway (approximately 150 feet east of the proposed driveway). By moving the access east, observed gaps were noted to be closer to 8 to 8.5 seconds and available sight distance is approximately 390 to 400 feet depending on vehicle height, which would be acceptable for a 35 mph roadway.



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Project Introduction

The Marsh Run II project is proposed by Doran Development, LLC and includes redevelopment of the existing Marsh Run Offices. The project site is located at 11900 Wayzata Boulevard in Minnetonka, Minnesota and is within the jurisdiction of the Bassett Creek Watershed Management Commission (BCWMC). The proposed redevelopment will result in the construction of one multifamily apartment complex with associated parking lots, sidewalks, and utility improvements. The Marsh Run II redevelopment will meet the stormwater design requirements of the City of Minnetonka, BCWMC, and MPCA through construction of a treatment train involving one underground detention facility and Manufactured Treatment Devices. The design requirements for the site are as follows:

- Rate control requirement: proposed nonlinear projects creating one of more acres of new and/or fully reconstructed impervious surfaces much manage stormwater runoff such that the peak flow rates leaving the site are equal to or less than the existing rate leaving the site for the 1-, 2-, 10-, and 100-year events based on Atlas 14 precipitation (City, Watershed)
- Volume control requirement: proposed nonlinear development/redevelopment projects which
 create one of more acres of new and/or fully reconstructed impervious surfaces shall capture
 and retain onsite 1.1 inches of runoff from new and/or fully reconstructed impervious surfaces
 (City, Watershed).
 - If the performance goal is not feasible and/or is not allowed, project proposer must implement flexible treatment options from the BCWMC Design Sequence Flow Chart and City's Stormwater Management Design Guidelines.
- Water quality requirements: for sites where the volume reduction goal is unfeasible, project proposers must utilize the Design Sequence Flow Chart to review Flexible Treatment Options (FTO) to satisfy water quality control (City, Watershed).
 - The site conditions for the proposed location result in FTO #2 applying to the site.
 - FTO #2 includes providing volume abstraction to the maximum extent practicable and providing 60% annual phosphorous removal from site runoff.
- Provide maintenance of wetland hydrology in accordance with wetland Manage 2 classification requirements.

Soil Classification

Boring logs were completed by Braun Intertec on October 17, 2022. These logs showed existing soils onsite consist of fill (SM, SC, CL) from elevations 0-11' below ground surface and lean clay (CL) from 7-54' below ground surface. These soils are hydrologic soil group (HSG) D and unsuitable for infiltration. Water was observed at elevations of 12-40' below ground surface. Please see the complete borings logs included in the appendices. A complete geotechnical evaluation will be completed along with the final plans.





Existing Conditions

The existing project area consists of three buildings, parking lots, and one existing wetland. Existing impervious onsite includes office buildings along with parking lots and sidewalks for a total of 1.54 acres of impervious surfaces. Ground cover consists of trees and grass surrounding the wetland. There are no existing stormwater management facilities onsite. There is one existing outlet control structure which conveys flow from the onsite wetland offsite to the north.

In existing conditions, the majority of site runoff flows into onsite storm sewers(1E) and directly into the existing wetland (2E). A portion of pervious runoff from the perimeter of the site flows offsite to a larger existing wetland (3E) located north of the site, and the remainder of the site discharges south to Wayzata Boulevard (4E).

A summary of the existing areas and curve numbers is outlined below. Please see the appendices for existing drainage maps and models.

| EXISTING AREAS & CORVE NOMBERS | | | | | |
|--------------------------------------|------|----|--|--|--|
| Subcatchment Area (acres) Pervious C | | | | | |
| 1E | 1.86 | 80 | | | |
| 2E | 1.19 | 79 | | | |
| 3E | 0.65 | 79 | | | |
| 4E | 0.20 | 80 | | | |

EXISTING AREAS & CURVE NUMBERS

Proposed Conditions

The proposed redevelopment project will disturb approximately 2.65 acres of the site and result in 0.43 acres of net new impervious surface. Stormwater management facilities proposed for the site include a treatment train with underground detention to provide rate control and a manufactured water quality treatment device to provide water quality treatment for the required abstraction volume. A second proprietary device will provide water quality treatment for one area of impervious runoff which bypasses the detention pipes. There is no volume abstraction proposed onsite due to site constraints such as HSG D soils and proximity to existing wetlands. The proposed treatment train will provide water quality treatment to an equivalent volume which would be abstracted given more favorable existing site conditions.

Runoff from the proposed building and the majority of the parking lot will be routed to the treatment train before ultimately discharging to the existing wetland onsite (1S). One garage ramp will route through a second proprietary device before discharging to the existing wetland (5S). The wetland will also receive a portion of direct runoff from the site area surrounding it (2S). The perimeter of the site will continue to discharge north (3S) to another wetland offsite in maintenance of existing drainage patterns. A portion of the front of the site will continue to discharge directly onto Wayzata Boulevard (4S) as in existing conditions.

A summary of the proposed areas and curve numbers is outlined below. Please see the appendices for existing drainage maps and models.

PROPOSED AREAS & CURVE NUMBERS

| Subcatchment | Area | Pervious CN |
|--------------|------|-------------|
| 1\$ | 1.83 | 80 |





| 2\$ | 1.09 | 80 |
|-----|------|----|
| 3\$ | 0.59 | 79 |
| 4\$ | 0.25 | 80 |
| 5S | 0.15 | 80 |

Rate Control

BCWMC requires proposed nonlinear projects creating one of more acres of fully reconstructed impervious surfaces much manage stormwater runoff such that the peak flow rates leaving the site are equal to or less than the existing rate leaving the site for the 2-, 10-, and 100-year events. The City of Minnetonka requires submittals show the existing and proposed 1-, 2-, 10-, and 100-year stormwater runoff volume and rate analysis. Runoff calculations were performed in HydroCAD using the Dynamic Storage Indicator method and MSE-3 distribution with Atlas 14 rainfall data for Hennepin County. Sub catchments with time of concentration greater than 7 minutes were calculated using sheet flow and shallow concentrated flow. Stormwater discharges from the proposed site to the north to an offsite wetland and south to Wayzata Boulevard. The results of runoff rate comparison and summarized in the tables below and detailed calculations can be found in the appendices.

DESIGN RAINFALL EVENTS

| Storm Event | (in) |
|-------------|------|
| 1-Year | 2.48 |
| 2-Year | 2.86 |
| 10-Year | 4.26 |
| 100-Year | 7.32 |

EXISTING MAXIMUM RATE OF RUNOFF (CFS)

| Storm Event | To Wayzata Blvd (node 4E) | To Onsite Wetland (node Wtld EXS inflow) | To Offsite Wetland (reach 1R) | Total Existing (reach 2R) |
|-------------|------------------------------|--|----------------------------------|---------------------------|
| 1-Year | 0.46 | 7.36 | 0.72 | <u>1.07</u> |
| 2-Year | 0.57 | 8.97 | 0.97 | <u>1.40</u> |
| 10-Year | 0.99 | 15.06 | 1.96 | 2.73 |
| 100-Year | 1.91 | 28.61 | 4.33 | <u>5.82</u> |

PROPOSED MAXIMUM RATE OF RUNOFF (CFS)

| Storm Event | To Wayzata | To Onsite Wetland | To Offsite Wetland | Total Existing |
|-------------|----------------|------------------------|--------------------|----------------|
| | Blvd (node 4S) | (node Wtld Prd inflow) | (reach 3R) | (reach 4R) |
| 1-Year | 0.45 | 2.64 | 0.59 | 0.84 |
| 2-Year | 0.58 | 3.26 | 0.79 | <u>1.11</u> |
| 10-Year | 1.09 | 11.92 | 1.58 | 2.19 |
| 100-Year | 2.22 | 30.24 | 3.45 | 4.74 |





Water Quality

Due to the presence of HSG D soils onsite and volume abstraction being infeasible, the Marsh Run II project utilizes alternate compliance to satisfy water quality requirements. The City of Minnetonka's Volume Retention Compliance Sequencing Approach requires new development and redevelopment projects provide for 60% Total Phosphorus (TP) removal and 90% Total Suspended Solids (TSS) removal. BCWMC utilizes a Flexible Treatment Option flowchart to determine the water quality requirements. The Marsh Run II site is restricted due to the presence of HSG D soils and proximity to the existing wetland which results in the classification of Flexible Treatment Option #2. FTO#2 requires providing 60% annual phosphorous removal from site runoff. Manufactured Treatment Devices (MTD) were selected to provide water quality control for the site given limited surface area and depth for media filtration or wet sedimentation. An MPCA-approved StormFilter was selected to provide 60% TP removal along with 85% TSS removal as stated in the Minnesota Stormwater Manual and will treat discharge from the detention pipes. An MPCA-approved Jellyfish was selected to provide 56% TP removal and 80% TSS removal as stated in the Minnesota Stormwater Manual and will treat runoff from the garage entrance. The MIDS Calculator was used to model the nutrient loads of the proposed site and the results of the model are summarized in the table below. Please see the appendices for the full MIDS printout.

NUTRIENT ANALYSIS

| ВМР | TSS Load (lb) | TP Load (lb) |
|-------------------------|---------------|--------------|
| Proposed Load Generated | 798.8 | 4.397 |
| Load Removed by BMPs | 716.2 | 2.780 |
| % Removed | 90 | 63 |

Pretreatment

Pretreatment prior to the subsurface detention pipes and StormFilter will be provided in the form of sump manholes. SHSAM was used to determine the required sump size given removal requirements and incorporated in the MIDS model.

| <u>Pretreatment</u> | | Standard Sumps A | | Are | a | 1.83 ac | |
|---------------------|-------------------------|------------------|--|-----------------|---------------------|---------------------|-------------------|
| Precipitati | recipitation Golden Val | | Golden Valley ('95-'07) Hydraulic Length | | 76 ft | | |
| PSD | PSD OK110-PSE | | OK110-PSD Average Slope | | 3.0% | | |
| Temperatu | ıre | St. Paul | Pervious CN | | 80 | | |
| Influent Co | onc. (mg/L) | 200 | 00 Impervious % | | 95% | | |
| Name | Model | Total Load (lbs) | Total Load Remo | Removal Efficie | n Model Height (ft) | Model Diameter (ft) | Pipe Diameter (in |
| StandardSumps | 42 | 22790 | 753 | 3.3 | 20 | 4.0 | 12 |
| StandardSumps | 44 | 22790 | 2186 | 9.6 | 4.0 | 4.0 | 15 |
| StandardSumps | 55 | 22790 | 4413 | 19.4 | 5.0 | 5.0 | 18 |





Volume Reduction

Due to the presence of HSG D soils onsite and volume abstraction being infeasible, the Marsh Run II project utilizes alternate compliance to satisfy volume reduction requirements. The City of Minnetonka's Volume Retention Compliance Sequencing Approach requires new development and redevelopment projects retain runoff to the maximum extent practicable. BCWMC's FTO#2 also requires providing volume abstraction to the maximum extent practicable.

Given limited surface area and proximity to an existing wetland, the chosen solution for the Marsh Run II project includes filtrating 1.1" of runoff over the project's new and disturbed impervious surfaces through an MPCA-approved Manufactured Treatment Device. Discharge from the MTD will flow into the existing wetland located north of the proposed building. Detailed calculations outlining the volume reduction requirements are outlined below. Further information may be found in the appendices.

Required Treatment Volume(
$$ft^3$$
) = V_{inf} = 1.1(in) * $\frac{1 ft}{12 in}$ * New Impervious Area (ft^2)
$$V_{inf}(ft^3) = 1.1(in) * \frac{1 ft}{12 in} * 86,261(ft^2) = 7,907 ft^3$$

VOLUME CONTROL ANALYSIS

| New Impervious Surface | 86,261 | sf |
|---------------------------------|--------|-----|
| Design Treatment Rainfall Event | 1.1 | in |
| Required Treatment Volume | 7,907 | cf |
| Required Drawdown Time | 48 | hrs |
| Provided Volume Below Outlet | 7,920 | cf |

Wetlands

The existing wetland located onsite is classified as Manage 2 per communication with the City of Minnetonka. Marsh Run II will provide the required limited impacts to wetland hydrology. The results of wetland hydrologic impacts are summarized below. Detailed calculations may be found in the HydroCad analysis of the appendices.

WETLAND BOUNCE ANALYSIS (FT)

| STORM | EXISTING | PROPOSED | CHANGE |
|----------|----------|----------|--------|
| 1-YEAR | 916.71 | 916.81 | 0.10 |
| 2-YEAR | 916.87 | 916.97 | 0.10 |
| 10-YEAR | 917.44 | 917.55 | 0.11 |
| 100-YEAR | 918.22 | 918.21 | 0.01 |

WETLAND INFLOW ANALYSIS (AC-FT)

| STORM | EXISTING | PROPOSED | CHANGE |
|----------|----------|----------|--------|
| 1-YEAR | 0.369 | 0.421 | 14% |
| 2-YEAR | 0.451 | 0.508 | 13% |
| 10-YEAR | 0.771 | 0.839 | 9% |
| 100-YEAR | 1.509 | 1.592 | 6% |





Wetland buffers are provided in accordance with BCWMC and the City of Minnetonka standards. BCWMC requires Manage 2 wetlands have an average buffer width of 25' and minimum width of 15', while the City of Minnetonka requires a 16.5' buffer. A summary of the buffer analysis is provided below. Please see the civil sheets for buffer delineation.

WETLAND BUFFER ANALYSIS

| WETLAND | REQUIRED (25' AVERAGE) (SF) | PROVIDED (SF) |
|---------|-----------------------------|---------------|
| ONSITE | 18,870 | 18,870 |
| OFFSITE | 14,832 | 14,877 |

Emergency Overflow

The grading design will convey overflow runoff through the site should a catch basin or pipe become plugged or if a rainfall event occurs that exceeds the design capacity of the storm sewer system. Overflow runoff will be routed offsite without impacting any neighboring structures. The high-water level of the underground detention system is 928.10 which provides greater than one foot of elevation separation between the HWL and the FFE of the proposed building.

Stormwater System Operations & Maintenance

An operations & maintenance agreement will be prepared for the project if required by the LGU.

Erosion & Sediment Control

A comprehensive Stormwater Pollution Prevention Plan (SWPPP) meeting the requirements of the MPCA NPDES permit will be developed as a part of the proposed plans.

Summary

The proposed Marsh Run II project will meet the requirements of the City of Minnetonka, BCWMC, and MPCA through construction of underground detention and filtration through one MTD. These BMPs will provide the required rate control, water quality, and volume reduction improvements prior to discharging stormwater runoff from the site to downstream receiving waters.

If you have any questions, comments, or additional information regarding this report, please contact me at JBailey@sambatek.com or 763.746.1606

Enclosures

Appendix A – Drainage Maps

Appendix B - Hydrocad Report

Appendix C - MIDS Model

Appendix D - Boring Logs

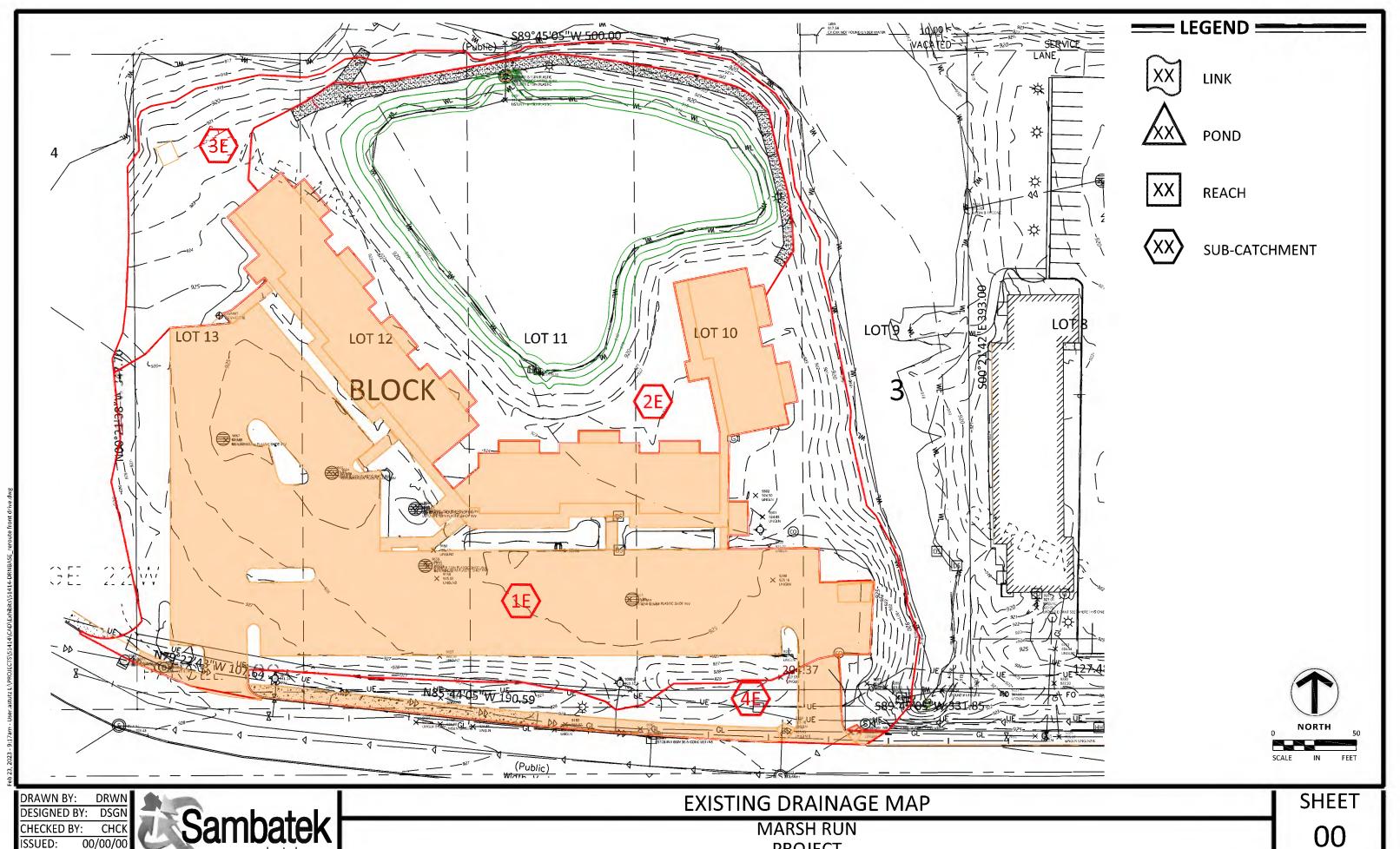




APPENDIX A - DRAINAGE MAPS





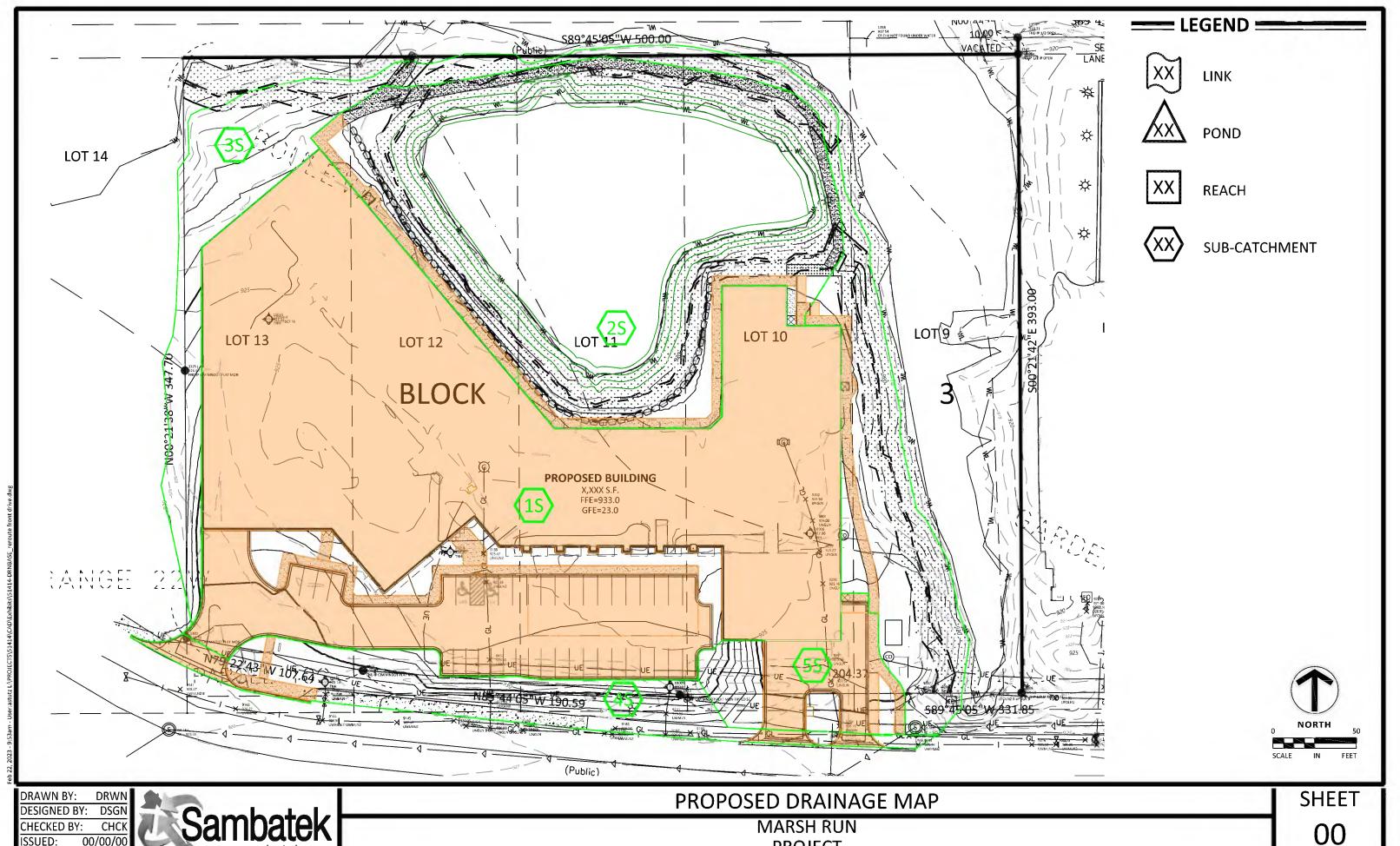


REVISION: REV DATE:

Engineering | Surveying | Planning | Environmental

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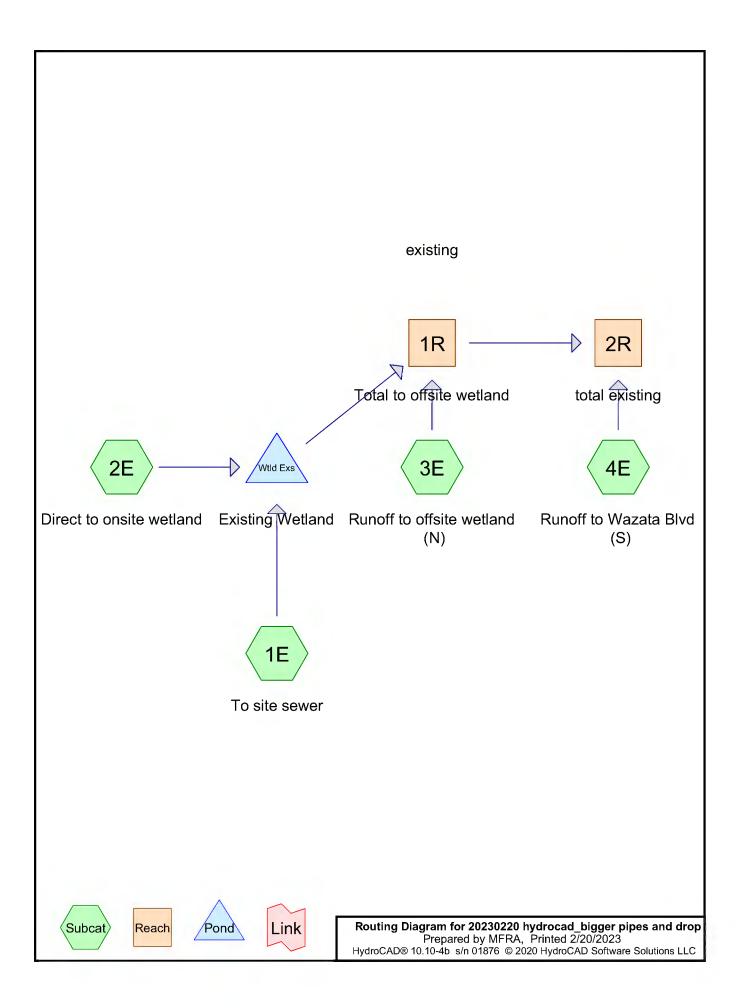
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APPENDIX B - HYDROCAD REPORT







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Project Notes

Rainfall events imported from "NRCS-Rain.txt" for 5327 MN Hennepin

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Rainfall Events Listing (selected events)

| Event# | Event | Storm Type | Curve | Mode | Duration | B/B | Depth | AMC |
|--------|----------|------------|-------|---------|----------|-----|----------|-----|
| | Name | | | | (hours) | | (inches) | |
| 1 | 1-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 2.48 | 2 |
| 2 | 2-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 2.86 | 2 |
| 3 | 10-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 4.26 | 2 |
| 4 | 100-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 7.32 | 2 |

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Area Listing (selected nodes)

| Are | a CN | Description |
|--------|------|---|
| (acres | 3) | (subcatchment-numbers) |
| 0.52 | 0 80 | >75% Grass cover, Good, HSG D (1E, 4E) |
| 1.54 | 2 98 | Paved parking, HSG D (1E, 4E) |
| 1.84 | 1 79 | Woods/grass comb., Good, HSG D (2E, 3E) |
| 3.90 | 2 87 | TOTAL AREA |

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Soil Listing (selected nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|-------------------------|
| 0.000 | HSG A | |
| 0.000 | HSG B | |
| 0.000 | HSG C | |
| 3.902 | HSG D | 1E, 2E, 3E, 4E |
| 0.000 | Other | |
| 3.902 | | TOTAL AREA |

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Ground Covers (selected nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|------------------|------------------|------------------|------------------|---------------|------------------|-------------------------|-------------------------|
| 0.000 | 0.000 | 0.000 | 0.520 | 0.000 | 0.520 | >75% Grass cover, Good | 1E, 4E |
| 0.000 | 0.000 | 0.000 | 1.542 | 0.000 | 1.542 | Paved parking | 1E, 4E |
| 0.000 | 0.000 | 0.000 | 1.841 | 0.000 | 1.841 | Woods/grass comb., Good | 2E, 3E |
| 0.000 | 0.000 | 0.000 | 3.902 | 0.000 | 3.902 | TOTAL AREA | |

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Pipe Listing (selected nodes)

| Li | ine# | Node | In-Invert | Out-Invert | Length | Slope | n | Width | Diam/Height | Inside-Fill |
|----|------|----------|-----------|------------|--------|---------|-------|----------|-------------|-------------|
| | | Number | (feet) | (feet) | (feet) | (ft/ft) | | (inches) | (inches) | (inches) |
| | 1 | Wtld Exs | 916.35 | 916.22 | 18.0 | 0.0072 | 0.010 | 0.0 | 15.0 | 0.0 |
| | 2 | Wtld Exs | 917.07 | 916.39 | 12.0 | 0.0567 | 0.010 | 0.0 | 15.0 | 0.0 |

MSE 24-hr 3 1-Year Rainfall=2.48" Printed 2/20/2023

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1E: To site sewer Runoff Area=80,945 sf 78.49% Impervious Runoff Depth=1.85"

Tc=7.0 min CN=94 Runoff=5.68 cfs 0.287 af

Subcatchment2E: Direct to onsite wetland Runoff Area=52,054 sf 0.00% Impervious Runoff Depth=0.82"

Tc=7.0 min CN=79 Runoff=1.69 cfs 0.082 af

Subcatchment3E: Runoff to offsite wetland Runoff Area=28,124 sf 0.00% Impervious Runoff Depth=0.82"

Flow Length=170' Slope=0.1000 '/' Tc=12.6 min CN=79 Runoff=0.72 cfs 0.044 af

Subcatchment4E: Runoff to Wazata Blvd Runoff Area=8,855 sf 40.99% Impervious Runoff Depth=1.29"

Tc=7.0 min CN=87 Runoff=0.46 cfs 0.022 af

Reach 1R: Total to offsite wetland Inflow=0.72 cfs 0.044 af

Outflow=0.72 cfs 0.044 af

Reach 2R: total existing Inflow=1.07 cfs 0.066 af

Outflow=1.07 cfs 0.066 af

Pond Wtld Exs: Existing Wetland Peak Elev=916.71' Storage=16,056 cf Inflow=7.36 cfs 0.369 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.902 ac Runoff Volume = 0.435 af Average Runoff Depth = 1.34" 60.49% Pervious = 2.360 ac 39.51% Impervious = 1.542 ac

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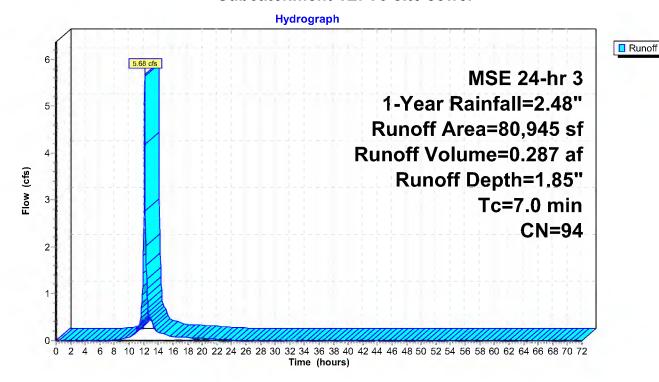
Summary for Subcatchment 1E: To site sewer

Runoff = 5.68 cfs @ 12.14 hrs, Volume= 0.287 af, Depth= 1.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| _ | Α | rea (sf) | CN | Description | | | |
|---|-------|----------|---------|--------------------------|-------------|---------------|--|
| | | 63,533 | 98 | Paved park | ing, HSG D |) | |
| _ | | 17,412 | 80 | >75% Gras | s cover, Go | ood, HSG D | |
| | | 80,945 | 94 | Weighted A | verage | | |
| | | 17,412 | | 21.51% Pei | rvious Area | 1 | |
| | | 63,533 | | 78.49% lm <mark>r</mark> | pervious Ar | ea | |
| | _ | | | | | | |
| | Tc | Length | Slope | _ | Capacity | Description | |
| _ | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | |
| | 7.0 | | | | | Direct Entry. | |

Subcatchment 1E: To site sewer



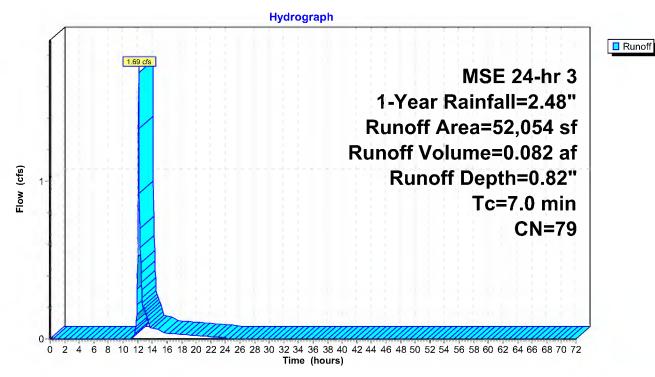
Summary for Subcatchment 2E: Direct to onsite wetland

Runoff = 1.69 cfs @ 12.15 hrs, Volume= 0.082 af, Depth= 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| A | rea (sf) | CN | Description | | |
|-------|----------|---------|-------------|-------------|---------------|
| | 0 | 98 | Paved park | ing, HSG D | D |
| | 52,054 | 79 | Woods/gras | s comb., C | Good, HSG D |
| | 52,054 | 79 | Weighted A | verage | |
| | 52,054 | | 100.00% Pe | ervious Are | ea |
| _ | | | | | |
| Tc | Length | Slope | • | Capacity | Description |
| (min) | (feet) | (ft/ft) |) (ft/sec) | (cfs) | |
| 7.0 | - | | - | | Direct Entry, |

Subcatchment 2E: Direct to onsite wetland



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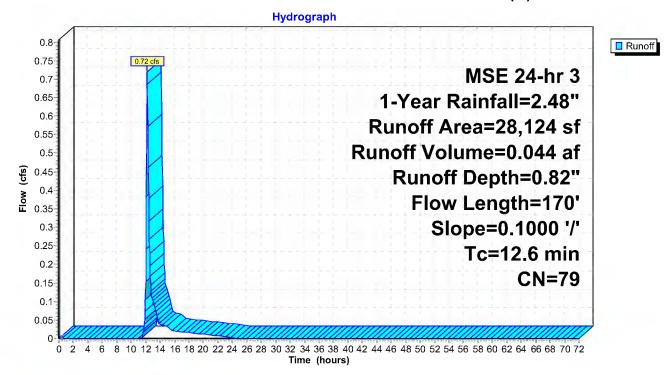
Summary for Subcatchment 3E: Runoff to offsite wetland (N)

Runoff = 0.72 cfs @ 12.22 hrs, Volume= 0.044 af, Depth= 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | Area (sf) | CN | Description | | | | | |
|------------|-----------|---------------------------|-------------|-------------------|--|--|--|--|
| | 0 | 0 98 Paved parking, HSG D | | | | | | |
| | 28,124 | 79 | Woods/gras | ss comb., C | Good, HSG D | | | |
| | 28,124 | 79 | Weighted A | verage | | | | |
| | 28,124 | | 100.00% P | ervious Are | a | | | |
| To (min | | Slope (ft/ft) | • | Capacity (cfs) | Description | | | |
| 11.9 | 9 100 | 0.1000 | 0.14 | | Sheet Flow, | | | |
| 0. | 7 70 | 0.1000 | 1.58 | | Woods: Light underbrush n= 0.400 P2= 2.86" Shallow Concentrated Flow, Woodland Kv= 5.0 fps | | | |
| 12.0 | 3 170 | Total | | | | | | |

Subcatchment 3E: Runoff to offsite wetland (N)



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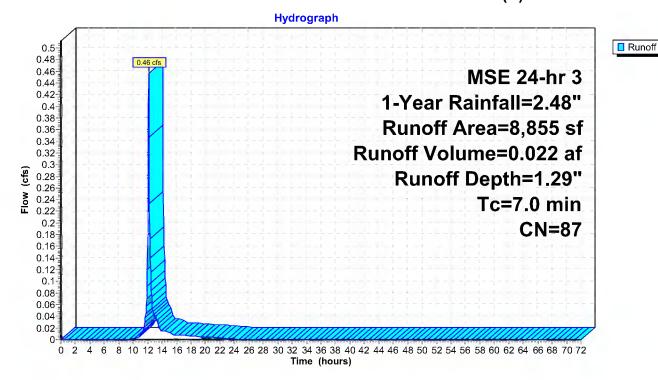
Summary for Subcatchment 4E: Runoff to Wazata Blvd (S)

Runoff = 0.46 cfs @ 12.14 hrs, Volume= 0.022 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | rea (sf) | CN | Description | | | |
|-------|----------|--------|-------------|-------------|---------------|--|
| | 3,630 | 98 | Paved park | ing, HSG E |) | |
| | 5,225 | 80 | >75% Gras | s cover, Go | ood, HSG D | |
| | 8,855 | 87 | Weighted A | verage | | |
| | 5,225 | | 59.01% Pe | rvious Area | 1 | |
| | 3,630 | | 40.99% lm | pervious Ar | rea | |
| Tc | Length | Slope | e Velocity | Capacity | Description | |
| (min) | (feet) | (ft/ft | _ | (cfs) | Description | |
| | (ieet) | ועונ |) (10/500) | (CIS) | | |
| 7.0 | | | | | Direct Entry. | |

Subcatchment 4E: Runoff to Wazata Blvd (S)



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Summary for Reach 1R: Total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

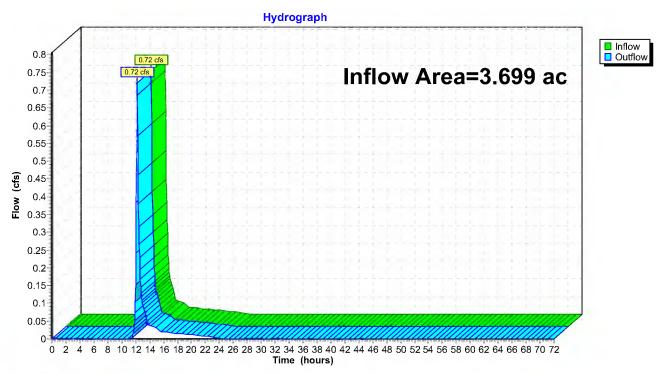
Inflow Area = 3.699 ac, 39.43% Impervious, Inflow Depth = 0.14" for 1-Year event

Inflow = 0.72 cfs @ 12.22 hrs, Volume= 0.044 af

Outflow = 0.72 cfs @ 12.22 hrs, Volume= 0.044 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 1R: Total to offsite wetland



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Summary for Reach 2R: total existing

[40] Hint: Not Described (Outflow=Inflow)

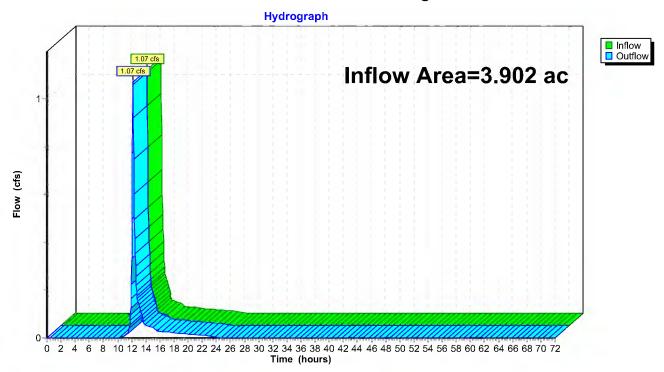
Inflow Area = 3.902 ac, 39.51% Impervious, Inflow Depth = 0.20" for 1-Year event

Inflow = 1.07 cfs @ 12.18 hrs, Volume= 0.066 af

Outflow = 1.07 cfs @ 12.18 hrs, Volume= 0.066 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 2R: total existing



MSE 24-hr 3 1-Year Rainfall=2.48" Printed 2/20/2023

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Volume

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Summary for Pond Wtld Exs: Existing Wetland

Inflow Area = 3.053 ac, 47.77% Impervious, Inflow Depth = 1.45" for 1-Year event

Inflow = 7.36 cfs @ 12.14 hrs, Volume= 0.369 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 916.71' @ 24.45 hrs Surf.Area= 23,389 sf Storage= 16,056 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Avail.Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

Invert

| | | , | | | | |
|-----------|----------|---|------------------|---------------------|---------------------|------------|
| #1 | 916.0 | 76,7 | 84 cf Custom | Stage Data (Pris | matic)Listed below | (Recalc) |
| Elevation | | Surf.Area | Inc.Store | Cum.Store | | |
| (fee | t) | (sq-ft) | (cubic-feet) | (cubic-feet) | | |
| 916.0 | 0 | 21,538 | 0 | 0 | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | |
| Dovice | Douting | lovert | Outlet Device | • | | |
| Device | Routing | Invert | | | | |
| #1 | Primary | 916.35' | 15.0" Round | ocs outlet L= 18 | .0' Ke= 0.900 | |
| | | | Inlet / Outlet I | nvert= 916.35' / 91 | 6.22' S= 0.0072 '/' | Cc = 0.900 |
| | | | n= 0.010, Flo | w Area= 1.23 sf | | |
| #2 | Device 1 | 918.08' | 4.0' long ocs | weir wall 2 End | Contraction(s) | |
| #3 | Device 2 | 917.07' | 15.0" Round | ocs inlet L= 12.0 |)' Ke= 0.900 | |
| | | | Inlet / Outlet I | nvert= 917.07' / 91 | 6.39' S= 0.0567 '/' | Cc = 0.900 |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

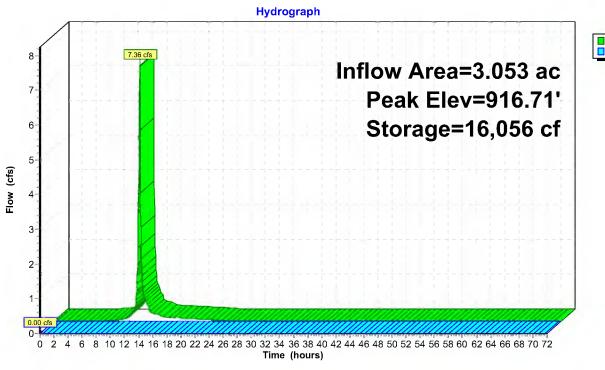
1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs)
-3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Exs: Existing Wetland





Storage

63,564

65,000

66,444

67,897

69,357

70,826

72,303

73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Exs: Existing Wetland

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| | • | • | |
|---------------------|--------------------|-------------------------|---------------------|
| Elevation (feet) | Surface (sg-ft) | Storage (cubic-feet) | Elevation (feet) |
| 916.00 | 21,538 | 0 | 918.55 |
| 916.05 | 21,667 | 1,080 | 918.60 |
| 916.10 | 21,797 | 2,167 | 918.65 |
| 916.15 | 21,926 | 3,260 | 918.70 |
| 916.20 | 22,056 | 4,359 | 918.75 |
| | | · · | |
| 916.25 | 22,186 | 5,465 6 579 | 918.80 |
| 916.30 | 22,315 | 6,578 | 918.85 |
| 916.35 | 22,445 22,574 | 7,697 | 918.90 |
| 916.40 | · · | 8,822 | 918.95 |
| 916.45 | 22,704 | 9,954 | 919.00 |
| 916.50 | 22,833 | 11,093 | |
| 916.55 | 22,962 | 12,238 | |
| 916.60 | 23,092 | 13,389 | |
| 916.65 | 23,221 | 14,547 | |
| 916.70 | 23,351 | 15,711 | |
| 916.75 | 23,481 | 16,882 | |
| 916.80 | 23,610 | 18,059 | |
| 916.85 | 23,740 | 19,243 | |
| 916.90 | 23,869 | 20,433 | |
| 916.95 | 23,999 | 21,630 | |
| 917.00 | 24,128 | 22,833 | |
| 917.05 | 24,263 | 24,043 | |
| 917.10 | 24,398 | 25,259 | |
| 917.15 | 24,533 | 26,483 | |
| 917.20 | 24,668 | 27,713 | |
| 917.25 | 24,803 | 28,949 | |
| 917.30 | 24,938 | 30,193 | |
| 917.35 | 25,073 | 31,443 | |
| 917.40 | 25,208 | 32,700 | |
| 917.45 | 25,343 | 33,964 | |
| 917.50 | 25,478 | 35,235 | |
| 917.55 | 25,613 | 36,512 | |
| 917.60 | 25,748 | 37,796 | |
| 917.65 | 25,883 | 39,087 | |
| 917.70 | 26,018 | 40,384 | |
| 917.75 | 26,153 | 41,688 | |
| 917.80 | 26,288 | 42,999 | |
| 917.85 | 26,423 | 44,317 | |
| 917.90 | 26,558 | 45,642 | |
| 917.95 | 26,693 | 46,973 | |
| 918.00 | 26,828 | 48,311 | |
| 918.05 | 26,992 | 49,657 | |
| 918.10 | 27,157 | 51,010 | |
| 918.15 | 27,321 | 52,372 | |
| 918.20 | 27,486 | 53,742 | |
| 918.25 | 27,651 | 55,121 | |
| 918.30 | 27,815 | 56,507 | |
| 918.35 | 27,980 | 57,902 | |
| 918.40 | 28,144 | 59,305 | |
| 918.45 | 28,309 | 60,717 | |
| 918.50 | 28,473 | 62,136 | |

MSE 24-hr 3 2-Year Rainfall=2.86" Printed 2/20/2023

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1E: To site sewer Runoff Area=80,945 sf 78.49% Impervious Runoff Depth=2.21"

Tc=7.0 min CN=94 Runoff=6.73 cfs 0.343 af

Subcatchment2E: Direct to onsite wetland Runoff Area=52,054 sf 0.00% Impervious Runoff Depth=1.09"

Tc=7.0 min CN=79 Runoff=2.25 cfs 0.108 af

Subcatchment3E: Runoff to offsite wetland Runoff Area=28,124 sf 0.00% Impervious Runoff Depth=1.09"

Flow Length=170' Slope=0.1000 '/' Tc=12.6 min CN=79 Runoff=0.97 cfs 0.058 af

Subcatchment4E: Runoff to Wazata Blvd Runoff Area=8,855 sf 40.99% Impervious Runoff Depth=1.62"

Tc=7.0 min CN=87 Runoff=0.57 cfs 0.027 af

Reach 1R: Total to offsite wetland Inflow=0.97 cfs 0.058 af

Outflow=0.97 cfs 0.058 af

Reach 2R: total existing Inflow=1.40 cfs 0.086 af

Outflow=1.40 cfs 0.086 af

Pond Wtld Exs: Existing Wetland Peak Elev=916.87' Storage=19,656 cf Inflow=8.97 cfs 0.451 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.902 ac Runoff Volume = 0.537 af Average Runoff Depth = 1.65" 60.49% Pervious = 2.360 ac 39.51% Impervious = 1.542 ac Prepared by MFRA

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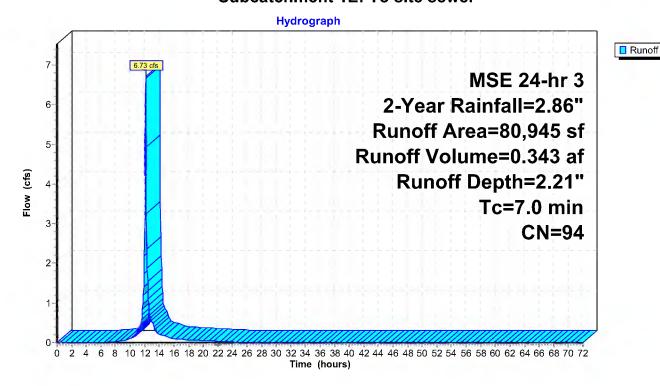
Summary for Subcatchment 1E: To site sewer

Runoff = 6.73 cfs @ 12.14 hrs, Volume= 0.343 af, Depth= 2.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| A | rea (sf) | CN | Description | | | |
|-------------|------------------|----------------------------------|------------------------|-------------------|---------------|--|
| 63,533 98 | | | Paved parking, HSG D | | | |
| | 17,412 | 80 >75% Grass cover, Good, HSG D | | | | |
| 80,945 | | 94 | Weighted Average | | | |
| 17,412 | | | 21.51% Pervious Area | | | |
| 63,533 | | | 78.49% Impervious Area | | | |
| Tc (min) | Length (feet) | Slope (ft/ft) | • | Capacity (cfs) | · | |
| 7.0 | | | | | Direct Entry, | |

Subcatchment 1E: To site sewer



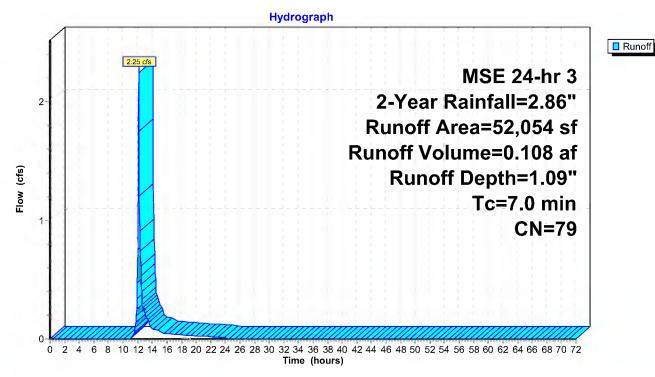
Summary for Subcatchment 2E: Direct to onsite wetland

Runoff = 2.25 cfs @ 12.15 hrs, Volume= 0.108 af, Depth= 1.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| A | rea (sf) | CN | Description | | | | | |
|-------|----------|---------------------|----------------------|--------------------------------|---------------|--|--|--|
| | 0 | 98 | Paved parking, HSG D | | | | | |
| | 52,054 | 79 | Woods/gras | Woods/grass comb., Good, HSG D | | | | |
| | 52,054 | 79 Weighted Average | | | | | | |
| | 52,054 | | 100.00% Pe | ervious Are | ea | | | |
| _ | | 0.1 | | | | | | |
| Tc | Length | Slope | • | Capacity | Description | | | |
| (min) | (feet) | (ft/ft) |) (ft/sec) | (cfs) | | | | |
| 7.0 | | | | | Direct Entry, | | | |

Subcatchment 2E: Direct to onsite wetland



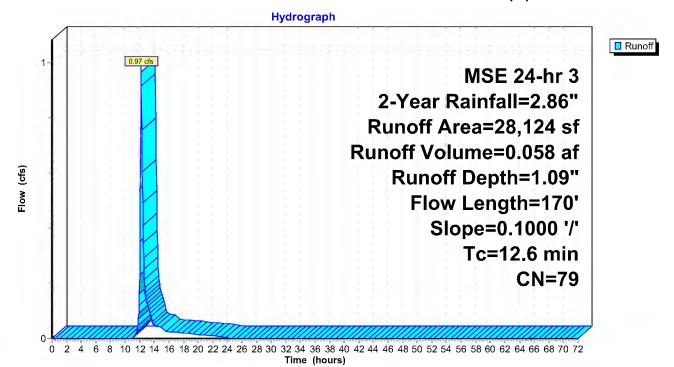
Summary for Subcatchment 3E: Runoff to offsite wetland (N)

Runoff = 0.97 cfs @ 12.21 hrs, Volume= 0.058 af, Depth= 1.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| | rea (sf) | CN [| Description | | | | | | | |
|-------|----------|---------|-------------------------|-------------|--|--|--|--|--|--|
| | 0 | 98 F | 98 Paved parking, HSG D | | | | | | | |
| | 28,124 | 79 V | Voods/gras | ss comb., C | Good, HSG D | | | | | |
| | 28,124 | 79 V | Veighted A | verage | | | | | | |
| | 28,124 | 1 | 00.00% Pe | ervioūs Are | a | | | | | |
| | | | | | | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description | | | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | | | |
| 11.9 | 100 | 0.1000 | 0.14 | | Sheet Flow, | | | | | |
| | | | | | Woods: Light underbrush n= 0.400 P2= 2.86" | | | | | |
| 0.7 | 70 | 0.1000 | 1.58 | | Shallow Concentrated Flow, | | | | | |
| | | | | | Woodland Kv= 5.0 fps | | | | | |
| 12.6 | 170 | Total | | | | | | | | |

Subcatchment 3E: Runoff to offsite wetland (N)



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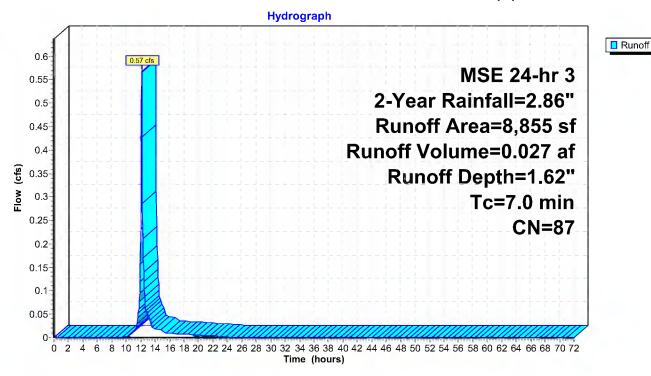
Summary for Subcatchment 4E: Runoff to Wazata Blvd (S)

Runoff = 0.57 cfs @ 12.14 hrs, Volume= 0.027 af, Depth= 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| A | rea (sf) | CN | Description | | | | | |
|-------|----------|---------|----------------------|-------------|---------------|--|--|--|
| | 3,630 | 98 | Paved parking, HSG D | | | | | |
| | 5,225 | 80 | >75% Gras | s cover, Go | ood, HSG D | | | |
| | 8,855 | 87 | Weighted Average | | | | | |
| | 5,225 | | 59.01% Pervious Area | | | | | |
| | 3,630 | | 40.99% lmp | pervious Ar | ea | | | |
| _ | | | | | | | | |
| Tc | Length | Slope | - | Capacity | Description | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | |
| 7.0 | | | | | Direct Entry. | | | |

Subcatchment 4E: Runoff to Wazata Blvd (S)



MSE 24-hr 3 2-Year Rainfall=2.86" Printed 2/20/2023

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Summary for Reach 1R: Total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

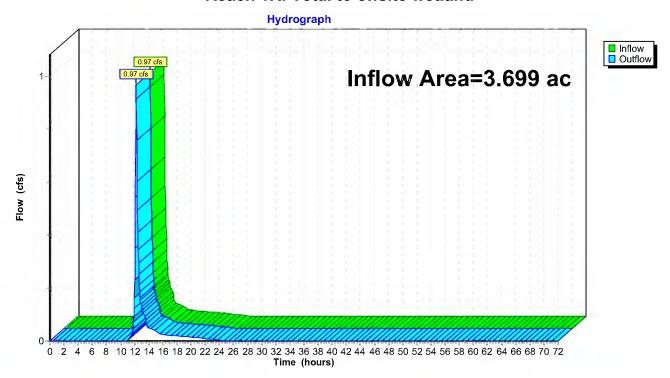
Inflow Area = 3.699 ac, 39.43% Impervious, Inflow Depth = 0.19" for 2-Year event

Inflow = 0.97 cfs @ 12.21 hrs, Volume= 0.058 af

Outflow = 0.97 cfs @ 12.21 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 1R: Total to offsite wetland



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Summary for Reach 2R: total existing

[40] Hint: Not Described (Outflow=Inflow)

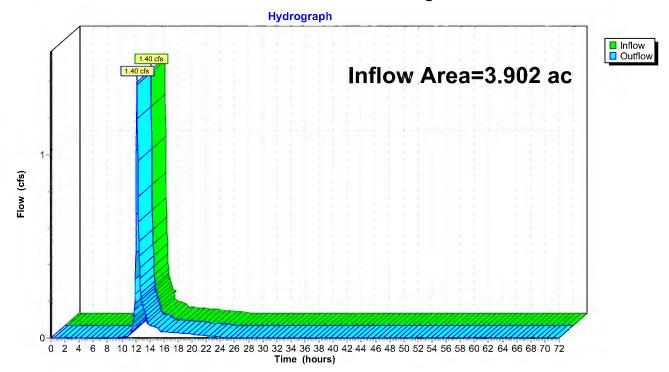
Inflow Area = 3.902 ac, 39.51% Impervious, Inflow Depth = 0.26" for 2-Year event

Inflow = 1.40 cfs @ 12.18 hrs, Volume= 0.086 af

Outflow = 1.40 cfs @ 12.18 hrs, Volume= 0.086 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 2R: total existing



MSE 24-hr 3 2-Year Rainfall=2.86" Printed 2/20/2023

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Volume

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Summary for Pond Wtld Exs: Existing Wetland

Inflow Area = 3.053 ac, 47.77% Impervious, Inflow Depth = 1.77" for 2-Year event

Inflow = 8.97 cfs @ 12.14 hrs, Volume= 0.451 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 916.87' @ 24.45 hrs Surf.Area= 23,785 sf Storage= 19,656 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Avail Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

Invert

| VOIGITIC | IIIVCI | t /\vaii.Oto | rage Otorage E | CSCHPHOH | | | |
|-------------|----------|--------------|--|--------------------|----------------------|-----------|--|
| #1 | 916.00 | 76,78 | 34 cf Custom S | Stage Data (Pris | matic)Listed below (| (Recalc) | |
| Elevation S | | Surf.Area | Inc.Store | Cum.Store | | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | | |
| 918.00 | | 26,828 | 25,478 | 48,311 | | | |
| 919.00 | | 30,118 | 28,473 | 76,784 | | | |
| Device | Routing | Invert | Outlet Devices | | | | |
| #1 | Primary | 916.35' | 15.0" Round o | ocs outlet L= 18 | 3.0' Ke= 0.900 | _ | |
| | • | | Inlet / Outlet Invert= 916.35' / 916.22' S= 0.0072 '/' Cc= 0.900 | | | | |
| | | | n= 0.010, Flow | / Area= 1.23 sf | | | |
| #2 | Device 1 | 918.08' | 4.0' long ocs v | veir wall 2 End | Contraction(s) | | |
| #3 | Device 2 | 917.07' | 15.0" Round of | ocs inlet L= 12.0 | 0' Ke= 0.900 | | |
| | | | Inlet / Outlet Inv | vert= 917.07' / 91 | 6.39' S= 0.0567 '/' | Cc= 0.900 | |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

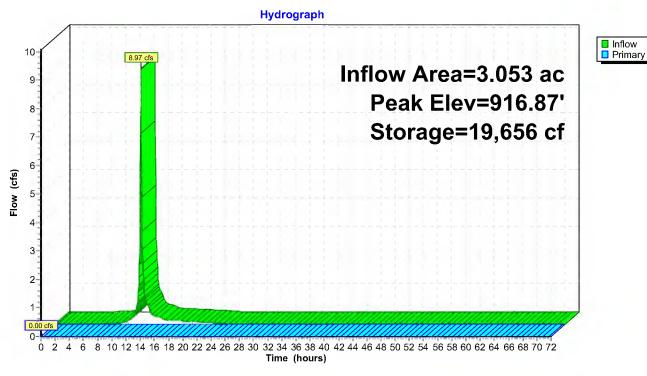
1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs)
-3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Exs: Existing Wetland



Storage

63,564

65,000

66,444

67,897

69,357

70,826

72,303

73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Exs: Existing Wetland

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| Elevation | Surface | Storage | Elevation |
|------------------|------------------|------------------|------------------|
| (feet) | (s <u>q</u> -ft) | (cubic-feet) | (feet) |
| 916.00 916.05 | 21,538 21,667 | 0 1,080 | 918.55 918.60 |
| 916.10 | 21,797 | 2,167 | 918.65 |
| 916.15 | 21,926 | 3,260 | 918.70 |
| 916.20 | 22,056 | 4,359 | 918.75 |
| 916.25 916.30 | 22,186 22,315 | 5,465 6,578 | 918.80 918.85 |
| 916.35 | 22,445 | 7,697 | 918.90 |
| 916.40 | 22,574 | 8,822 | 918.95 |
| 916.45 916.50 | 22,704 22,833 | 9,954 11,093 | 919.00 |
| 916.55 | 22,962 | 12,238 | |
| 916.60 | 23,092 | 13,389 | |
| 916.65 916.70 | 23,221 23,351 | 14,547 15,711 | |
| 916.75 | 23,481 | 16,882 | |
| 916.80 | 23,610 | 18,059 | |
| 916.85 | 23,740 | 19,243 | |
| 916.90 916.95 | 23,869 23,999 | 20,433 21,630 | |
| 917.00 | 24,128 | 22,833 | |
| 917.05 | 24,263 | 24,043 | |
| 917.10 917.15 | 24,398 24,533 | 25,259 26,483 | |
| 917.20 | 24,668 | 27,713 | |
| 917.25 | 24,803 | 28,949 | |
| 917.30 917.35 | 24,938 25,073 | 30,193 31,443 | |
| 917.40 | 25,208 | 32,700 | |
| 917.45 | 25,343 | 33,964 | |
| 917.50 917.55 | 25,478 25,613 | 35,235 36,512 | |
| 917.60 | 25,748 | 37,796 | |
| 917.65 | 25,883 | 39,087 | |
| 917.70 917.75 | 26,018 26,153 | 40,384 41,688 | |
| 917.73 | 26,288 | 42,999 | |
| 917.85 | 26,423 | 44,317 | |
| 917.90 917.95 | 26,558 | 45,642 | |
| 918.00 | 26,693 26,828 | 46,973 48,311 | |
| 918.05 | 26,992 | 49,657 | |
| 918.10 | 27,157 | 51,010 52,272 | |
| 918.15 918.20 | 27,321 27,486 | 52,372 53,742 | |
| 918.25 | 27,651 | 55,121 | |
| 918.30 | 27,815 | 56,507 57,000 | |
| 918.35 918.40 | 27,980 28,144 | 57,902 59,305 | |
| 918.45 | 28,309 | 60,717 | |
| 918.50 | 28,473 | 62,136 | |

20230220 hydrocad_bigger pipes and drop

MSE 24-hr 3 10-Year Rainfall=4.26" Printed 2/20/2023

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1E: To site sewer Runoff Area=80,945 sf 78.49% Impervious Runoff Depth=3.58"

Tc=7.0 min CN=94 Runoff=10.54 cfs 0.554 af

Subcatchment2E: Direct to onsite wetland Runoff Area=52,054 sf 0.00% Impervious Runoff Depth=2.18"

Tc=7.0 min CN=79 Runoff=4.52 cfs 0.217 af

Subcatchment3E: Runoff to offsite wetland Runoff Area=28,124 sf 0.00% Impervious Runoff Depth=2.18"

Flow Length=170' Slope=0.1000 '/' Tc=12.6 min CN=79 Runoff=1.96 cfs 0.117 af

Subcatchment4E: Runoff to Wazata Blvd Runoff Area=8,855 sf 40.99% Impervious Runoff Depth=2.88"

Tc=7.0 min CN=87 Runoff=0.99 cfs 0.049 af

Reach 1R: Total to offsite wetland Inflow=1.96 cfs 0.117 af

Outflow=1.96 cfs 0.117 af

Reach 2R: total existing Inflow=2.73 cfs 0.166 af

Outflow=2.73 cfs 0.166 af

Pond Wtld Exs: Existing Wetland Peak Elev=917.44' Storage=33,586 cf Inflow=15.06 cfs 0.771 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.902 ac Runoff Volume = 0.937 af Average Runoff Depth = 2.88" 60.49% Pervious = 2.360 ac 39.51% Impervious = 1.542 ac

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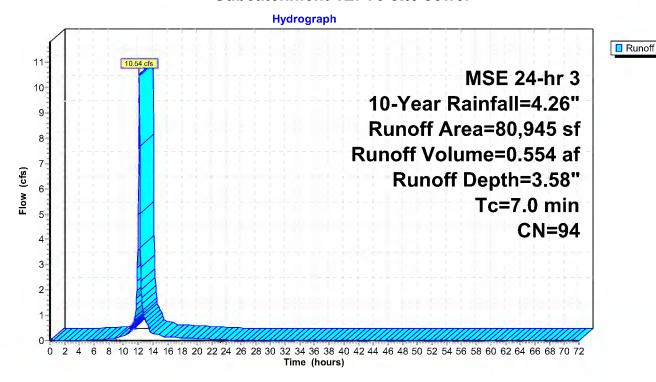
Summary for Subcatchment 1E: To site sewer

Runoff = 10.54 cfs @ 12.14 hrs, Volume= 0.554 af, Depth= 3.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| Α | rea (sf) | CN | Description | | | | |
|-------|----------|------------------------|-------------|-------------|--------------|--|--|
| | 63,533 | 98 | Paved park | ing, HSG E |) | | |
| | 17,412 | 80 | >75% Gras | s cover, Go | ood, HSG D | | |
| | 80,945 | 94 Weighted Average | | | | | |
| | 17,412 | | | | | | |
| | 63,533 | 78.49% Impervious Area | | | | | |
| _ | | | | . | | | |
| Tc | Length | Slope | | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry | | |

Subcatchment 1E: To site sewer



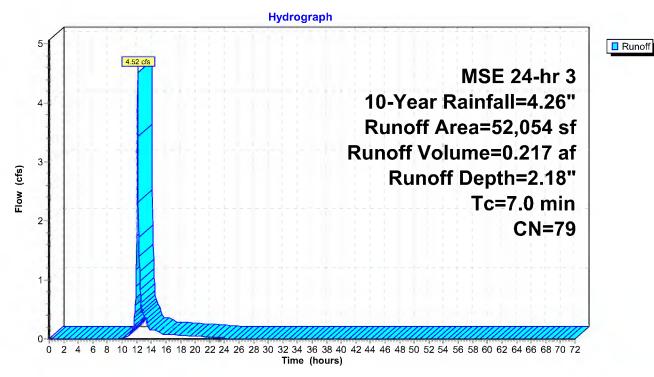
Summary for Subcatchment 2E: Direct to onsite wetland

Runoff = 4.52 cfs @ 12.14 hrs, Volume= 0.217 af, Depth= 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| A | rea (sf) | CN | Description | | | | | |
|-------|----------|---------------------|----------------------|--------------------------------|---------------|--|--|--|
| | 0 | 98 | Paved parking, HSG D | | | | | |
| | 52,054 | 79 | Woods/gras | Woods/grass comb., Good, HSG D | | | | |
| | 52,054 | 79 Weighted Average | | | | | | |
| | 52,054 | | 100.00% Pe | ervious Are | ea | | | |
| _ | | | | | | | | |
| Tc | Length | Slope | e Velocity | Capacity | Description | | | |
| (min) | (feet) | (ft/ft) |) (ft/sec) | (cfs) | | | | |
| 7.0 | | | | | Direct Entry, | | | |

Subcatchment 2E: Direct to onsite wetland



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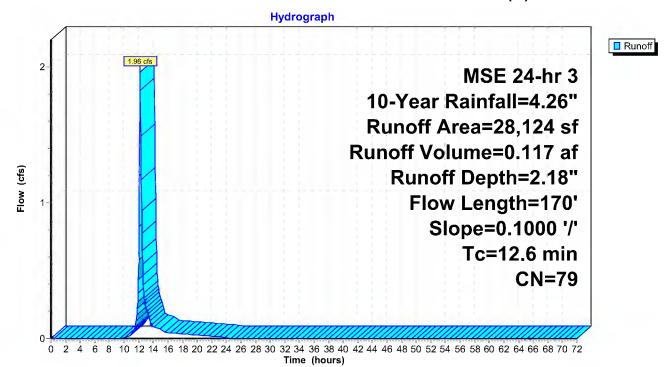
Summary for Subcatchment 3E: Runoff to offsite wetland (N)

Runoff = 1.96 cfs @ 12.21 hrs, Volume= 0.117 af, Depth= 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| A | rea (sf) | CN [| Description | | | | | | | |
|-------|----------|---------|-------------------------|-------------|--|--|--|--|--|--|
| | 0 | 98 F | 98 Paved parking, HSG D | | | | | | | |
| | 28,124 | 79 ١ | Voods/gras | ss comb., C | Good, HSG D | | | | | |
| | 28,124 | 79 \ | Veighted A | verage | | | | | | |
| | 28,124 | 1 | 100.00% Pe | ervious Are | a | | | | | |
| Tc | | | | | | | | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | | | |
| 11.9 | 100 | 0.1000 | 0.14 | | Sheet Flow, | | | | | |
| 0.7 | 70 | 0.1000 | 1.58 | | Woods: Light underbrush n= 0.400 P2= 2.86" Shallow Concentrated Flow, Woodland Kv= 5.0 fps | | | | | |
| 12.6 | 170 | Total | | | | | | | | |

Subcatchment 3E: Runoff to offsite wetland (N)



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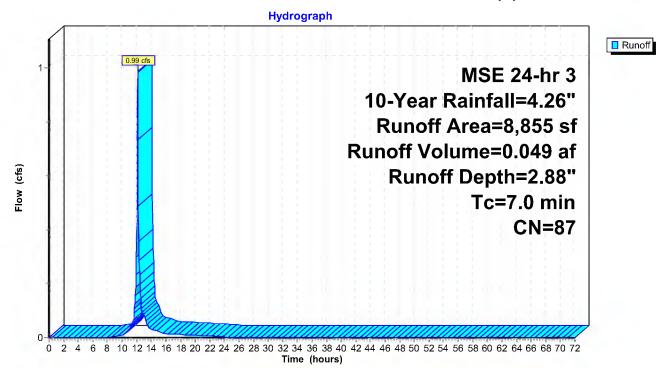
Summary for Subcatchment 4E: Runoff to Wazata Blvd (S)

Runoff = 0.99 cfs @ 12.14 hrs, Volume= 0.049 af, Depth= 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| | Α | rea (sf) | CN | Description | | | | |
|---|-------|----------|---------|-------------------------------|------------|---------------|--|--|
| | | 3,630 | 98 | Paved park | ing, HSG E |) | | |
| | | 5,225 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | | 8,855 | 87 | Weighted A | verage | | | |
| | | 5,225 | | 59.01% Pervious Area | | | | |
| | | 3,630 | | 40.99% Impervious Area | | | | |
| | | | | | | | | |
| | Тс | Length | Slope | - | Capacity | Description | | |
| (| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| | 7.0 | | | | | Direct Entry. | | |

Subcatchment 4E: Runoff to Wazata Blvd (S)



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Summary for Reach 1R: Total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

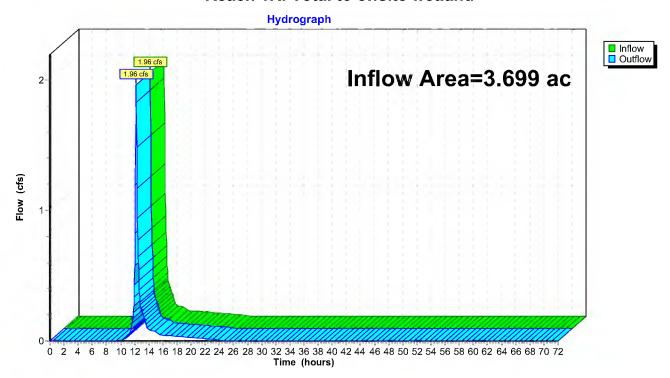
Inflow Area = 3.699 ac, 39.43% Impervious, Inflow Depth = 0.38" for 10-Year event

Inflow = 1.96 cfs @ 12.21 hrs, Volume= 0.117 af

Outflow = 1.96 cfs @ 12.21 hrs, Volume= 0.117 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 1R: Total to offsite wetland



MSE 24-hr 3 10-Year Rainfall=4.26" Printed 2/20/2023

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Summary for Reach 2R: total existing

[40] Hint: Not Described (Outflow=Inflow)

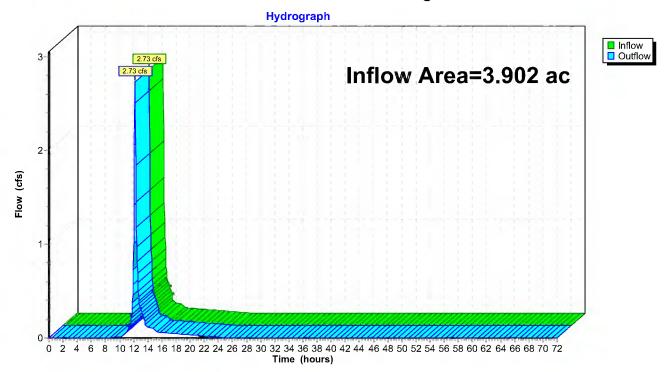
Inflow Area = 3.902 ac, 39.51% Impervious, Inflow Depth = 0.51" for 10-Year event

Inflow = 2.73 cfs @ 12.18 hrs, Volume= 0.166 af

Outflow = 2.73 cfs @ 12.18 hrs, Volume= 0.166 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 2R: total existing



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Summary for Pond Wtld Exs: Existing Wetland

Inflow Area = 3.053 ac, 47.77% Impervious, Inflow Depth = 3.03" for 10-Year event

15.06 cfs @ 12.14 hrs, Volume= Inflow 0.771 af

Outflow 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 917.44' @ 24.45 hrs Surf.Area= 25,303 sf Storage= 33,586 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

| Volume | Inve | rt Avail.Sto | rage Storaç | ge Description | | |
|----------|----------|----------------------|---------------------------|--|---|-----------|
| #1 | 916.0 | 0' 76,78 | 34 cf Custo | m Stage Data (Pr | ismatic) Listed below (| (Recalc) |
| Elevatio | | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | |
| Device | Routing | Invert | Outlet Devi | ces | | |
| #1 | Primary | 916.35' | 15.0" Roui | nd ocs outlet L= | 18.0' Ke= 0.900 | |
| | • | | | t Invert= 916.35' / 9 Flow Area= 1.23 sf | 916.22' S= 0.0072 '/' | Cc= 0.900 |
| #2 | Device 1 | 918.08' | 4.0' long o | cs weir wall 2 End | d Contraction(s) | |
| #3 | Device 2 | 917.07' | | nd ocs inlet L= 12 t Invert= 917.07' / 9 | 2.0' Ke= 0.900 916.39' S= 0.0567 '/' | Cc= 0.900 |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

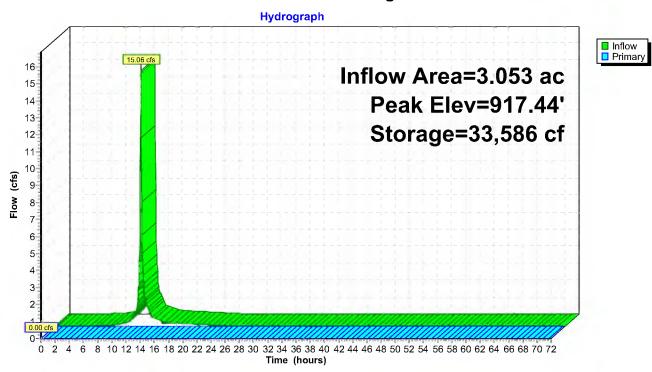
n= 0.010, Flow Area= 1.23 sf

-1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs) 3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Exs: Existing Wetland



Stage-Area-Storage for Pond Wtld Exs: Existing Wetland

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

Storage

63,564

65,000

66,444

67,897

69,357

70,826

72,303

73,789

75,282

76,784

(cubic-feet)

| | • | • | |
|---------------------|--------------------|-------------------------|---------------------|
| Elevation (feet) | Surface (sg-ft) | Storage (cubic-feet) | Elevation (feet) |
| 916.00 | 21,538 | 0 | 918.55 |
| 916.05 | 21,667 | 1,080 | 918.60 |
| 916.10 | 21,797 | 2,167 | 918.65 |
| | | | |
| 916.15 | 21,926 | 3,260 | 918.70 |
| 916.20 | 22,056 | 4,359 | 918.75 |
| 916.25 | 22,186 | 5,465 | 918.80 |
| 916.30 | 22,315 | 6,578 | 918.85 |
| 916.35 | 22,445 | 7,697 | 918.90 |
| 916.40 | 22,574 | 8,822 | 918.95 |
| 916.45 | 22,704 | 9,954 | 919.00 |
| 916.50 | 22,833 | 11,093 | |
| 916.55 | 22,962 | 12,238 | |
| 916.60 | 23,092 | 13,389 | |
| 916.65 | 23,221 | 14,547 | |
| 916.70 | 23,351 | 15,711 | |
| | 23,481 | | |
| 916.75 | | 16,882 | |
| 916.80 | 23,610 | 18,059 | |
| 916.85 | 23,740 | 19,243 | |
| 916.90 | 23,869 | 20,433 | |
| 916.95 | 23,999 | 21,630 | |
| 917.00 | 24,128 | 22,833 | |
| 917.05 | 24,263 | 24,043 | |
| 917.10 | 24,398 | 25,259 | |
| 917.15 | 24,533 | 26,483 | |
| 917.20 | 24,668 | 27,713 | |
| 917.25 | 24,803 | 28,949 | |
| 917.30 | 24,938 | 30,193 | |
| 917.35 | 25,073 | 31,443 | |
| 917.40 | 25,208 | 32,700 | |
| | | | |
| 917.45 | 25,343 | 33,964 | |
| 917.50 | 25,478 | 35,235 | |
| 917.55 | 25,613 | 36,512 | |
| 917.60 | 25,748 | 37,796 | |
| 917.65 | 25,883 | 39,087 | |
| 917.70 | 26,018 | 40,384 | |
| 917.75 | 26,153 | 41,688 | |
| 917.80 | 26,288 | 42,999 | |
| 917.85 | 26,423 | 44,317 | |
| 917.90 | 26,558 | 45,642 | |
| 917.95 | 26,693 | 46,973 | |
| 918.00 | 26,828 | 48,311 | |
| 918.05 | 26,992 | 49,657 | |
| 918.10 | 27,157 | 51,010 | |
| 918.15 | 27,321 | 52,372 | |
| 918.20 | 27,486 | 53,742 | |
| | | | |
| 918.25 | 27,651 | 55,121 50,507 | |
| 918.30 | 27,815 | 56,507 | |
| 918.35 | 27,980 | 57,902 | |
| 918.40 | 28,144 | 59,305 | |
| 918.45 | 28,309 | 60,717 | |
| 918.50 | 28,473 | 62,136 | |
| | | | |

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MSE 24-hr 3 100-Year Rainfall=7.32" Printed 2/20/2023

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1E: To site sewer Runoff Area=80,945 sf 78.49% Impervious Runoff Depth=6.61"

Tc=7.0 min CN=94 Runoff=18.74 cfs 1.023 af

Subcatchment2E: Direct to onsite wetland Runoff Area=52,054 sf 0.00% Impervious Runoff Depth=4.88"

Tc=7.0 min CN=79 Runoff=9.88 cfs 0.486 af

Subcatchment3E: Runoff to offsite wetland Runoff Area=28,124 sf 0.00% Impervious Runoff Depth=4.88"

Flow Length=170' Slope=0.1000 '/' Tc=12.6 min CN=79 Runoff=4.33 cfs 0.262 af

Subcatchment4E: Runoff to Wazata Blvd Runoff Area=8,855 sf 40.99% Impervious Runoff Depth=5.79"

Tc=7.0 min CN=87 Runoff=1.91 cfs 0.098 af

Reach 1R: Total to offsite wetland Inflow=4.33 cfs 0.612 af

Outflow=4.33 cfs 0.612 af

Reach 2R: total existing Inflow=5.82 cfs 0.710 af

Outflow=5.82 cfs 0.710 af

Pond Wtld Exs: Existing Wetland Peak Elev=918.22' Storage=54,202 cf Inflow=28.61 cfs 1.509 af

Outflow=0.66 cfs 0.350 af

Total Runoff Area = 3.902 ac Runoff Volume = 1.869 af Average Runoff Depth = 5.75" 60.49% Pervious = 2.360 ac 39.51% Impervious = 1.542 ac

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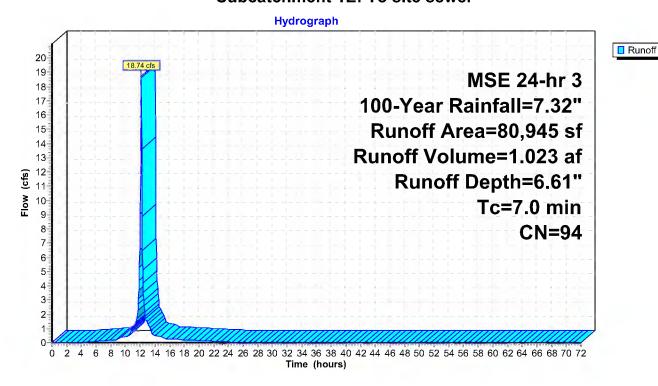
Summary for Subcatchment 1E: To site sewer

Runoff = 18.74 cfs @ 12.14 hrs, Volume= 1.023 af, Depth= 6.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN | Description | | | | | |
|-------|-----------------------------|---------|--------------------------|-------------|---------------|--|--|--|
| | 63,533 | 98 | Paved parking, HSG D | | | | | |
| | 17,412 | 80 | >75% Gras | s cover, Go | od, HSG D | | | |
| | 80,945 | 94 | Weighted A | verage | | | | |
| | 17,412 21.51% Pervious Area | | | | | | | |
| | 63,533 | | 78.49% lm <mark>բ</mark> | pervious Ar | ea | | | |
| _ | | 0.1 | | | — | | | |
| Tc | Length | Slope | - | Capacity | Description | | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | |
| 7.0 | | | | | Direct Entry. | | | |

Subcatchment 1E: To site sewer



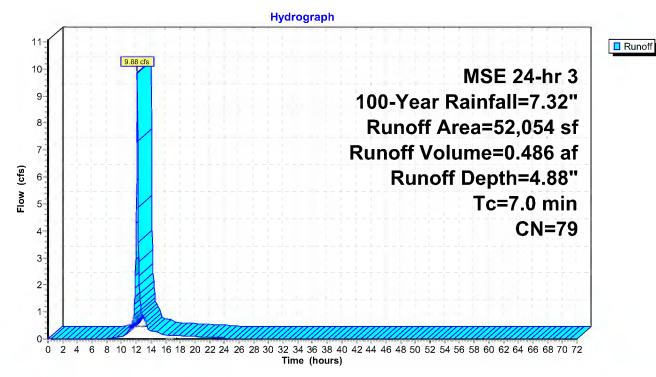
Summary for Subcatchment 2E: Direct to onsite wetland

Runoff = 9.88 cfs @ 12.14 hrs, Volume= 0.486 af, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN | Description | | | | | | |
|-------|----------|--------|-------------|--------------------------------|---------------|--|--|--|--|
| | 0 | 98 | Paved park | ing, HSG D | | | | | |
| | 52,054 | 79 | Woods/gras | Voods/grass comb., Good, HSG D | | | | | |
| | 52,054 | 79 | Weighted A | verage | | | | | |
| | 52,054 | | 100.00% Pe | ervious Are | ea | | | | |
| | | | | | | | | | |
| Tc | Length | Slope | e Velocity | Capacity | Description | | | | |
| (min) | (feet) | (ft/ft |) (ft/sec) | (cfs) | | | | | |
| 7.0 | | | | | Direct Entry, | | | | |

Subcatchment 2E: Direct to onsite wetland



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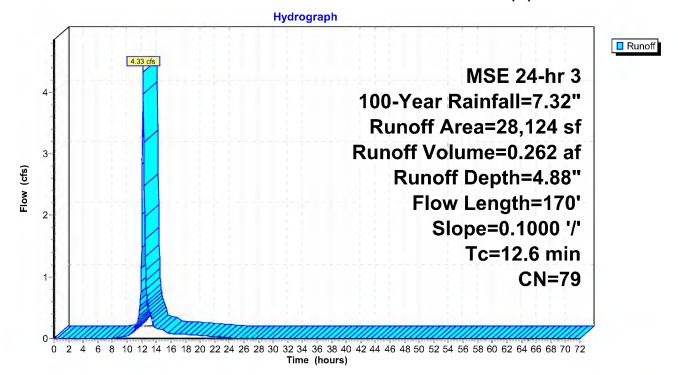
Summary for Subcatchment 3E: Runoff to offsite wetland (N)

Runoff = 4.33 cfs @ 12.20 hrs, Volume= 0.262 af, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| _ | Α | rea (sf) | CN E | Description | | | |
|----------------------------|-------------|------------------|------------------|----------------------|-------------------|--|--|
| Ī | | 0 | 98 F | Paved park | ing, HSG D |) | |
| _ | | 28,124 | 79 V | Voods/gras | ss comb., C | Good, HSG D | |
| 28,124 79 Weighted Average | | | | | | | |
| | | 28,124 | 1 | 00.00% Pe | ervious Are | a | |
| | _ | | 01 | N/ 1 '' | 0 :1 | | |
| | Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description | |
| - | 11.9 | 100 | 0.1000 | 0.14 | (0.0) | Sheet Flow, | |
| | | | | | | Woods: Light underbrush n= 0.400 P2= 2.86" | |
| | 0.7 | 70 | 0.1000 | 1.58 | | Shallow Concentrated Flow, | |
| _ | | | | | | Woodland Kv= 5.0 fps | |
| | 12.6 | 170 | Total | | | | |

Subcatchment 3E: Runoff to offsite wetland (N)



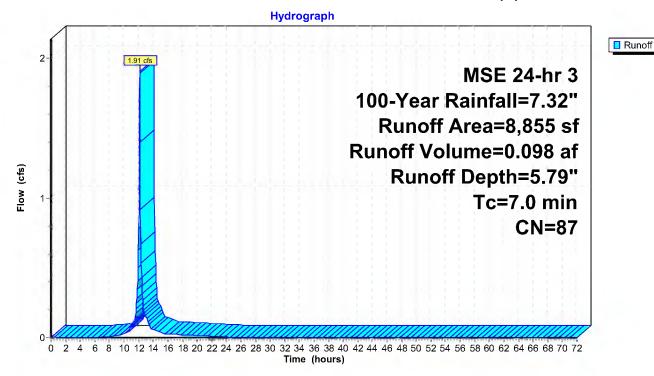
Summary for Subcatchment 4E: Runoff to Wazata Blvd (S)

Runoff = 1.91 cfs @ 12.14 hrs, Volume= 0.098 af, Depth= 5.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| _ | Α | rea (sf) | CN | Description | | | | | | |
|---|-------|----------|---------|------------------------|------------------------------|--------------|--|--|--|--|
| _ | | 3,630 | 98 | Paved parking, HSG D | | | | | | |
| _ | | 5,225 | 80 | >75% Gras | 75% Grass cover, Good, HSG D | | | | | |
| | | 8,855 | 87 | Weighted Average | | | | | | |
| | | 5,225 | | 59.01% Pervious Area | | | | | | |
| | | 3,630 | | 40.99% Impervious Area | | | | | | |
| | _ | | | | | | | | | |
| | Tc | Length | Slope | • | Capacity | Description | | | | |
| _ | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | | |
| | 7.0 | | | | | Direct Entry | | | | |

Subcatchment 4E: Runoff to Wazata Blvd (S)



MSE 24-hr 3 100-Year Rainfall=7.32" Printed 2/20/2023

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Summary for Reach 1R: Total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

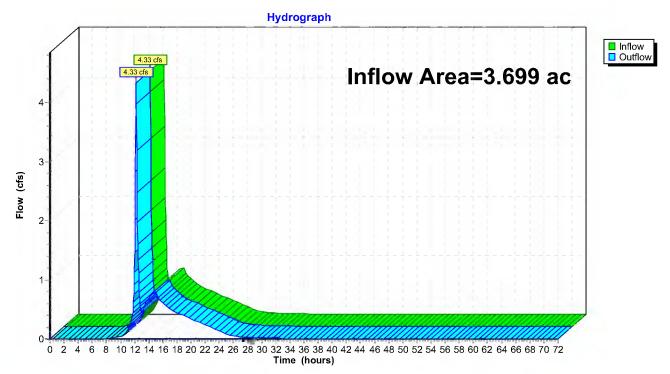
Inflow Area = 3.699 ac, 39.43% Impervious, Inflow Depth = 1.99" for 100-Year event

Inflow = 4.33 cfs @ 12.20 hrs, Volume= 0.612 af

Outflow = 4.33 cfs @ 12.20 hrs, Volume= 0.612 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 1R: Total to offsite wetland



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Summary for Reach 2R: total existing

[40] Hint: Not Described (Outflow=Inflow)

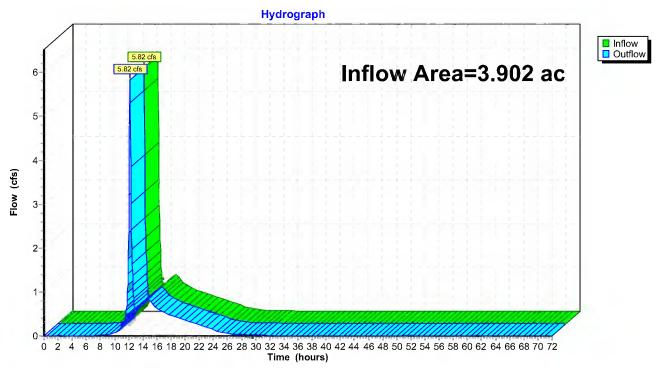
Inflow Area = 3.902 ac, 39.51% Impervious, Inflow Depth = 2.18" for 100-Year event

Inflow = 5.82 cfs @ 12.18 hrs, Volume= 0.710 af

Outflow = 5.82 cfs @ 12.18 hrs, Volume= 0.710 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 2R: total existing



MSE 24-hr 3 100-Year Rainfall=7.32" Printed 2/20/2023

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Summary for Pond Wtld Exs: Existing Wetland

Inflow Area = 3.053 ac, 47.77% Impervious, Inflow Depth = 5.93" for 100-Year event

Inflow = 28.61 cfs @ 12.14 hrs, Volume= 1.509 af

Outflow = 0.66 cfs @ 15.05 hrs, Volume= 0.350 af, Atten= 98%, Lag= 174.5 min

Primary = 0.66 cfs @ 15.05 hrs, Volume= 0.350 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 918.22' @ 15.05 hrs Surf.Area= 27,541 sf Storage= 54,202 cf

Plug-Flow detention time= 465.9 min calculated for 0.350 af (23% of inflow)

Center-of-Mass det. time= 334.2 min (1,103.1 - 768.9)

| Volume | Inve | ert Avail.Sto | rage Storage | e Description | | | | | | |
|----------|----------|---------------|----------------|--|--------------------------|-----------|--|--|--|--|
| #1 | 916.0 | 0' 76,78 | 34 cf Custon | n Stage Data (Pi | rismatic)Listed below (I | Recalc) | | | | |
| Elevatio | on | Surf.Area | Inc.Store | Cum.Store | | | | | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | | | | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | | | | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | | | | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | | | | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | | | | | |
| Device | Routing | Invert | Outlet Device | es | | | | | | |
| #1 | Primary | 916.35' | 15.0" Roun | d ocs outlet L= | 18.0' Ke= 0.900 | | | | | |
| | | | Inlet / Outlet | Invert= 916.35' / | 916.22' S= 0.0072 '/' | Cc= 0.900 | | | | |
| | | | n= 0.010, Fl | n= 0.010, Flow Area= 1.23 sf | | | | | | |
| #2 | Device 1 | 918.08' | 4.0' long oc | 4.0' long ocs weir wall 2 End Contraction(s) | | | | | | |
| #3 | Device 2 | 917.07' | 15.0" Roun | d ocs inlet L= 1 | 2.0' Ke= 0.900 | | | | | |
| | | | | | 916.39' S= 0.0567 '/' | Cc= 0.900 | | | | |
| | | | n= 0.010, Fl | ow Area= 1.23 sf | : | | | | | |

Primary OutFlow Max=0.66 cfs @ 15.05 hrs HW=918.22' TW=0.00' (Dynamic Tailwater)

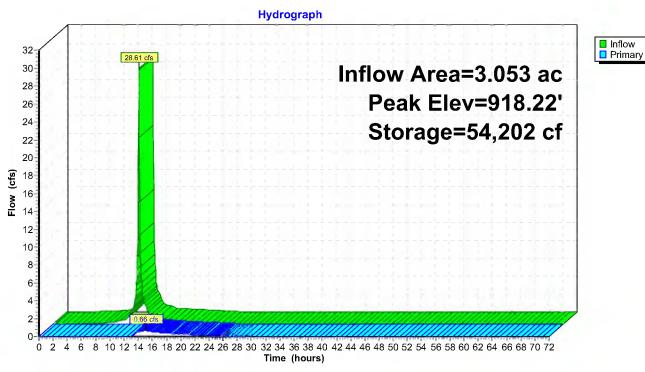
-1=ocs outlet (Passes 0.66 cfs of 5.20 cfs potential flow)
-2=ocs weir wall (Weir Controls 0.66 cfs @ 1.21 fps)

3=ocs inlet (Passes 0.66 cfs of 1.66 cfs potential flow)

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Pond Wtld Exs: Existing Wetland



Storage

63,564

65,000

66,444

67,897

69,357

70,826

72,303

73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Exs: Existing Wetland

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

Elevation

(feet)

918.55

918.60

918.65

918.70

918.75

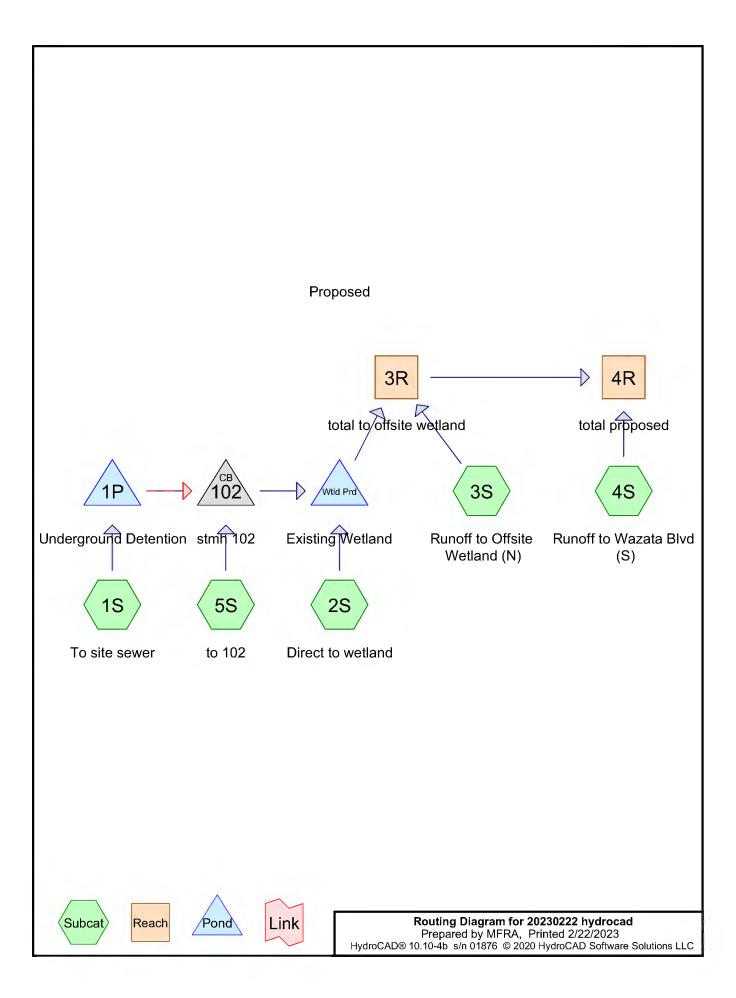
918.80 918.85

918.90

918.95

919.00

| | • | | |
|---------------------|--------------------|-------------------------|--|
| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | |
| 916.00 | 21,538 | 0 | |
| 916.05 | 21,667 | 1,080 | |
| 916.10 | 21,797 | 2,167 | |
| 916.15 | 21,926 | 3,260 | |
| 916.20 | 22,056 | 4,359 | |
| 916.25 | 22,186 | 5,465 | |
| 916.30 | 22,315 | 6,578 | |
| 916.35 | 22,445 | 7,697 | |
| 916.40 | 22,574 | 8,822 | |
| 916.45 | 22,704 | 9,954 | |
| 916.50 | 22,833 | 11,093 | |
| 916.55 | 22,962 | 12,238 | |
| 916.60 | 23,092 | 13,389 | |
| 916.65 | 23,221 | 14,547 | |
| 916.70 | 23,351 | 15,711 | |
| 916.75 | 23,481 | 16,882 | |
| 916.80 | 23,610 | 18,059 | |
| 916.85 | 23,740 | 19,243 | |
| 916.90 | 23,869 | 20,433 | |
| 916.95 | 23,999 | 21,630 | |
| 917.00 | 24,128 | 22,833 | |
| 917.05 | 24,126 | 24,043 | |
| 917.00 | 24,398 | 25,259 | |
| 917.15 | 24,533 | 26,483 | |
| 917.20 | 24,668 | | |
| 917.25 | 24,803 | 27,713 | |
| 917.30 | 24,803 24,938 | 28,949 30,193 | |
| 917.35 | 25,073 | 31,443 | |
| 917.40 | 25,208 | 32,700 | |
| 917.45 | 25,343 | 33,964 | |
| 917.50 | | | |
| 917.55 | 25,478 25,613 | 35,235 | |
| 917.60 | 25,748 | 36,512 37,796 | |
| 917.65 | 25,883 | 39,087 | |
| 917.03 | 26,018 | 40,384 | |
| 917.75 | 26,153 | 41,688 | |
| 917.73 | 26,288 | 42,999 | |
| 917.85 | 26,423 | 44,317 | |
| 917.90 | 26,558 | 45,642 | |
| 917.95 | 26,693 | 46,973 | |
| 918.00 | 26,828 | 48,311 | |
| 918.05 | 26,992 | 49,657 | |
| 918.10 | 27,157 | 51,010 | |
| 918.15 | 27,321 | 52,372 | |
| 918.20 | 27,486 | 53,742 | |
| 918.25 | 27,460 | 55,121 | |
| 918.30 | 27,815 | 56,507 | |
| 918.35 | 27,980 | 57,902 | |
| 918.40 | 28,144 | 59,305 | |
| 918.45 | 28,309 | 60,717 | |
| 918.50 | 28,473 | 62,136 | |
| 310.00 | 20,473 | 02,100 | |



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Project Notes

Rainfall events imported from "NRCS-Rain.txt" for 5327 MN Hennepin

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Rainfall Events Listing (selected events)

| Event# | Event | Storm Type | Curve | Mode | Duration | B/B | Depth | AMC |
|--------|----------|------------|-------|---------|----------|-----|----------|-----|
| | Name | | | | (hours) | | (inches) | |
| 1 | 1-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 2.48 | 2 |
| 2 | 2-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 2.86 | 2 |
| 3 | 10-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 4.26 | 2 |
| 4 | 100-Year | MSE 24-hr | 3 | Default | 24.00 | 1 | 7.32 | 2 |

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Area Listing (selected nodes)

| Area | CN | Description |
|---------|----|--|
| (acres) | | (subcatchment-numbers) |
| 1.372 | 80 | >75% Grass cover, Good, HSG D (1S, 2S, 4S, 5S) |
| 1.980 | 98 | Paved parking, HSG D (1S, 2S, 3S, 4S, 5S) |
| 0.560 | 79 | Woods/grass comb., Good, HSG D (3S) |
| 3.913 | 89 | TOTAL AREA |

Soil Listing (selected nodes)

| Area | Soil | Subcatchment |
|---------|-------|--------------------|
| (acres) | Group | Numbers |
| 0.000 | HSG A | |
| 0.000 | HSG B | |
| 0.000 | HSG C | |
| 3.913 | HSG D | 1S, 2S, 3S, 4S, 5S |
| 0.000 | Other | |
| 3.913 | | TOTAL AREA |

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Ground Covers (selected nodes)

| HSG-A | HSG-B | HSG-C | HSG-D | Other | Total | Ground | Subcatchment |
|-------------|---------|---------|---------|---------|---------|-------------------------|--------------|
| (acres) | (acres) | (acres) | (acres) | (acres) | (acres) | Cover | Numbers |
| 0.000 | 0.000 | 0.000 | 1.372 | 0.000 | 1.372 | >75% Grass cover, Good | 1S, |
| | | | | | | | 2S, |
| | | | | | | | 4S, 5S |
| 0.000 | 0.000 | 0.000 | 1.980 | 0.000 | 1.980 | Paved parking | 1S, |
| | | | | | | | 2S, |
| | | | | | | | 3S, |
| | | | | | | | 4S, 5S |
| 0.000 | 0.000 | 0.000 | 0.560 | 0.000 | 0.560 | Woods/grass comb., Good | 3S |
| 0.000 | 0.000 | 0.000 | 3.913 | 0.000 | 3.913 | TOTAL AREA | |

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Pipe Listing (selected nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Width (inches) | Diam/Height (inches) | Inside-Fill (inches) |
|-------|----------------|---------------------|----------------------|------------------|------------------|-------|----------------|----------------------|-------------------------|
| 1 | 1P | 920.70 | 920.17 | 108.0 | 0.0049 | 0.011 | 0.0 | 24.0 | 0.0 |
| 2 | 102 | 919.93 | 918.80 | 281.0 | 0.0040 | 0.011 | 0.0 | 24.0 | 0.0 |
| 3 | Wtld Prd | 916.35 | 916.22 | 18.0 | 0.0072 | 0.010 | 0.0 | 15.0 | 0.0 |
| 4 | Wtld Prd | 917.07 | 916.39 | 12.0 | 0.0567 | 0.010 | 0.0 | 15.0 | 0.0 |

Proposed

MSE 24-hr 3 1-Year Rainfall=2.48"

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To site sewer Runoff Area=79,886 sf 95.12% Impervious Runoff Depth=2.14"

Tc=7.0 min CN=97 Runoff=6.15 cfs 0.328 af

Subcatchment2S: Direct to wetland Runoff Area=47,288 sf 6.48% Impervious Runoff Depth=0.93"

Tc=7.0 min CN=81 Runoff=1.74 cfs 0.084 af

Subcatchment3S: Runoff to Offsite Runoff Area=25,698 sf 5.00% Impervious Runoff Depth=0.88"

Flow Length=260' Slope=0.0200 '/' Tc=17.8 min CN=80 Runoff=0.59 cfs 0.043 af

Subcatchment4S: Runoff to Wazata Blvd Runoff Area=10,922 sf 16.27% Impervious Runoff Depth=1.04"

Tc=7.0 min CN=83 Runoff=0.45 cfs 0.022 af

Subcatchment 5S: to 102 Runoff Area = 6,651 sf 62.29% Impervious Runoff Depth = 1.59"

Tc=7.0 min CN=91 Runoff=0.41 cfs 0.020 af

Reach 3R: total to offsite wetland Inflow=0.59 cfs 0.043 af

Outflow=0.59 cfs 0.043 af

Reach 4R: total proposed Inflow=0.84 cfs 0.065 af

Outflow=0.84 cfs 0.065 af

Pond 1P: Underground Detention Peak Elev=926.39' Storage=7,086 cf Inflow=6.15 cfs 0.328 af

Outflow=0.48 cfs 0.328 af

Pond 102: stmh 102 Peak Elev=920.37' Inflow=0.89 cfs 0.348 af

24.0" Round Culvert n=0.011 L=281.0' S=0.0040 '/' Outflow=0.89 cfs 0.348 af

Pond Wtld Prd: Existing Wetland Peak Elev=916.83' Storage=18,813 cf Inflow=2.64 cfs 0.432 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.913 ac Runoff Volume = 0.497 af Average Runoff Depth = 1.52" 49.39% Pervious = 1.933 ac 50.61% Impervious = 1.980 ac

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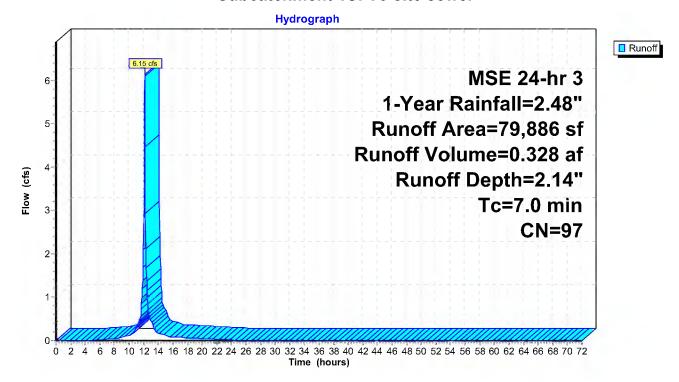
Summary for Subcatchment 1S: To site sewer

Runoff = 6.15 cfs @ 12.14 hrs, Volume= 0.328 af, Depth= 2.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | Area (sf) | CN | Description | | | | |
|-------|---------------------------|---------------------------|-------------|-------------|--------------|--|--|
| | 75,991 | 98 | Paved park | ing, HSG E |) | | |
| | 3,895 | 80 | >75% Gras | s cover, Go | ood, HSG D | | |
| | 79,886 | 97 | Weighted A | verage | | | |
| | 3,895 4.88% Pervious Area | | | | | | |
| | 75,991 | 91 95.12% Impervious Area | | | | | |
| То | Longth | Slope | Volocity | Conneity | Description | | |
| Tc | | Slope | - | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry | | |

Subcatchment 1S: To site sewer



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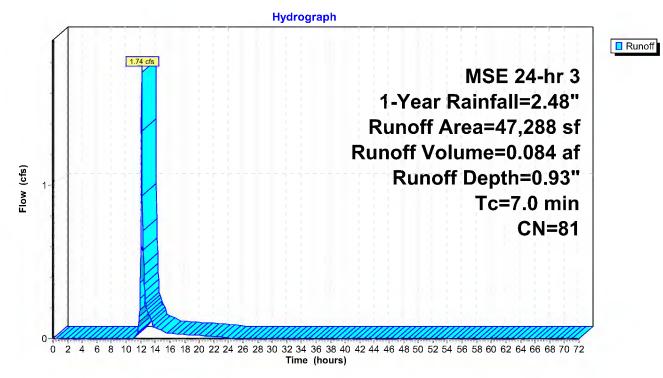
Summary for Subcatchment 2S: Direct to wetland

Runoff = 1.74 cfs @ 12.15 hrs, Volume= 0.084 af, Depth= 0.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | Area (sf) | CN | Description | | | | |
|-------------|-----------|----------------------|-----------------------|-------------|---------------|--|--|
| | 3,064 | 98 | Paved park | ing, HSG E |) | | |
| | 44,224 | 80 | >75% Gras | s cover, Go | ood, HSG D | | |
| | 47,288 | 81 | 31 Weighted Average | | | | |
| | 44,224 | 93.52% Pervious Area | | | | | |
| | 3,064 | | 6.48% Impervious Area | | | | |
| _ | | | | | | | |
| To | | Slope | • | Capacity | Description | | |
| <u>(min</u> |) (feet) | (ft/ft) |) (ft/sec) | (cfs) | | | |
| 7.0 |) | | | | Direct Entry. | | |

Subcatchment 2S: Direct to wetland



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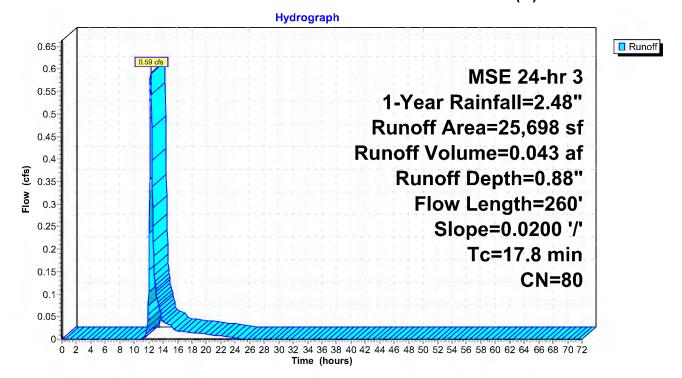
Summary for Subcatchment 3S: Runoff to Offsite Wetland (N)

Runoff = 0.59 cfs @ 12.28 hrs, Volume= 0.043 af, Depth= 0.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | Α | rea (sf) | CN E | Description | | |
|----|------|----------|---------|-------------|-------------|---------------------------------|
| | | 1,286 | 98 F | Paved park | ing, HSG D |) |
| | | 24,412 | 79 V | Voods/gras | ss comb., G | Good, HSG D |
| | | 25,698 | 80 V | Veighted A | verage | |
| | | 24,412 | 9 | 5.00% Per | vious Area | |
| | | 1,286 | 5 | 5.00% Impe | ervious Are | a |
| | | | | | | |
| | Тс | Length | Slope | Velocity | Capacity | Description |
| (m | ıin) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 15 | 5.1 | 100 | 0.0200 | 0.11 | | Sheet Flow, SWALE |
| | | | | | | Grass: Dense n= 0.240 P2= 2.86" |
| 2 | 2.7 | 160 | 0.0200 | 0.99 | | Shallow Concentrated Flow, |
| | | | | | | Short Grass Pasture Kv= 7.0 fps |
| 17 | 7.8 | 260 | Total | | | |

Subcatchment 3S: Runoff to Offsite Wetland (N)



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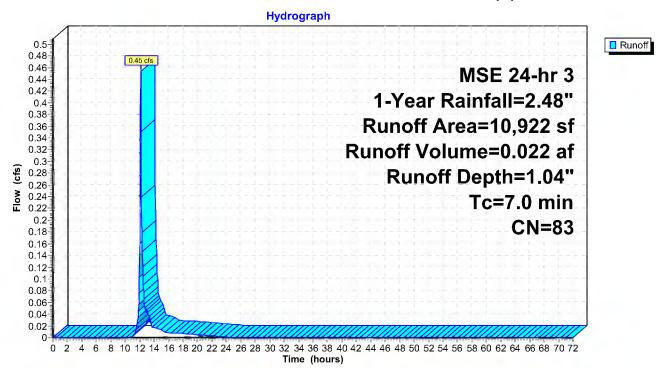
Summary for Subcatchment 4S: Runoff to Wazata Blvd (S)

Runoff = 0.45 cfs @ 12.15 hrs, Volume= 0.022 af, Depth= 1.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | Aı | rea (sf) | CN | Description | | | | |
|-----------|------|-------------|--------|---------------------|-------------|---------------|--|--|
| | | 1,777 | 98 | Paved park | ing, HSG E |) | | |
| | | 9,145 | 80 | >75% Gras | s cover, Go | ood, HSG D | | |
| | | 10,922 | 83 | 83 Weighted Average | | | | |
| | | 9,145 | | 83.73% Per | rvious Area | 1 | | |
| | | 1,777 | | 16.27% Imp | pervious Ar | ea | | |
| | т. | مالايم مريا | Clar. | | 0 | Danamintian | | |
| , | Tc | Length | Slope | • | Capacity | Description | | |
| <u>(r</u> | min) | (feet) | (ft/ft |) (ft/sec) | (cfs) | | | |
| | 7.0 | | | | | Direct Entry. | | |

Subcatchment 4S: Runoff to Wazata Blvd (S)



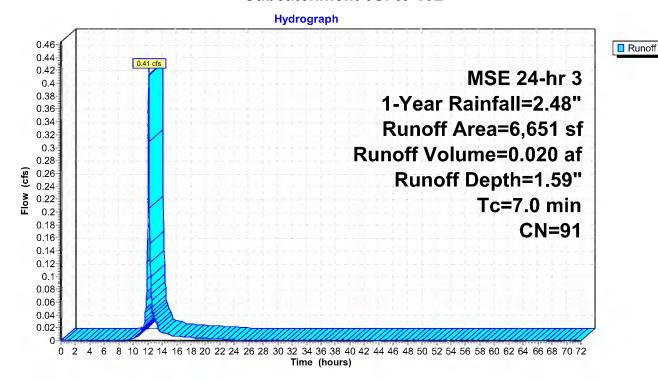
Summary for Subcatchment 5S: to 102

Runoff = 0.41 cfs @ 12.14 hrs, Volume= 0.020 af, Depth= 1.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 1-Year Rainfall=2.48"

| | rea (sf) | CN | Description | | | | |
|-------|----------|---------|----------------------|-------------|--------------|--|--|
| | 4,143 | 98 | Paved park | ing, HSG E |) | | |
| | 2,508 | 80 | >75% Ġras | s cover, Go | ood, HSG D | | |
| | 6,651 | 91 | Weighted Average | | | | |
| | 2,508 | | 37.71% Pervious Area | | | | |
| | 4,143 | | 62.29% lmp | pervious Ar | rea | | |
| Тс | Length | Slope | Velocity | Capacity | Description | | |
| | | | • | | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry | | |

Subcatchment 5S: to 102



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Summary for Reach 3R: total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

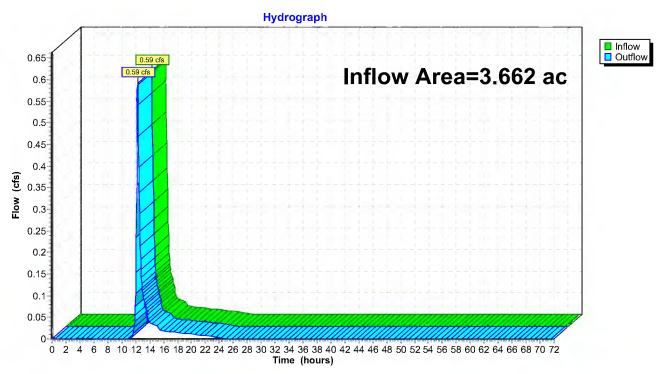
Inflow Area = 3.662 ac, 52.96% Impervious, Inflow Depth = 0.14" for 1-Year event

Inflow = 0.59 cfs @ 12.28 hrs, Volume= 0.043 af

Outflow = 0.59 cfs @ 12.28 hrs, Volume= 0.043 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 3R: total to offsite wetland



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Summary for Reach 4R: total proposed

[40] Hint: Not Described (Outflow=Inflow)

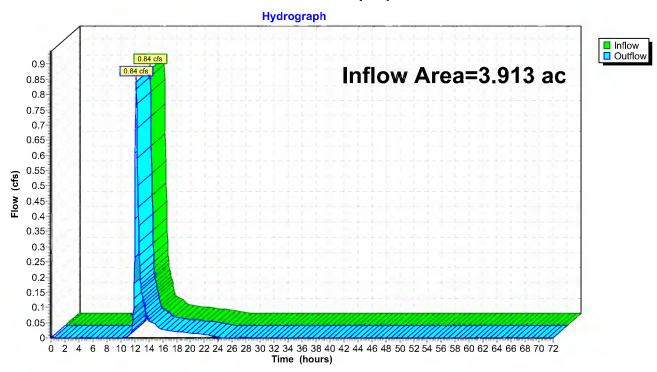
Inflow Area = 3.913 ac, 50.61% Impervious, Inflow Depth = 0.20" for 1-Year event

Inflow = 0.84 cfs @ 12.20 hrs, Volume= 0.065 af

Outflow = 0.84 cfs @ 12.20 hrs, Volume= 0.065 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 4R: total proposed



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Summary for Pond 1P: Underground Detention

Inflow Area = 1.834 ac, 95.12% Impervious, Inflow Depth = 2.14" for 1-Year event

6.15 cfs @ 12.14 hrs, Volume= Inflow 0.328 af

Outflow 0.48 cfs @ 12.05 hrs, Volume= 0.328 af, Atten= 92%, Lag= 0.0 min

Primary 0.48 cfs @ 12.05 hrs, Volume= 0.328 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 926.39' @ 12.91 hrs Surf.Area= 3,774 sf Storage= 7,086 cf

Flood Elev= 926.76' Surf.Area= 3,774 sf Storage= 7,920 cf

Plug-Flow detention time= 128.2 min calculated for 0.327 af (100% of inflow)

Center-of-Mass det. time= 128.2 min (893.6 - 765.3)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1A | 922.50' | 0 cf | 37.00'W x 102.00'L x 6.00'H Field A |
| | | | 22,644 cf Overall - 9,817 cf Embedded = 12,827 cf x 0.0% Voids |
| #2A | 923.00' | 9,817 cf | CMP Round 60 x 25 Inside #1 |
| | | | Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf |
| | | | Overall Size= 60.0"W x 60.0"H x 20.00'L |
| | | | 25 Chambers in 5 Rows |
| #3 | 928.00' | 137 cf | riser storage (Prismatic)Listed below (Recalc) |
| | | 9,954 cf | Total Available Storage |

Storage Group A created with Chamber Wizard

| Elevation | Surf.Area | Inc.Store | Cum.Store |
|-----------|-----------|--------------|--------------|
| (feet) | (sq-ft) | (cubic-feet) | (cubic-feet) |
| 928.00 | 65 | 0 | 0 |
| 930.10 | 65 | 137 | 137 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 920.70' | 24.0" Round device outlet L= 108.0' Ke= 0.900 |
| | • | | Inlet / Outlet Invert= 920.70' / 920.17' S= 0.0049 '/' Cc= 0.900 |
| | | | n= 0.011, Flow Area= 3.14 sf |
| #2 | Device 1 | 923.00' | 0.480 cfs 18" phospho, 14 cartridge |
| #3 | Device 2 | 923.00' | 4.0" Vert. device inlet C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 926.76' | 4.0' long device bypass weir 2 End Contraction(s) |

Primary OutFlow Max=0.48 cfs @ 12.05 hrs HW=924.58' TW=920.32' (Dynamic Tailwater)

-1=device outlet (Passes 0.48 cfs of 20.26 cfs potential flow)

-2=18" phospho, 14 cartridge (Constant Controls 0.48 cfs)
-3=device inlet (Passes 0.48 cfs of 0.50 cfs potential flow)

-4=device bypass weir (Controls 0.00 cfs)

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Pond 1P: Underground Detention - Chamber Wizard Field A

Chamber Model = CMP Round 60 (Round Corrugated Metal Pipe)

Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf Overall Size= 60.0"W x 60.0"H x 20.00'L

60.0" Wide + 30.0" Spacing = 90.0" C-C Row Spacing

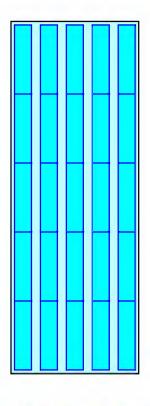
5 Chambers/Row x 20.00' Long = 100.00' Row Length +12.0" End Stone x 2 = 102.00' Base Length 5 Rows x 60.0" Wide + 30.0" Spacing x 4 + 12.0" Side Stone x 2 = 37.00' Base Width 6.0" Stone Base + 60.0" Chamber Height + 6.0" Stone Cover = 6.00' Field Height

25 Chambers x 392.7 cf = 9,817.5 cf Chamber Storage

22,644.0 cf Field - 9,817.5 cf Chambers = 12,826.5 cf Stone x 0.0% Voids = 0.0 cf Stone Storage

Chamber Storage = 9,817.5 cf = 0.225 af Overall Storage Efficiency = 43.4% Overall System Size = 102.00' x 37.00' x 6.00'

25 Chambers 838.7 cy Field 475.1 cy Stone

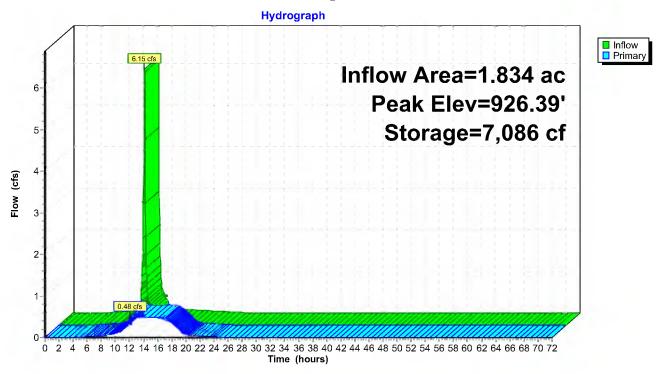




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Pond 1P: Underground Detention



Stage-Area-Storage for Pond 1P: Underground Detention

Storage (cubic-feet)

9,450

9,577

9,686

9,770 9,817

9,824

9,830

9,837

9,843

9,850 9,856

9,863

9,869

9,876 9,882

9,889

9,895

9,902

9,908

9,915 9,921

9,928

9,934 9,941

9,947

9,954

| Elevation | Storage | Elevation |
|------------------|----------------|------------------|
| (feet) | (cubic-feet) | (feet) |
| 922.50 | 0 | 927.60 |
| 922.60 | 0 | 927.70 |
| 922.70 | 0 | 927.80 |
| 922.80 | 0 | 927.90 |
| 922.90 | 0 | 928.00 |
| 923.00 | 0 | 928.10 |
| 923.10 | 47 | 928.20 |
| 923.20 | 132 | 928.30 |
| 923.30 | 240 368 | 928.40 |
| 923.40 923.50 | 511 | 928.50 928.60 |
| 923.60 | 667 | 928.70 |
| 923.70 | 835 | 928.80 |
| 923.80 | 1,014 | 928.90 |
| 923.90 | 1,202 | 929.00 |
| 924.00 | 1,398 | 929.10 |
| 924.10 | 1,601 | 929.20 |
| 924.20 | 1,812 | 929.30 |
| 924.30 | 2,028 | 929.40 |
| 924.40 | 2,250 | 929.50 |
| 924.50 | 2,477 | 929.60 |
| 924.60 | 2,708 | 929.70 |
| 924.70 | 2,943 | 929.80 |
| 924.80 | 3,182 | 929.90 |
| 924.90 925.00 | 3,423 3,667 | 930.00 930.10 |
| 925.10 | 3,913 | 930.10 |
| 925.20 | 4,161 | |
| 925.30 | 4,409 | |
| 925.40 | 4,659 | |
| 925.50 | 4,909 | |
| 925.60 | 5,159 | |
| 925.70 | 5,408 | |
| 925.80 | 5,657 | |
| 925.90 | 5,904 | |
| 926.00 | 6,150 | |
| 926.10 | 6,394 | |
| 926.20 926.30 | 6,636 6,874 | |
| 926.40 | 7,109 | |
| 926.50 | 7,103 | |
| 926.60 | 7,567 | |
| 926.70 | 7,789 | |
| 926.80 | 8,006 | |
| 926.90 | 8,216 | |
| 927.00 | 8,420 | |
| 927.10 | 8,616 | |
| 927.20 | 8,804 | |
| 927.30 | 8,982 | |
| 927.40 | 9,150 | |
| 927.50 | 9,307 | |

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Summary for Pond 102: stmh 102

[57] Hint: Peaked at 920.37' (Flood elevation advised)

Inflow Area = 1.987 ac, 92.60% Impervious, Inflow Depth = 2.10" for 1-Year event

Inflow = 0.89 cfs @ 12.14 hrs, Volume= 0.348 af

Outflow = 0.89 cfs @ 12.14 hrs, Volume= 0.348 af, Atten= 0%, Lag= 0.0 min

Primary = 0.89 cfs @ 12.14 hrs, Volume= 0.348 af

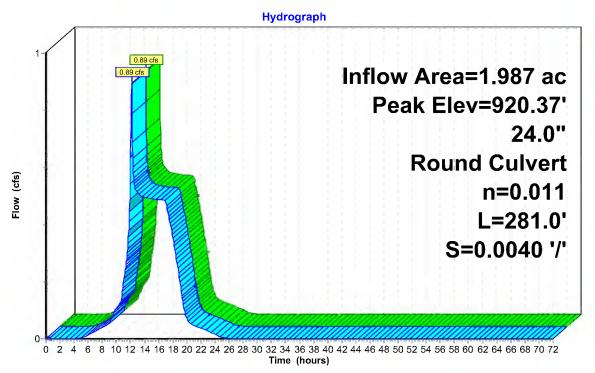
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 920.37' @ 12.14 hrs

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|---|
| #1 | Primary | 919.93' | 24.0" Round Culvert L= 281.0' Ke= 0.900 Inlet / Outlet Invert= 919.93' / 918.80' S= 0.0040 '/' Cc= 0.900 |
| | | | n= 0.011, Flow Area= 3.14 sf |

Primary OutFlow Max=0.88 cfs @ 12.14 hrs HW=920.36' TW=916.17' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.88 cfs @ 1.77 fps)

Pond 102: stmh 102





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Stage-Area-Storage for Pond 102: stmh 102

| Elevation | Storage | Elevation | Storage |
|------------------|----------------|------------------|----------------|
| (feet) | (acre-feet) | (feet) | (acre-feet) |
| 919.93 | 0.000 | 920.95 | 0.000 |
| 919.95 | 0.000 | 920.97 | 0.000 |
| 919.97 | 0.000 | 920.99 | 0.000 |
| 919.99 | 0.000 | 921.01 | 0.000 |
| 920.01 | 0.000 | 921.03 | 0.000 |
| 920.03 | 0.000 | 921.05 | 0.000 |
| 920.05 | 0.000 | 921.07 | 0.000 |
| 920.07 | 0.000 | 921.09 | 0.000 |
| 920.09 | 0.000 | 921.11 | 0.000 |
| 920.11 | 0.000 | 921.13 | 0.000 |
| 920.13 920.15 | 0.000 0.000 | 921.15 921.17 | 0.000 0.000 |
| 920.13 | 0.000 | 921.17 | 0.000 |
| 920.17 | 0.000 | 921.13 | 0.000 |
| 920.21 | 0.000 | 921.23 | 0.000 |
| 920.23 | 0.000 | 921.25 | 0.000 |
| 920.25 | 0.000 | 921.27 | 0.000 |
| 920.27 | 0.000 | 921.29 | 0.000 |
| 920.29 | 0.000 | 921.31 | 0.000 |
| 920.31 | 0.000 | 921.33 | 0.000 |
| 920.33 | 0.000 | 921.35 | 0.000 |
| 920.35 | 0.000 | 921.37 | 0.000 |
| 920.37 | 0.000 | 921.39 | 0.000 |
| 920.39 | 0.000 | 921.41 | 0.000 |
| 920.41 | 0.000 | 921.43 921.45 | 0.000 |
| 920.43 920.45 | 0.000 0.000 | 921.45 921.47 | 0.000 0.000 |
| 920.43 | 0.000 | 921.47 | 0.000 |
| 920.49 | 0.000 | 921.51 | 0.000 |
| 920.51 | 0.000 | 921.53 | 0.000 |
| 920.53 | 0.000 | 921.55 | 0.000 |
| 920.55 | 0.000 | 921.57 | 0.000 |
| 920.57 | 0.000 | 921.59 | 0.000 |
| 920.59 | 0.000 | 921.61 | 0.000 |
| 920.61 | 0.000 | 921.63 | 0.000 |
| 920.63 | 0.000 | 921.65 | 0.000 |
| 920.65 | 0.000 | 921.67 | 0.000 |
| 920.67 | 0.000 | 921.69 921.71 | 0.000 |
| 920.69 920.71 | 0.000 0.000 | 921.71 | 0.000 0.000 |
| 920.71 | 0.000 | 921.75 | 0.000 |
| 920.75 | 0.000 | 921.77 | 0.000 |
| 920.77 | 0.000 | 921.79 | 0.000 |
| 920.79 | 0.000 | 921.81 | 0.000 |
| 920.81 | 0.000 | 921.83 | 0.000 |
| 920.83 | 0.000 | 921.85 | 0.000 |
| 920.85 | 0.000 | 921.87 | 0.000 |
| 920.87 | 0.000 | 921.89 | 0.000 |
| 920.89 | 0.000 | 921.91 | 0.000 |
| 920.91 | 0.000 | 921.93 | 0.000 |
| 920.93 | 0.000 | | |

Volume

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Summary for Pond Wtld Prd: Existing Wetland

Inflow Area = 3.072 ac, 62.17% Impervious, Inflow Depth = 1.69" for 1-Year event

Inflow = 2.64 cfs @ 12.15 hrs, Volume= 0.432 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 916.83' @ 37.35 hrs Surf.Area= 23,693 sf Storage= 18,813 cf

Avail.Storage Storage Description

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Invert

| VOIGITIC | 111401 | 7 | rage Clorage B | Coonplion | | |
|-----------|----------|---|--------------------|-------------------|-----------------------|-----------|
| #1 | 916.00 | 0' 76,78 | 34 cf Custom S | Stage Data (Pris | smatic)Listed below (| (Recalc) |
| Elevation | on S | Surf.Area | Inc.Store | Cum.Store | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | |
| Device | Routing | Invert | Outlet Devices | | | |
| #1 | Primary | 916.35' | 15.0" Round o | ocs outlet L= 18 | 3.0' Ke= 0.900 | |
| | • | | Inlet / Outlet Inv | vert= 916.35' / 9 | 16.22' S= 0.0072 '/' | Cc= 0.900 |
| | | | n= 0.010, Flow | / Area= 1.23 sf | | |
| #2 | Device 1 | 918.08' | 4.0' long ocs v | veir wall 2 End | Contraction(s) | |
| #3 | Device 2 | 917.07' | 15.0" Round o | ocs inlet L= 12. | 0' Ke= 0.900 | |
| | | | Inlet / Outlet Inv | vert= 917.07' / 9 | 16.39' S= 0.0567 '/' | Cc= 0.900 |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

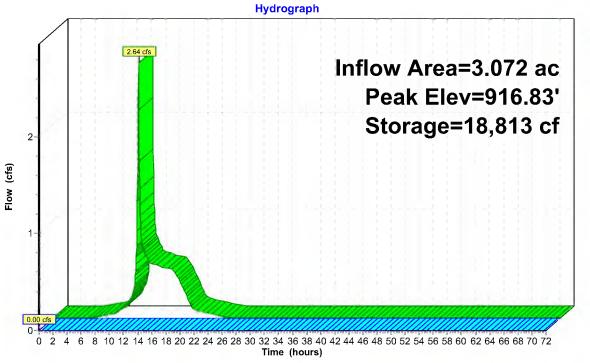
1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs)
-3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Prd: Existing Wetland





Storage

63,564

65,000

66,444

67,897

69,357 70,826

72,303 73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Prd: Existing Wetland

Elevation

(feet)

918.55

918.60

918.65

918.70

918.75

918.80 918.85

918.90

918.95

919.00

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| Elevation | Surface | Storage |
|-----------|---------|--------------|
| (feet) | (sq-ft) | (cubic-feet) |
| 916.00 | 21,538 | 0 |
| 916.05 | 21,667 | 1,080 |
| 916.10 | 21,797 | 2,167 |
| 916.15 | 21,926 | 3,260 |
| 916.20 | 22,056 | 4,359 |
| 916.25 | 22,186 | 5,465 |
| 916.30 | 22,315 | 6,578 |
| 916.35 | 22,445 | 7,697 |
| 916.40 | 22,574 | 8,822 |
| 916.45 | 22,704 | 9,954 |
| 916.50 | 22,833 | 11,093 |
| 916.55 | 22,962 | 12,238 |
| 916.60 | 23,092 | 13,389 |
| 916.65 | 23,221 | 14,547 |
| 916.70 | 23,351 | 15,711 |
| 916.75 | 23,481 | 16,882 |
| 916.80 | 23,610 | 18,059 |
| 916.85 | 23,740 | 19,243 |
| 916.90 | 23,869 | 20,433 |
| 916.95 | 23,999 | 21,630 |
| 917.00 | 24,128 | 22,833 |
| 917.05 | 24,263 | 24,043 |
| 917.10 | 24,398 | 25,259 |
| 917.15 | 24,533 | 26,483 |
| 917.20 | 24,668 | 27,713 |
| 917.25 | 24,803 | 28,949 |
| 917.30 | 24,938 | 30,193 |
| 917.35 | 25,073 | 31,443 |
| 917.40 | 25,208 | 32,700 |
| 917.45 | 25,343 | 33,964 |
| 917.50 | 25,478 | 35,235 |
| 917.55 | 25,613 | 36,512 |
| 917.60 | 25,748 | 37,796 |
| 917.65 | 25,883 | 39,087 |
| 917.70 | 26,018 | 40,384 |
| 917.75 | 26,153 | 41,688 |
| 917.80 | 26,288 | 42,999 |
| 917.85 | 26,423 | 44,317 |
| 917.90 | 26,558 | 45,642 |
| 917.95 | 26,693 | 46,973 |
| 918.00 | 26,828 | 48,311 |
| 918.05 | 26,992 | 49,657 |
| 918.10 | 27,157 | 51,010 |
| 918.15 | 27,321 | 52,372 |
| 918.20 | 27,486 | 53,742 |
| 918.25 | 27,651 | 55,121 |
| 918.30 | 27,815 | 56,507 |
| 918.35 | 27,980 | 57,902 |
| 918.40 | 28,144 | 59,305 |
| 918.45 | 28,309 | 60,717 |
| 918.50 | 28,473 | 62,136 |

Proposed MSE 24-hr 3 2-Year Rainfall=2.86"
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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To site sewer Runoff Area=79,886 sf 95.12% Impervious Runoff Depth=2.52"

Tc=7.0 min CN=97 Runoff=7.15 cfs 0.385 af

Subcatchment2S: Direct to wetland Runoff Area=47,288 sf 6.48% Impervious Runoff Depth=1.21"

Tc=7.0 min CN=81 Runoff=2.28 cfs 0.109 af

Subcatchment3S: Runoff to Offsite Runoff Area=25,698 sf 5.00% Impervious Runoff Depth=1.15"

Flow Length=260' Slope=0.0200 '/' Tc=17.8 min CN=80 Runoff=0.79 cfs 0.056 af

Subcatchment4S: Runoff to Wazata Blvd Runoff Area=10,922 sf 16.27% Impervious Runoff Depth=1.33"

Tc=7.0 min CN=83 Runoff=0.58 cfs 0.028 af

Subcatchment5S: to 102 Runoff Area=6,651 sf 62.29% Impervious Runoff Depth=1.94"

Tc=7.0 min CN=91 Runoff=0.50 cfs 0.025 af

Reach 3R: total to offsite wetland Inflow=0.79 cfs 0.056 af

Outflow=0.79 cfs 0.056 af

Reach 4R: total proposed Inflow=1.11 cfs 0.084 af

Outflow=1.11 cfs 0.084 af

Pond 1P: Underground Detention Peak Elev=926.88' Storage=8,173 cf Inflow=7.15 cfs 0.385 af

Outflow=1.02 cfs 0.385 af

Pond 102: stmh 102 Peak Elev=920.41' Inflow=1.09 cfs 0.410 af

24.0" Round Culvert n=0.011 L=281.0' S=0.0040 '/' Outflow=1.09 cfs 0.410 af

Pond Wtld Prd: Existing Wetland Peak Elev=916.99' Storage=22,605 cf Inflow=3.26 cfs 0.519 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.913 ac Runoff Volume = 0.603 af Average Runoff Depth = 1.85" 49.39% Pervious = 1.933 ac 50.61% Impervious = 1.980 ac

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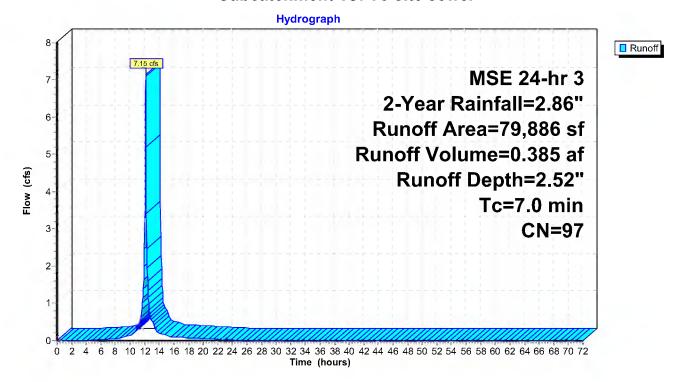
Summary for Subcatchment 1S: To site sewer

Runoff = 7.15 cfs @ 12.14 hrs, Volume= 0.385 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| | Α | rea (sf) | CN | Description | | | | |
|---|-------|----------|---------|-------------------------------|----------|--------------|--|--|
| - | | 75,991 | 98 | Paved parking, HSG D | | | | |
| | | 3,895 | 80 | >75% Grass cover, Good, HSG D | | | | |
| - | | 79,886 | 97 | Weighted Average | | | | |
| | | 3,895 | | 4.88% Pervious Area | | | | |
| | | 75,991 | | 95.12% Impervious Area | | | | |
| | _ | | | | | | | |
| | Тс | Length | Slope | - | Capacity | Description | | |
| | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| | 7.0 | | | | | Direct Entry | | |

Subcatchment 1S: To site sewer



Page 27

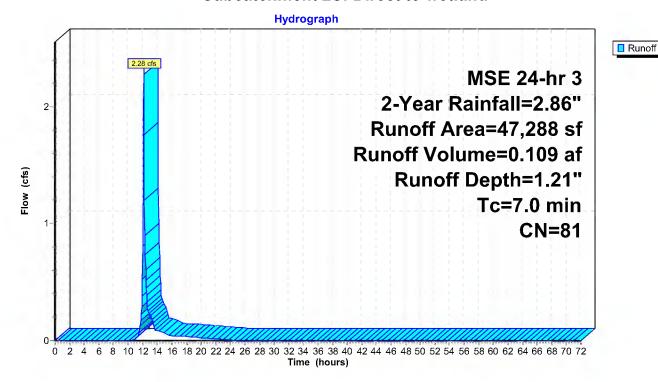
Summary for Subcatchment 2S: Direct to wetland

Runoff = 2.28 cfs @ 12.15 hrs, Volume= 0.109 af, Depth= 1.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| A | rea (sf) | CN | Description | | |
|-------------|------------------|------------------|-------------|-------------------|---|
| | 3,064 | 98 | Paved park | ing, HSG D |) |
| | 44,224 | 80 | >75% Gras | s cover, Go | ood, HSG D |
| | 47,288 | 81 | Weighted A | verage | |
| | 44,224 | | 93.52% Pei | vious Area | a e e e e e e e e e e e e e e e e e e e |
| | 3,064 | | 6.48% Impe | ervious Are | ea |
| Tc (min) | Length (feet) | Slope (ft/ft) | • | Capacity (cfs) | Description |
| 7.0 | | | | | Direct Entry, |

Subcatchment 2S: Direct to wetland



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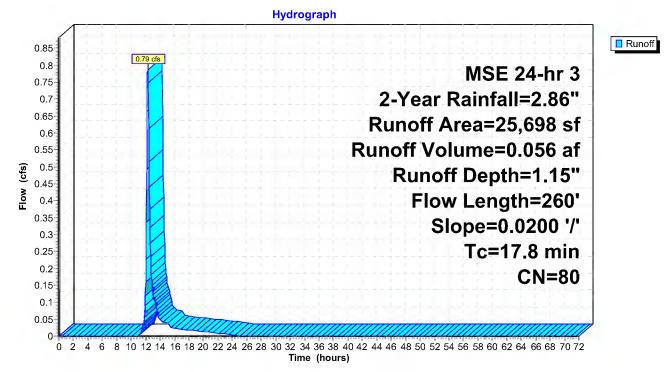
Summary for Subcatchment 3S: Runoff to Offsite Wetland (N)

Runoff = 0.79 cfs @ 12.28 hrs, Volume= 0.056 af, Depth= 1.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| | Α | rea (sf) | CN E | Description | | |
|----------------------------|-------------------------------|----------|---------|-------------|-------------|---------------------------------|
| | 1,286 98 Paved parking, HSG D | | | | | |
| | | 24,412 | 79 V | Voods/gras | s comb., C | Good, HSG D |
| 25,698 80 Weighted Average | | | | | | |
| | 24,412 95.00% Pervious Area | | | | | |
| | | 1,286 | 5 | .00% Impe | ervious Are | a |
| | | | | | _ | |
| | Tc | Length | Slope | Velocity | Capacity | Description |
| _ | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| | 15.1 | 100 | 0.0200 | 0.11 | | Sheet Flow, SWALE |
| | | | | | | Grass: Dense n= 0.240 P2= 2.86" |
| | 2.7 | 160 | 0.0200 | 0.99 | | Shallow Concentrated Flow, |
| _ | | | | | | Short Grass Pasture Kv= 7.0 fps |
| | 17.8 | 260 | Total | | | |

Subcatchment 3S: Runoff to Offsite Wetland (N)



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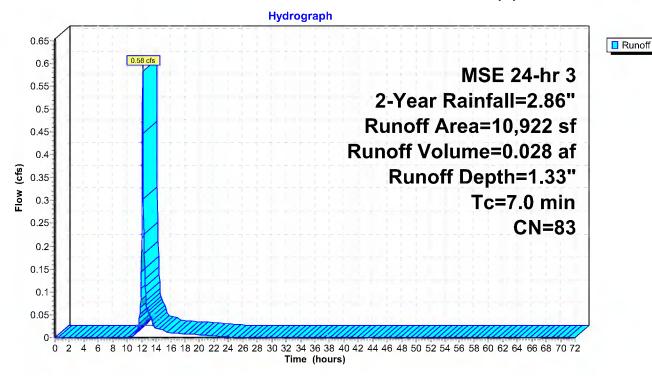
Summary for Subcatchment 4S: Runoff to Wazata Blvd (S)

Runoff = 0.58 cfs @ 12.15 hrs, Volume= 0.028 af, Depth= 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| _ | Α | rea (sf) | CN | Description | | | | |
|---|-------|----------|---------|-------------------------------|------------|---------------|--|--|
| _ | | 1,777 | 98 | Paved parking, HSG D | | | | |
| _ | | 9,145 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | | 10,922 | 83 | 83 Weighted Average | | | | |
| | | 9,145 | | 83.73% Pei | vious Area | 1 | | |
| | | 1,777 | | 16.27% Impervious Area | | | | |
| | _ | | O. | N/ 1 '1 | 0 " | D : 0 | | |
| | Tc | Length | Slope | _ | Capacity | Description | | |
| _ | (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| | 7.0 | | | | | Direct Entry. | | |

Subcatchment 4S: Runoff to Wazata Blvd (S)



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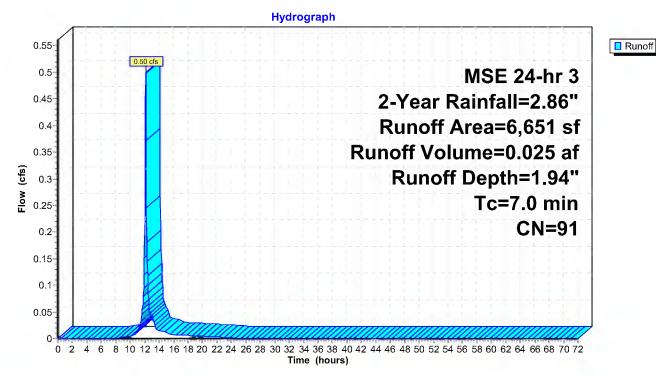
Summary for Subcatchment 5S: to 102

Runoff = 0.50 cfs @ 12.14 hrs, Volume= 0.025 af, Depth= 1.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 2-Year Rainfall=2.86"

| | rea (sf) | CN | Description | | | | |
|-------|----------|---------|-------------------------------|----------|--------------|--|--|
| | 4,143 | 98 | Paved parking, HSG D | | | | |
| | 2,508 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | 6,651 | 91 | Weighted Average | | | | |
| | 2,508 | | 37.71% Pervious Area | | | | |
| | 4,143 | | 62.29% Impervious Area | | | | |
| Tc | Length | Slope | e Velocity | Capacity | Description | | |
| | | | • | | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry | | |

Subcatchment 5S: to 102



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Summary for Reach 3R: total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

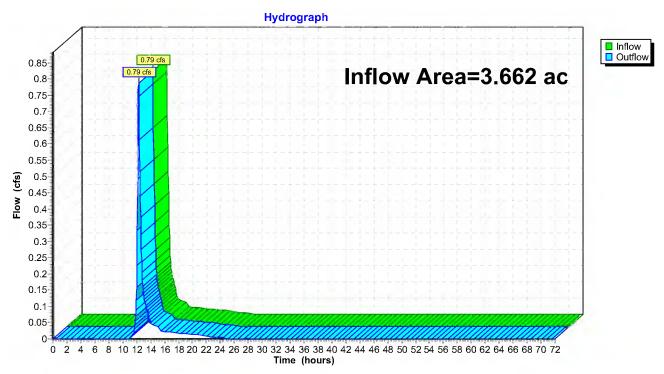
Inflow Area = 3.662 ac, 52.96% Impervious, Inflow Depth = 0.18" for 2-Year event

Inflow = 0.79 cfs @ 12.28 hrs, Volume= 0.056 af

Outflow = 0.79 cfs @ 12.28 hrs, Volume= 0.056 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 3R: total to offsite wetland



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Summary for Reach 4R: total proposed

[40] Hint: Not Described (Outflow=Inflow)

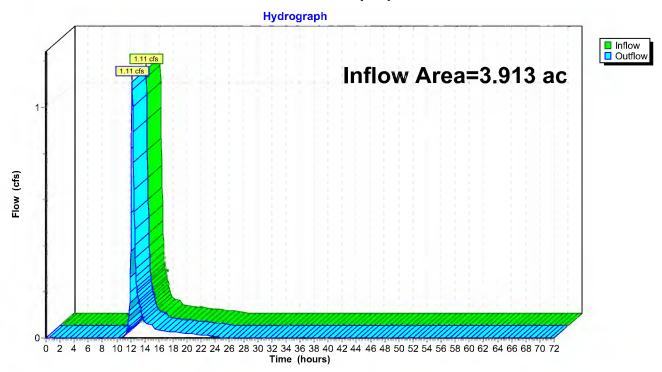
Inflow Area = 3.913 ac, 50.61% Impervious, Inflow Depth = 0.26" for 2-Year event

Inflow = 1.11 cfs @ 12.20 hrs, Volume= 0.084 af

Outflow = 1.11 cfs @ 12.20 hrs, Volume= 0.084 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 4R: total proposed



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Summary for Pond 1P: Underground Detention

[58] Hint: Peaked 0.12' above defined flood level

Inflow Area = 1.834 ac, 95.12% Impervious, Inflow Depth = 2.52" for 2-Year event

Inflow = 7.15 cfs @ 12.14 hrs, Volume= 0.385 af

Outflow = 1.02 cfs @ 12.55 hrs, Volume= 0.385 af, Atten= 86%, Lag= 24.5 min

Primary = 1.02 cfs @ 12.55 hrs, Volume= 0.385 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 926.88' @ 12.55 hrs Surf.Area= 3,774 sf Storage= 8,173 cf

Flood Elev= 926.76' Surf.Area= 3,774 sf Storage= 7,920 cf

Plug-Flow detention time= 138.9 min calculated for 0.385 af (100% of inflow)

Center-of-Mass det. time= 138.6 min (901.0 - 762.4)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1A | 922.50' | 0 cf | 37.00'W x 102.00'L x 6.00'H Field A |
| | | | 22,644 cf Overall - 9,817 cf Embedded = 12,827 cf x 0.0% Voids |
| #2A | 923.00' | 9,817 cf | CMP Round 60 x 25 Inside #1 |
| | | | Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf |
| | | | Overall Size= 60.0"W x 60.0"H x 20.00'L |
| | | | 25 Chambers in 5 Rows |
| #3 | 928.00' | 137 cf | riser storage (Prismatic)Listed below (Recalc) |
| | | | |

9,954 cf Total Available Storage

Storage Group A created with Chamber Wizard

| Elevation | Surf.Area | Inc.Store | Cum.Store |
|-----------|-----------|--------------|--------------|
| (feet) | (sq-ft) | (cubic-feet) | (cubic-feet) |
| 928.00 | 65 | 0 | 0 |
| 930.10 | 65 | 137 | 137 |
| | | | |

| Device | Routing | Invert | Outlet Devices | | |
|--------|----------|---------|---|--|--|
| #1 | Primary | 920.70' | 24.0" Round device outlet L= 108.0' Ke= 0.900 | | |
| | - | | Inlet / Outlet Invert= 920.70' / 920.17' S= 0.0049 '/' Cc= 0.900 | | |
| | | | n= 0.011, Flow Area= 3.14 sf | | |
| #2 | Device 1 | 923.00' | 0.480 cfs 18" phospho, 14 cartridge | | |
| #3 | Device 2 | 923.00' | 4.0" Vert. device inlet C= 0.600 Limited to weir flow at low heads | | |
| #4 | Device 1 | 926.76' | 4.0' long device bypass weir 2 End Contraction(s) | | |

Primary OutFlow Max=1.01 cfs @ 12.55 hrs HW=926.88' TW=920.41' (Dynamic Tailwater)

1=device outlet (Passes 1.01 cfs of 27.18 cfs potential flow)

-2=18" phospho, 14 cartridge (Constant Controls 0.48 cfs)

3=device inlet (Passes 0.48 cfs of 0.81 cfs potential flow)

-4=device bypass weir (Weir Controls 0.53 cfs @ 1.13 fps)

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Pond 1P: Underground Detention - Chamber Wizard Field A

Chamber Model = CMP Round 60 (Round Corrugated Metal Pipe)

Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf Overall Size= 60.0"W x 60.0"H x 20.00'L

60.0" Wide + 30.0" Spacing = 90.0" C-C Row Spacing

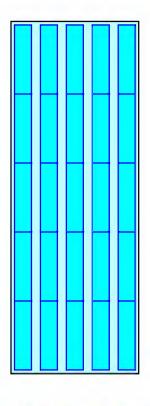
5 Chambers/Row x 20.00' Long = 100.00' Row Length +12.0" End Stone x 2 = 102.00' Base Length 5 Rows x 60.0" Wide + 30.0" Spacing x 4 + 12.0" Side Stone x 2 = 37.00' Base Width 6.0" Stone Base + 60.0" Chamber Height + 6.0" Stone Cover = 6.00' Field Height

25 Chambers x 392.7 cf = 9,817.5 cf Chamber Storage

22,644.0 cf Field - 9,817.5 cf Chambers = 12,826.5 cf Stone x 0.0% Voids = 0.0 cf Stone Storage

Chamber Storage = 9,817.5 cf = 0.225 af Overall Storage Efficiency = 43.4% Overall System Size = 102.00' x 37.00' x 6.00'

25 Chambers 838.7 cy Field 475.1 cy Stone

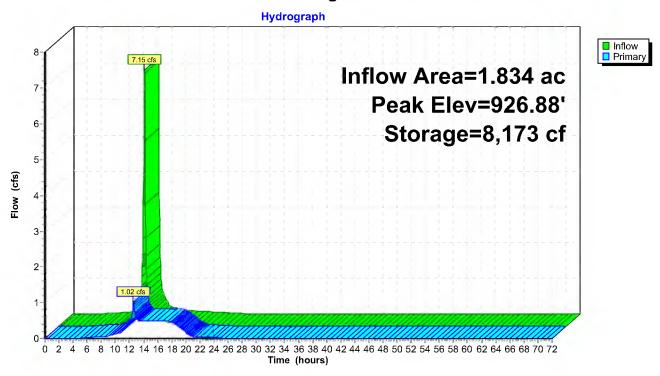




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Pond 1P: Underground Detention



Stage-Area-Storage for Pond 1P: Underground Detention

Storage (cubic-feet)

9,450 9,577

9,686

9,770

9,817 9,824

9,830

9,837

9,843

9,850 9,856

9,863

9,869

9,876 9,882

9,889

9,895

9,902

9,908

9,915

9,921 9,928

9,934 9,941

9,947

9,954

| Elevation | Storage (subjects) | Elevation |
|------------------|--------------------|------------------|
| (feet) 922.50 | (cubic-feet) 0 | (feet) 927.60 |
| 922.60 | 0 | 927.70 |
| 922.70 922.80 | 0 | 927.80 927.90 |
| 922.90 | 0 | 928.00 |
| 923.00 923.10 | 0 47 | 928.10 928.20 |
| 923.10 | 132 | 928.30 |
| 923.30 | 240 | 928.40 |
| 923.40 923.50 | 368 511 | 928.50 928.60 |
| 923.60 | 667 | 928.70 |
| 923.70 923.80 | 835 1,014 | 928.80 928.90 |
| 923.90 | 1,202 | 929.00 |
| 924.00 924.10 | 1,398 1,601 | 929.10 929.20 |
| 924.20 | 1,812 | 929.30 |
| 924.30 924.40 | 2,028 2,250 | 929.40 929.50 |
| 924.50 | 2,250 2,477 | 929.60 |
| 924.60 | 2,708 | 929.70 |
| 924.70 924.80 | 2,943 3,182 | 929.80 929.90 |
| 924.90 | 3,423 | 930.00 |
| 925.00 925.10 | 3,667 3,913 | 930.10 |
| 925.20 | 4,161 | |
| 925.30 925.40 | 4,409 4,659 | |
| 925.50 | 4,909 | |
| 925.60 925.70 | 5,159 5,408 | |
| 925.70 925.80 | 5,408 5,657 | |
| 925.90 | 5,904 | |
| 926.00 926.10 | 6,150 6,394 | |
| 926.20 | 6,636 | |
| 926.30 926.40 | 6,874 7,109 | |
| 926.50 | 7,340 | |
| 926.60 926.70 | 7,567 7,789 | |
| 926.80 | 8,006 | |
| 926.90 927.00 | 8,216 8,420 | |
| 927.10 | 8,616 | |
| 927.20 927.30 | 8,804 8,982 | |
| 927.30 927.40 | 8,982 9,150 | |
| 927.50 | 9,307 | |

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Summary for Pond 102: stmh 102

[57] Hint: Peaked at 920.41' (Flood elevation advised)

Inflow Area = 1.987 ac, 92.60% Impervious, Inflow Depth = 2.48" for 2-Year event

Inflow = 1.09 cfs @ 12.54 hrs, Volume= 0.410 af

Outflow = 1.09 cfs @ 12.54 hrs, Volume= 0.410 af, Atten= 0%, Lag= 0.0 min

Primary = 1.09 cfs @ 12.54 hrs, Volume= 0.410 af

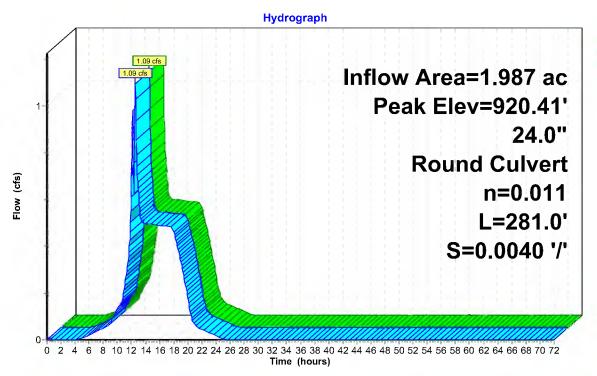
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 920.41' @ 12.54 hrs

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|---|
| #1 | Primary | 919.93' | 24.0" Round Culvert L= 281.0' Ke= 0.900 Inlet / Outlet Invert= 919.93' / 918.80' S= 0.0040 '/' Cc= 0.900 n= 0.011 Flow Area= 3.14 sf |

Primary OutFlow Max=1.08 cfs @ 12.54 hrs HW=920.41' TW=916.32' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.08 cfs @ 1.86 fps)

Pond 102: stmh 102





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Stage-Area-Storage for Pond 102: stmh 102

| Elevation | Storogo | l Elevetion | Storogo |
|------------------|-----------------------------|------------------|------------------------|
| Elevation (feet) | Storage | Elevation | Storage (acre-feet) |
| (feet) 919.93 | (acre-feet) 0.000 | (feet) 920.95 | 0.000 |
| 919.95 | 0.000 | 920.93 | 0.000 |
| 919.97 | 0.000 | 920.97 | 0.000 |
| 919.99 | 0.000 | 920.99 | 0.000 |
| 920.01 | 0.000 | 921.03 | 0.000 |
| 920.03 | 0.000 | 921.05 | 0.000 |
| 920.05 | 0.000 | 921.03 | 0.000 |
| 920.07 | 0.000 | 921.09 | 0.000 |
| 920.09 | 0.000 | 921.11 | 0.000 |
| 920.11 | 0.000 | 921.13 | 0.000 |
| 920.13 | 0.000 | 921.15 | 0.000 |
| 920.15 | 0.000 | 921.17 | 0.000 |
| 920.17 | 0.000 | 921.19 | 0.000 |
| 920.19 | 0.000 | 921.21 | 0.000 |
| 920.21 | 0.000 | 921.23 | 0.000 |
| 920.23 | 0.000 | 921.25 | 0.000 |
| 920.25 | 0.000 | 921.27 | 0.000 |
| 920.27 | 0.000 | 921.29 | 0.000 |
| 920.29 | 0.000 | 921.31 | 0.000 |
| 920.31 | 0.000 | 921.33 | 0.000 |
| 920.33 | 0.000 | 921.35 | 0.000 |
| 920.35 | 0.000 | 921.37 | 0.000 |
| 920.37 | 0.000 | 921.39 | 0.000 |
| 920.39 | 0.000 | 921.41 | 0.000 |
| 920.41 | 0.000 | 921.43 | 0.000 |
| 920.43 | 0.000 | 921.45 | 0.000 |
| 920.45 | 0.000 | 921.47 | 0.000 |
| 920.47 | 0.000 | 921.49 | 0.000 |
| 920.49 | 0.000 | 921.51 | 0.000 |
| 920.51 | 0.000 | 921.53 | 0.000 |
| 920.53 | 0.000 | 921.55 | 0.000 |
| 920.55 920.57 | 0.000 0.000 | 921.57 921.59 | 0.000 0.000 |
| 920.59 | 0.000 | 921.61 | 0.000 |
| 920.61 | 0.000 | 921.63 | 0.000 |
| 920.63 | 0.000 | 921.65 | 0.000 |
| 920.65 | 0.000 | 921.67 | 0.000 |
| 920.67 | 0.000 | 921.69 | 0.000 |
| 920.69 | 0.000 | 921.71 | 0.000 |
| 920.71 | 0.000 | 921.73 | 0.000 |
| 920.73 | 0.000 | 921.75 | 0.000 |
| 920.75 | 0.000 | 921.77 | 0.000 |
| 920.77 | 0.000 | 921.79 | 0.000 |
| 920.79 | 0.000 | 921.81 | 0.000 |
| 920.81 | 0.000 | 921.83 | 0.000 |
| 920.83 | 0.000 | 921.85 | 0.000 |
| 920.85 | 0.000 | 921.87 | 0.000 |
| 920.87 | 0.000 | 921.89 | 0.000 |
| 920.89 | 0.000 | 921.91 | 0.000 |
| 920.91 | 0.000 | 921.93 | 0.000 |
| 920.93 | 0.000 | | |
| | | I | |

Volume

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Summary for Pond Wtld Prd: Existing Wetland

Inflow Area = 3.072 ac, 62.17% Impervious, Inflow Depth = 2.03" for 2-Year event

Inflow = 3.26 cfs @ 12.15 hrs, Volume= 0.519 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 916.99' @ 38.25 hrs Surf.Area= 24,104 sf Storage= 22,605 cf

Avail.Storage Storage Description

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Invert

| VOIGITIC | 11110 | 7 | rage Clorage B | Coonplion | | | | |
|---|----------|---|--|-------------------|-----------------------|-----------|--|--|
| #1 | 916.00 | 0' 76,78 | 34 cf Custom S | Stage Data (Pris | smatic)Listed below (| (Recalc) | | |
| Elevation | | Surf.Area | Inc.Store | Cum.Store | | | | |
| (feet) | | (sq-ft) | (cubic-feet) | (cubic-feet) | | | | |
| 916.00 | | 21,538 | 0 | 0 | | | | |
| 917.00 | | 24,128 | 22,833 | 22,833 | | | | |
| 918.00 | | 26,828 | 25,478 | 48,311 | | | | |
| 919.00 | | 30,118 | 28,473 | 76,784 | | | | |
| Device Routing | | Invert | Outlet Devices | | | | | |
| #1 Primary 916.35' 15.0" Rour | | | | ocs outlet L= 18 | 3.0' Ke= 0.900 | | | |
| | • | | Inlet / Outlet Inv | vert= 916.35' / 9 | 16.22' S= 0.0072 '/' | Cc= 0.900 | | |
| | | n= 0.010, Flow Area= 1.23 sf | | | | | | |
| #2 | Device 1 | 918.08' | 918.08' 4.0' long ocs weir wall 2 End Contraction(s) | | | | | |
| #3 Device 2 917.07' 15.0" Round ocs inlet L= 12.0' Ke= 0.900 | | | | | | | | |
| | | | Inlet / Outlet Inv | vert= 917.07' / 9 | 16.39' S= 0.0567 '/' | Cc= 0.900 | | |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

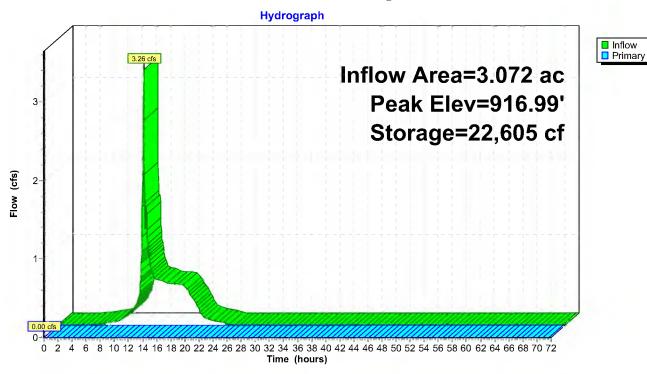
-1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs)
-3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Prd: Existing Wetland



Storage

63,564

65,000

66,444

67,897

69,357 70,826

72,303 73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Prd: Existing Wetland

Elevation

(feet)

918.55

918.60

918.65

918.70

918.75

918.80 918.85

918.90

918.95

919.00

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| | • | • | |
|---------------------|--------------------|-------------------------|--|
| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | |
| 916.00 | 21,538 | 0 | |
| 916.05 | 21,667 | 1,080 | |
| 916.10 | 21,797 | 2,167 | |
| 916.15 | 21,926 | 3,260 | |
| 916.20 | 22,056 | 4,359 | |
| 916.25 | 22,186 | 5,465 | |
| 916.30 | 22,315 | 6,578 | |
| 916.35 | 22,445 | 7,697 | |
| 916.40 | 22,574 | 8,822 | |
| 916.45 | 22,704 | 9,954 | |
| 916.50 | 22,833 | 11,093 | |
| 916.55 | 22,962 | 12,238 | |
| 916.60 | 23,092 | 13,389 | |
| 916.65 | 23,221 | 14,547 | |
| 916.70 | 23,351 | 15,711 | |
| 916.75 916.80 | 23,481 23,610 | 16,882 18,059 | |
| 916.85 | 23,740 | 19,243 | |
| 916.90 | 23,869 | 20,433 | |
| 916.95 | 23,999 | 21,630 | |
| 917.00 | 24,128 | 22,833 | |
| 917.05 | 24,263 | 24,043 | |
| 917.10 | 24,398 | 25,259 | |
| 917.15 | 24,533 | 26,483 | |
| 917.20 | 24,668 | 27,713 | |
| 917.25 | 24,803 | 28,949 | |
| 917.30 | 24,938 | 30,193 | |
| 917.35 | 25,073 | 31,443 | |
| 917.40 | 25,208 | 32,700 | |
| 917.45 | 25,343 | 33,964 | |
| 917.50 | 25,478 | 35,235 | |
| 917.55 917.60 | 25,613 25,748 | 36,512 37,796 | |
| 917.65 | 25,748 25,883 | 39,087 | |
| 917.70 | 26,018 | 40,384 | |
| 917.75 | 26,153 | 41,688 | |
| 917.80 | 26,288 | 42,999 | |
| 917.85 | 26,423 | 44,317 | |
| 917.90 | 26,558 | 45,642 | |
| 917.95 | 26,693 | 46,973 | |
| 918.00 | 26,828 | 48,311 | |
| 918.05 | 26,992 | 49,657 | |
| 918.10 | 27,157 | 51,010 | |
| 918.15 | 27,321 | 52,372 | |
| 918.20 | 27,486 | 53,742 | |
| 918.25 | 27,651 | 55,121 | |
| 918.30 | 27,815 | 56,507 | |
| 918.35 | 27,980 | 57,902 50,305 | |
| 918.40 918.45 | 28,144 28,309 | 59,305 60,717 | |
| 918.50 | 28,473 | 62,136 | |
| 910.30 | 20,413 | 02,130 | |

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To site sewer Runoff Area=79,886 sf 95.12% Impervious Runoff Depth=3.91"

Tc=7.0 min CN=97 Runoff=10.83 cfs 0.598 af

Subcatchment2S: Direct to wetland Runoff Area=47,288 sf 6.48% Impervious Runoff Depth=2.34"

Tc=7.0 min CN=81 Runoff=4.40 cfs 0.212 af

Subcatchment3S: Runoff to Offsite Runoff Area=25,698 sf 5.00% Impervious Runoff Depth=2.26"

Flow Length=260' Slope=0.0200 '/' Tc=17.8 min CN=80 Runoff=1.58 cfs 0.111 af

Subcatchment4S: Runoff to Wazata Blvd Runoff Area=10,922 sf 16.27% Impervious Runoff Depth=2.51"

Tc=7.0 min CN=83 Runoff=1.09 cfs 0.053 af

Subcatchment5S: to 102 Runoff Area=6,651 sf 62.29% Impervious Runoff Depth=3.27"

Tc=7.0 min CN=91 Runoff=0.82 cfs 0.042 af

Reach 3R: total to offsite wetland Inflow=1.58 cfs 0.111 af

Outflow=1.58 cfs 0.111 af

Reach 4R: total proposed Inflow=2.19 cfs 0.164 af

Outflow=2.19 cfs 0.164 af

Pond 1P: Underground Detention Peak Elev=927.49' Storage=9,293 cf Inflow=10.83 cfs 0.598 af

Outflow=8.26 cfs 0.598 af

Pond 102: stmh 102 Peak Elev=921.49' Inflow=8.80 cfs 0.639 af

24.0" Round Culvert n=0.011 L=281.0' S=0.0040 '/' Outflow=8.80 cfs 0.639 af

Pond Wtld Prd: Existing Wetland Peak Elev=917.57' Storage=37,069 cf Inflow=11.92 cfs 0.851 af

Outflow=0.00 cfs 0.000 af

Total Runoff Area = 3.913 ac Runoff Volume = 1.015 af Average Runoff Depth = 3.11" 49.39% Pervious = 1.933 ac 50.61% Impervious = 1.980 ac

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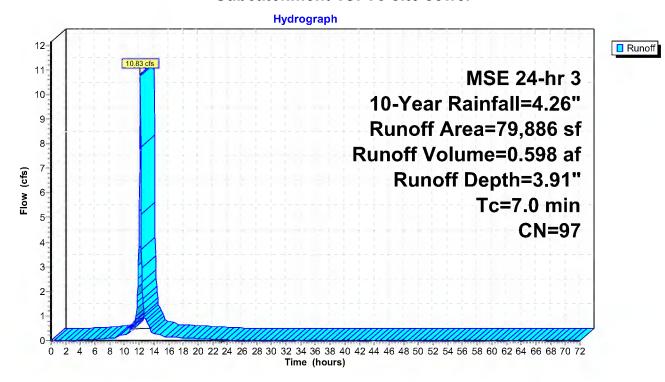
Summary for Subcatchment 1S: To site sewer

Runoff = 10.83 cfs @ 12.14 hrs, Volume= 0.598 af, Depth= 3.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| | Area (sf) | CN | Description | | | | |
|-----------------------------|---------------------------|---------|-------------------------------|-------------|--------------|--|--|
| | 75,991 | 98 | 98 Paved parking, HSG D | | | | |
| | 3,895 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | 79,886 | 97 | Weighted A | verage | | | |
| | 3,895 4.88% Pervious Area | | | | | | |
| 75,991 95.12% Impervious Ar | | | | pervious Ar | rea | | |
| - | | O. | 37.1.20 | 0 " | D | | |
| Tc | | Slope | - | Capacity | · | | |
| <u>(min)</u> | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry | | |

Subcatchment 1S: To site sewer



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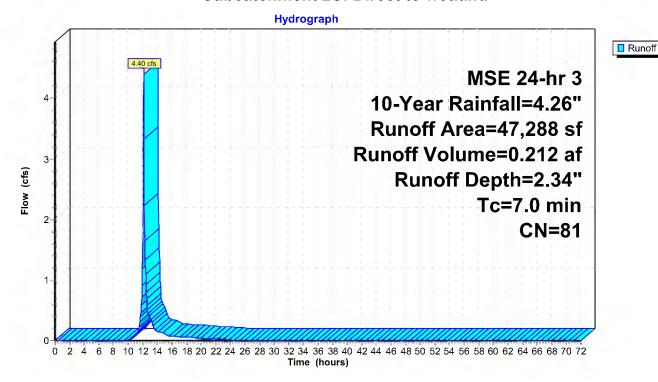
Summary for Subcatchment 2S: Direct to wetland

Runoff = 4.40 cfs @ 12.14 hrs, Volume= 0.212 af, Depth= 2.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| | Area (sf) | CN | Description | | | | |
|-----------------------------|----------------------------|---------|-------------------------------|----------|---------------|--|--|
| | 3,064 | 98 | Paved parking, HSG D | | | | |
| | 44,224 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | 47,288 81 Weighted Average | | | | | | |
| 44,224 93.52% Pervious Area | | | | | | | |
| | 3,064 | | 6.48% Impervious Area | | | | |
| _ | | ٥. | | | | | |
| Tc | | Slope | - | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry. | | |

Subcatchment 2S: Direct to wetland



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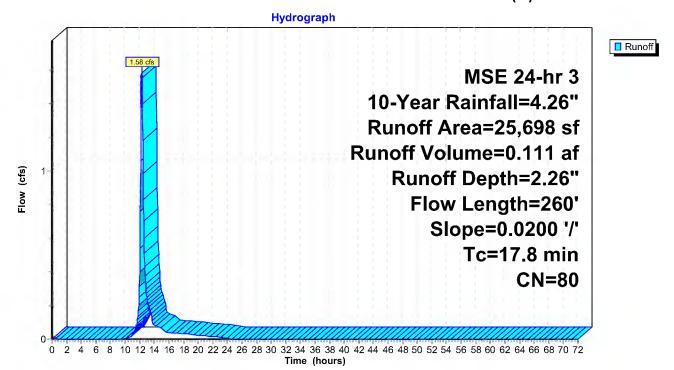
Summary for Subcatchment 3S: Runoff to Offsite Wetland (N)

Runoff = 1.58 cfs @ 12.27 hrs, Volume= 0.111 af, Depth= 2.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| A | rea (sf) | CN E | escription | | | | | |
|--------|----------|---------|-------------------------|-------------|---------------------------------|--|--|--|
| | 1,286 | 98 F | 98 Paved parking, HSG D | | | | | |
| | 24,412 | 79 V | Voods/gras | ss comb., C | Good, HSG D | | | |
| | 25,698 | 80 V | Veighted A | verage | | | | |
| | 24,412 | 9 | 5.00% Per | vious Area | | | | |
| | 1,286 | 5 | .00% Impe | ervious Are | a | | | |
| | | | | | | | | |
| Тс | Length | Slope | Velocity | Capacity | Description | | | |
| (min)_ | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | | |
| 15.1 | 100 | 0.0200 | 0.11 | | Sheet Flow, SWALE | | | |
| | | | | | Grass: Dense n= 0.240 P2= 2.86" | | | |
| 2.7 | 160 | 0.0200 | 0.99 | | Shallow Concentrated Flow, | | | |
| | | | | | Short Grass Pasture Kv= 7.0 fps | | | |
| 17.8 | 260 | Total | | | | | | |

Subcatchment 3S: Runoff to Offsite Wetland (N)



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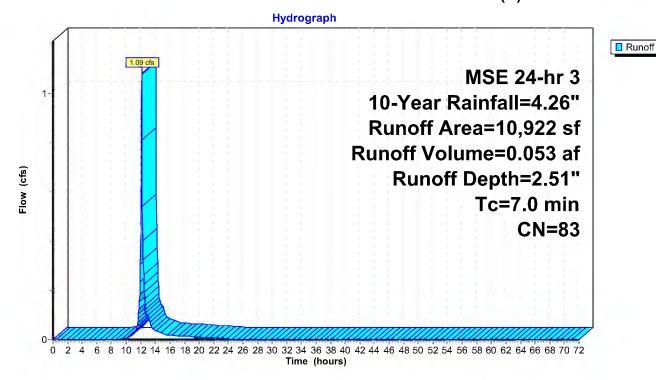
Summary for Subcatchment 4S: Runoff to Wazata Blvd (S)

Runoff = 1.09 cfs @ 12.14 hrs, Volume= 0.053 af, Depth= 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| A | rea (sf) | CN | Description | | | |
|-------------|------------------|------------------|-------------------------------|-------------------|---------------|--|
| | 1,777 | 98 | Paved park | ing, HSG D | D | |
| | 9,145 | 80 | >75% Grass cover, Good, HSG D | | | |
| | 10,922 | 83 | Weighted A | verage | | |
| | 9,145 | | 83.73% Pervious Area | | | |
| | 1,777 | | 16.27% Impervious Area | | | |
| Tc (min) | Length (feet) | Slope (ft/ft) | • | Capacity (cfs) | • | |
| 7.0 | | | | | Direct Entry, | |

Subcatchment 4S: Runoff to Wazata Blvd (S)



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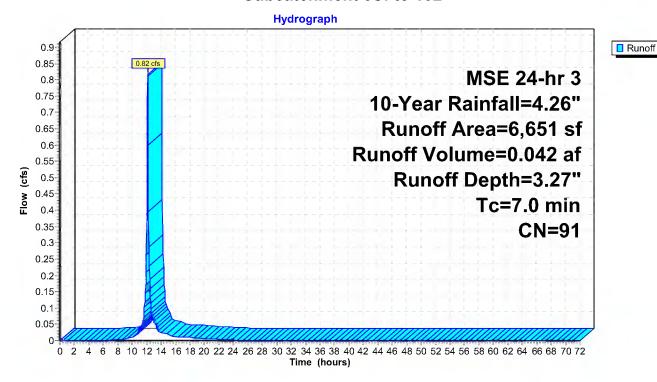
Summary for Subcatchment 5S: to 102

Runoff = 0.82 cfs @ 12.14 hrs, Volume= 0.042 af, Depth= 3.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 10-Year Rainfall=4.26"

| | Ar | ea (sf) | CN | Description | | | | |
|----|------|---------|--------|-------------------------------|-------------|---------------|--|--|
| | | 4,143 | 98 | Paved park | ing, HSG E | | | |
| | | 2,508 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | | 6,651 | 91 | Weighted Average | | | | |
| | | 2,508 | | 37.71% Pei | rvious Area | | | |
| | | 4,143 | | 62.29% lmp | pervious Ar | ea | | |
| | _ | | | | . | | | |
| _ | | Length | Slope | _ | Capacity | Description | | |
| (m | ıin) | (feet) | (ft/ft | (ft/sec) | (cfs) | | | |
| | 7.0 | | | | | Direct Entry. | | |

Subcatchment 5S: to 102



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Summary for Reach 3R: total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

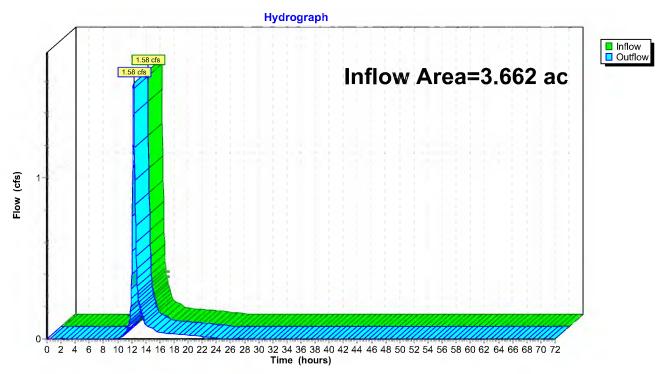
Inflow Area = 3.662 ac, 52.96% Impervious, Inflow Depth = 0.36" for 10-Year event

Inflow = 1.58 cfs @ 12.27 hrs, Volume= 0.111 af

Outflow = 1.58 cfs @ 12.27 hrs, Volume= 0.111 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 3R: total to offsite wetland



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Summary for Reach 4R: total proposed

[40] Hint: Not Described (Outflow=Inflow)

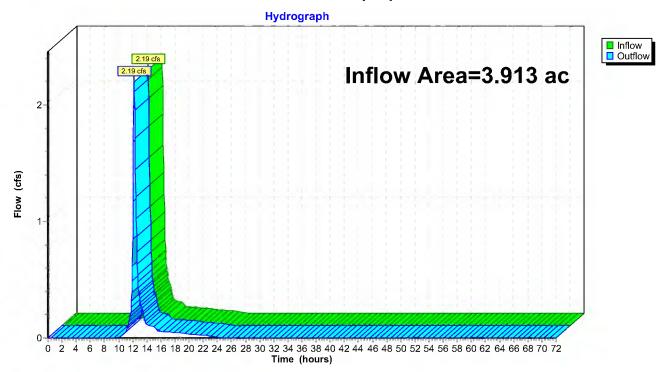
Inflow Area = 3.913 ac, 50.61% Impervious, Inflow Depth = 0.50" for 10-Year event

Inflow = 2.19 cfs @ 12.19 hrs, Volume= 0.164 af

Outflow = 2.19 cfs @ 12.19 hrs, Volume= 0.164 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 4R: total proposed



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Summary for Pond 1P: Underground Detention

[58] Hint: Peaked 0.73' above defined flood level

Inflow Area = 1.834 ac, 95.12% Impervious, Inflow Depth = 3.91" for 10-Year event

Inflow = 10.83 cfs @ 12.14 hrs, Volume= 0.598 af

Outflow = 8.26 cfs @ 12.22 hrs, Volume= 0.598 af, Atten= 24%, Lag= 4.6 min

Primary = 8.26 cfs @ 12.22 hrs, Volume= 0.598 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 927.49' @ 12.22 hrs Surf.Area= 3,774 sf Storage= 9,293 cf

Flood Elev= 926.76' Surf.Area= 3,774 sf Storage= 7,920 cf

Plug-Flow detention time= 108.6 min calculated for 0.597 af (100% of inflow)

Center-of-Mass det. time= 108.6 min (863.5 - 755.0)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|---|
| #1A | 922.50' | 0 cf | 37.00'W x 102.00'L x 6.00'H Field A |
| | | | 22,644 cf Overall - 9,817 cf Embedded = 12,827 cf x 0.0% Voids |
| #2A | 923.00' | 9,817 cf | CMP Round 60 x 25 Inside #1 |
| | | | Effective Size= 60.0 "W x 60.0 "H => 19.63 sf x 20.00 'L = 392.7 cf |
| | | | Overall Size= 60.0"W x 60.0"H x 20.00'L |
| | | | 25 Chambers in 5 Rows |
| #3 | 928.00' | 137 cf | riser storage (Prismatic)Listed below (Recalc) |
| | | | |

9,954 cf Total Available Storage

Storage Group A created with Chamber Wizard

| E | Elevation | Surf.Area | Inc.Store | Cum.Store |
|---|-----------|-----------|--------------|--------------|
| | (feet) | (sq-ft) | (cubic-feet) | (cubic-feet) |
| | 928.00 | 65 | 0 | 0 |
| | 930.10 | 65 | 137 | 137 |
| | | | | |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 920.70' | 24.0" Round device outlet L= 108.0' Ke= 0.900 |
| | • | | Inlet / Outlet Invert= 920.70' / 920.17' S= 0.0049 '/' Cc= 0.900 |
| | | | n= 0.011, Flow Area= 3.14 sf |
| #2 | Device 1 | 923.00' | 0.480 cfs 18" phospho, 14 cartridge |
| #3 | Device 2 | 923.00' | 4.0" Vert. device inlet C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 926.76' | 4.0' long device bypass weir 2 End Contraction(s) |

Primary OutFlow Max=7.54 cfs @ 12.22 hrs HW=927.44' TW=921.40' (Dynamic Tailwater)

1=device outlet (Passes 7.54 cfs of 28.61 cfs potential flow)

-2=18" phospho, 14 cartridge (Constant Controls 0.48 cfs)

3=device inlet (Passes 0.48 cfs of 0.87 cfs potential flow)

-4=device bypass weir (Weir Controls 7.06 cfs @ 2.69 fps)

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Pond 1P: Underground Detention - Chamber Wizard Field A

Chamber Model = CMP Round 60 (Round Corrugated Metal Pipe)

Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf Overall Size= 60.0"W x 60.0"H x 20.00'L

60.0" Wide + 30.0" Spacing = 90.0" C-C Row Spacing

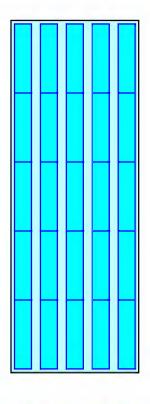
5 Chambers/Row x 20.00' Long = 100.00' Row Length +12.0" End Stone x 2 = 102.00' Base Length 5 Rows x 60.0" Wide + 30.0" Spacing x 4 + 12.0" Side Stone x 2 = 37.00' Base Width 6.0" Stone Base + 60.0" Chamber Height + 6.0" Stone Cover = 6.00' Field Height

25 Chambers x 392.7 cf = 9,817.5 cf Chamber Storage

22,644.0 cf Field - 9,817.5 cf Chambers = 12,826.5 cf Stone x 0.0% Voids = 0.0 cf Stone Storage

Chamber Storage = 9.817.5 cf = 0.225 afOverall Storage Efficiency = 43.4% Overall System Size = 102.00' x 37.00' x 6.00'

25 Chambers 838.7 cy Field 475.1 cy Stone

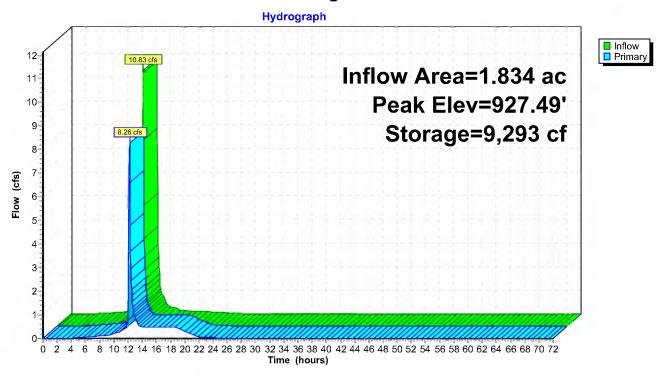




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Pond 1P: Underground Detention



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Stage-Area-Storage for Pond 1P: Underground Detention

| Elevation | Storage | Elevation | Storage |
|------------------|----------------|-----------|--------------|
| (feet) | (cubic-feet) | (feet) | (cubic-feet) |
| 922.50 | 0 | 927.60 | 9,450 |
| 922.60 | 0 | 927.70 | 9,577 |
| 922.70 | 0 | 927.80 | 9,686 |
| 922.80 | 0 | 927.90 | 9,770 |
| 922.90 | 0 | 928.00 | 9,817 |
| 923.00 | 0 | 928.10 | 9,824 |
| 923.10 | 47 | 928.20 | 9,830 |
| 923.20 | 132 | 928.30 | 9,837 |
| 923.30 | 240 | 928.40 | 9,843 |
| 923.40 | 368 | 928.50 | 9,850 |
| 923.50 | 511 | 928.60 | 9,856 |
| 923.60 | 667 | 928.70 | 9,863 |
| 923.70 | 835 | 928.80 | 9,869 |
| 923.80 | 1,014 | 928.90 | 9,876 |
| 923.90 | 1,202 | 929.00 | 9,882 |
| 924.00 | 1,398 | 929.10 | 9,889 |
| 924.10 | 1,601 | 929.20 | 9,895 |
| 924.20 | 1,812 | 929.30 | 9,902 |
| 924.30 | 2,028 | 929.40 | 9,908 |
| 924.40 | 2,250 | 929.50 | 9,915 |
| 924.50 | 2,477 | 929.60 | 9,921 |
| 924.60 | 2,708 | 929.70 | 9,928 |
| 924.70 | 2,943 | 929.80 | 9,934 |
| 924.80 | 3,182 | 929.90 | 9,941 |
| 924.90 | 3,423 | 930.00 | 9,947 |
| 925.00 | 3,667 | 930.10 | 9,954 |
| 925.10 | 3,913 | | |
| 925.20 | 4,161 | | |
| 925.30 | 4,409 | | |
| 925.40 925.50 | 4,659 4,909 | | |
| 925.60 | 5,159 | | |
| 925.70 | 5,408 | | |
| 925.80 | 5,657 | | |
| 925.90 | 5,904 | | |
| 926.00 | 6,150 | | |
| 926.10 | 6,394 | | |
| 926.20 | 6,636 | | |
| 926.30 | 6,874 | | |
| 926.40 | 7,109 | | |
| 926.50 | 7,340 | | |
| 926.60 | 7,567 | | |
| 926.70 | 7,789 | | |
| 926.80 | 8,006 | | |
| 926.90 | 8,216 | | |
| 927.00 | 8,420 | | |
| 927.10 | 8,616 | | |
| 927.20 | 8,804 | | |
| 927.30 | 8,982 | | |
| 927.40 | 9,150 | | |
| 927.50 | 9,307 | | |
| | 1.13 | | |

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Summary for Pond 102: stmh 102

[57] Hint: Peaked at 921.49' (Flood elevation advised)

Inflow Area = 1.987 ac, 92.60% Impervious, Inflow Depth = 3.86" for 10-Year event

Inflow = 8.80 cfs @ 12.21 hrs, Volume= 0.639 af

Outflow = 8.80 cfs @ 12.21 hrs, Volume= 0.639 af, Atten= 0%, Lag= 0.0 min

Primary = 8.80 cfs @ 12.21 hrs, Volume= 0.639 af

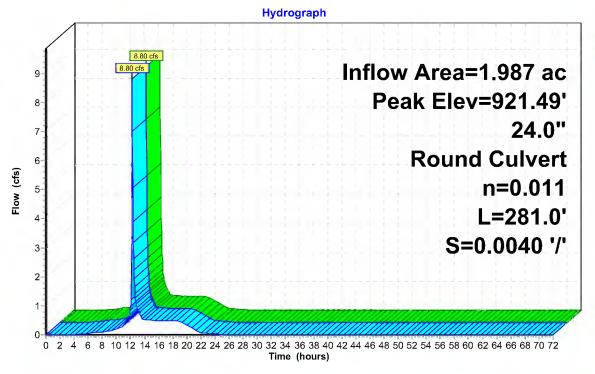
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 921.49' @ 12.21 hrs

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|---|
| #1 | Primary | 919.93' | 24.0" Round Culvert L= 281.0' Ke= 0.900 Inlet / Outlet Invert= 919.93' / 918.80' S= 0.0040 '/' Cc= 0.900 n= 0.011 Flow Area= 3.14 sf |

Primary OutFlow Max=8.14 cfs @ 12.21 hrs HW=921.41' TW=916.48' (Dynamic Tailwater) 1=Culvert (Inlet Controls 8.14 cfs @ 3.27 fps)

Pond 102: stmh 102





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Stage-Area-Storage for Pond 102: stmh 102

| Elevation | Storage | Elevation | Storage |
|------------------|----------------|------------------|----------------|
| (feet) | (acre-feet) | (feet) | (acre-feet) |
| 919.93 | 0.000 | 920.95 | 0.000 |
| 919.95 | 0.000 | 920.97 | 0.000 |
| 919.97 | 0.000 | 920.99 | 0.000 |
| 919.99 | 0.000 | 921.01 | 0.000 |
| 920.01 | 0.000 | 921.03 | 0.000 |
| 920.03 | 0.000 | 921.05 | 0.000 |
| 920.05 | 0.000 | 921.07 | 0.000 |
| 920.07 | 0.000 | 921.09 | 0.000 |
| 920.09 | 0.000 | 921.11 | 0.000 |
| 920.11 | 0.000 | 921.13 | 0.000 |
| 920.13 | 0.000 | 921.15 | 0.000 |
| 920.15 | 0.000 | 921.17 | 0.000 |
| 920.17 | 0.000 | 921.19 | 0.000 |
| 920.19 | 0.000 | 921.21 | 0.000 |
| 920.21 | 0.000 | 921.23 | 0.000 |
| 920.23 | 0.000 | 921.25 | 0.000 |
| 920.25 | 0.000 | 921.27 | 0.000 |
| 920.27 | 0.000 | 921.29 | 0.000 |
| 920.29 | 0.000 | 921.31 | 0.000 |
| 920.31 | 0.000 | 921.33 | 0.000 |
| 920.33 | 0.000 | 921.35 | 0.000 |
| 920.35 | 0.000 | 921.37 | 0.000 |
| 920.37 | 0.000 | 921.39 | 0.000 |
| 920.39 | 0.000 | 921.41 | 0.000 |
| 920.41 | 0.000 | 921.43 | 0.000 |
| 920.43 | 0.000 | 921.45 | 0.000 |
| 920.45 | 0.000 | 921.47 | 0.000 |
| 920.47 | 0.000 | 921.49 | 0.000 |
| 920.49 | 0.000 | 921.51 | 0.000 |
| 920.51 | 0.000 | 921.53 921.55 | 0.000 |
| 920.53 | 0.000 | 921.55 | 0.000 |
| 920.55 920.57 | 0.000 0.000 | 921.59 | 0.000 0.000 |
| 920.57 | 0.000 | 921.61 | 0.000 |
| 920.59 | 0.000 | 921.63 | 0.000 |
| 920.63 | 0.000 | 921.65 | 0.000 |
| 920.65 | 0.000 | 921.67 | 0.000 |
| 920.67 | 0.000 | 921.69 | 0.000 |
| 920.69 | 0.000 | 921.71 | 0.000 |
| 920.71 | 0.000 | 921.73 | 0.000 |
| 920.73 | 0.000 | 921.75 | 0.000 |
| 920.75 | 0.000 | 921.77 | 0.000 |
| 920.77 | 0.000 | 921.79 | 0.000 |
| 920.79 | 0.000 | 921.81 | 0.000 |
| 920.81 | 0.000 | 921.83 | 0.000 |
| 920.83 | 0.000 | 921.85 | 0.000 |
| 920.85 | 0.000 | 921.87 | 0.000 |
| 920.87 | 0.000 | 921.89 | 0.000 |
| 920.89 | 0.000 | 921.91 | 0.000 |
| 920.91 | 0.000 | 921.93 | 0.000 |
| 920.93 | 0.000 | | |
| | | | |
| | | | |

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Summary for Pond Wtld Prd: Existing Wetland

Inflow Area = 3.072 ac, 62.17% Impervious, Inflow Depth = 3.32" for 10-Year event

Inflow = 11.92 cfs @ 12.21 hrs, Volume= 0.851 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 917.57' @ 37.65 hrs Surf.Area= 25,672 sf Storage= 37,069 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Avail.Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

Invert

| | | , | | | | |
|-----------|----------|--|--------------------|-------------------|------------------------|-----------|
| #1 | 916.0 | 76,7 | 84 cf Custom S | Stage Data (Pr | ismatic)Listed below (| Recalc) |
| Elevation | on | Surf.Area | Inc.Store | Cum.Store | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | |
| | | | | | | |
| Device | Routing | Invert | Outlet Devices | | | |
| #1 | Primary | 916.35' | 15.0" Round o | ocs outlet L= 1 | 18.0' Ke= 0.900 | |
| ř | | Inlet / Outlet Invert= 916.35' / 916.22' S= 0.0072 '/' Cc= 0.900 | | | | |
| | | | n= 0.010, Flow | / Area= 1.23 sf | | |
| #2 | Device 1 | 918.08' | 4.0' long ocs v | veir wall 2 End | d Contraction(s) | |
| #3 | Device 2 | 917.07' | 15.0" Round o | ocs inlet L= 12 | 2.0' Ke= 0.900 | |
| | | | Inlet / Outlet Inv | vert= 917.07' / 9 | 916.39' S= 0.0567 '/' | Cc= 0.900 |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=916.00' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

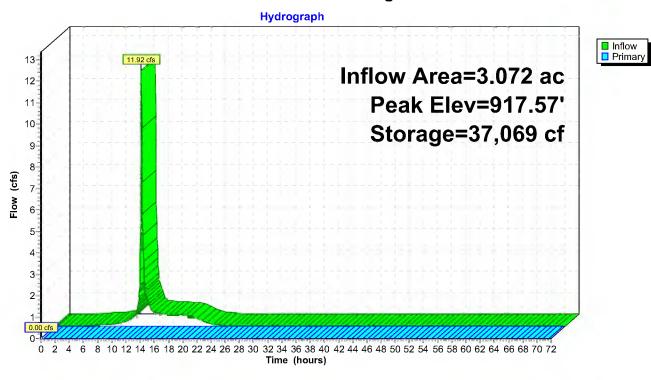
-1=ocs outlet (Controls 0.00 cfs)

-2=ocs weir wall (Controls 0.00 cfs)
-3=ocs inlet (Controls 0.00 cfs)

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Pond Wtld Prd: Existing Wetland



Storage

63,564

65,000

66,444

67,897

69,357 70,826

72,303 73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Prd: Existing Wetland

Elevation

(feet)

918.55

918.60

918.65

918.70

918.75

918.80 918.85

918.90

918.95

919.00

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| Elevation | Surface | Storage |
|------------------|------------------|------------------|
| (feet) | (s <u>q</u> -ft) | (cubic-feet) |
| 916.00 | 21,538 | 0 |
| 916.05 916.10 | 21,667 21,797 | 1,080 2,167 |
| 916.15 | 21,797 | 3,260 |
| 916.20 | 22,056 | 4,359 |
| 916.25 | 22,186 | 5,465 |
| 916.30 | 22,315 | 6,578 |
| 916.35 916.40 | 22,445 22,574 | 7,697 8,822 |
| 916.45 | 22,704 | 9,954 |
| 916.50 | 22,833 | 11,093 |
| 916.55 | 22,962 | 12,238 |
| 916.60 | 23,092 | 13,389 |
| 916.65 916.70 | 23,221 23,351 | 14,547 15,711 |
| 916.75 | 23,481 | 16,882 |
| 916.80 | 23,610 | 18,059 |
| 916.85 | 23,740 | 19,243 |
| 916.90 916.95 | 23,869 23,999 | 20,433 21,630 |
| 917.00 | 24,128 | 22,833 |
| 917.05 | 24,263 | 24,043 |
| 917.10 | 24,398 | 25,259 |
| 917.15 | 24,533 | 26,483 |
| 917.20 917.25 | 24,668 24,803 | 27,713 28,949 |
| 917.30 | 24,938 | 30,193 |
| 917.35 | 25,073 | 31,443 |
| 917.40 | 25,208 | 32,700 |
| 917.45 917.50 | 25,343 25,478 | 33,964 35,235 |
| 917.55 | 25,613 | 36,512 |
| 917.60 | 25,748 | 37,796 |
| 917.65 | 25,883 | 39,087 |
| 917.70 917.75 | 26,018 26,153 | 40,384 41,688 |
| 917.80 | 26,133 | 42,999 |
| 917.85 | 26,423 | 44,317 |
| 917.90 | 26,558 | 45,642 |
| 917.95 | 26,693 | 46,973 |
| 918.00 918.05 | 26,828 26,992 | 48,311 49,657 |
| 918.10 | 27,157 | 51,010 |
| 918.15 | 27,321 | 52,372 |
| 918.20 | 27,486 27,651 | 53,742 |
| 918.25 918.30 | 27,651 27,815 | 55,121 56,507 |
| 918.35 | 27,980 | 57,902 |
| 918.40 | 28,144 | 59,305 |
| 918.45 | 28,309 | 60,717 |
| 918.50 | 28,473 | 62,136 |

20230222 hydrocad

MSE 24-hr 3 100-Year Rainfall=7.32" Prepared by MFRA Printed 2/22/2023

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=79,886 sf 95.12% Impervious Runoff Depth=6.96" Subcatchment 1S: To site sewer

Tc=7.0 min CN=97 Runoff=18.80 cfs 1.064 af

Subcatchment2S: Direct to wetland Runoff Area=47.288 sf 6.48% Impervious Runoff Depth=5.10"

Tc=7.0 min CN=81 Runoff=9.31 cfs 0.462 af

Runoff Area=25,698 sf 5.00% Impervious Runoff Depth=4.99" Subcatchment3S: Runoff to Offsite

Flow Length=260' Slope=0.0200 '/' Tc=17.8 min CN=80 Runoff=3.45 cfs 0.245 af

Subcatchment 4S: Runoff to Wazata Blvd Runoff Area = 10,922 sf 16.27% Impervious Runoff Depth = 5.33"

Tc=7.0 min CN=83 Runoff=2.22 cfs 0.111 af

Subcatchment5S: to 102 Runoff Area=6,651 sf 62.29% Impervious Runoff Depth=6.25"

Tc=7.0 min CN=91 Runoff=1.50 cfs 0.080 af

Inflow=3.45 cfs 0.692 af Reach 3R: total to offsite wetland

Outflow=3.45 cfs 0.692 af

Inflow=4.74 cfs 0.803 af Reach 4R: total proposed

Outflow=4.74 cfs 0.803 af

Pond 1P: Underground Detention Peak Elev=928.10' Storage=9,824 cf Inflow=18.80 cfs 1.064 af

Outflow=19.45 cfs 1.064 af

Peak Elev=924.00' Inflow=20.95 cfs 1.143 af Pond 102: stmh 102

24.0" Round Culvert n=0.011 L=281.0' S=0.0040'/' Outflow=20.95 cfs 1.143 af

Peak Elev=918.21' Storage=53,987 cf Inflow=30.24 cfs 1.605 af Pond Wtld Prd: Existing Wetland

Outflow=0.60 cfs 0.446 af

Total Runoff Area = 3.913 ac Runoff Volume = 1.962 af Average Runoff Depth = 6.02" 49.39% Pervious = 1.933 ac 50.61% Impervious = 1.980 ac

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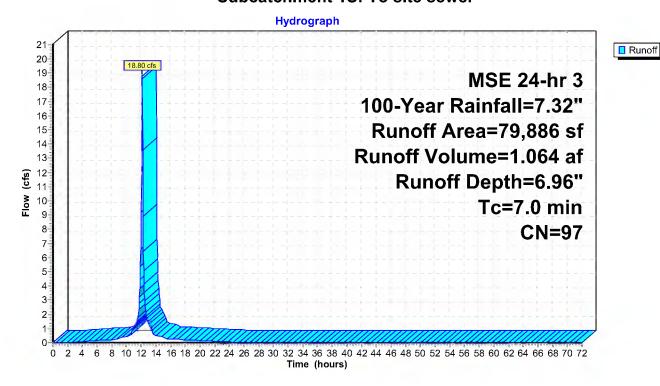
Summary for Subcatchment 1S: To site sewer

Runoff = 18.80 cfs @ 12.14 hrs, Volume= 1.064 af, Depth= 6.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN | Description | | | | |
|-------|-------------|---------|-------------------------------|------------|---------------|--|--|
| | 75,991 | 98 | Paved park | ing, HSG D |) | | |
| | 3,895 | 80 | >75% Grass cover, Good, HSG D | | | | |
| | 79,886 | 97 | Weighted A | verage | | | |
| | 3,895 | | 4.88 ⁻ % Perv | ious Ārea | | | |
| | 75,991 | | 95.12% Imp | ervious Ar | ea | | |
| т. | ملئيم مراجا | Clama. | \/alaait | 0 | Decembries | | |
| Tc | Length | Slope | • | Capacity | Description | | |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | | | |
| 7.0 | | | | | Direct Entry. | | |

Subcatchment 1S: To site sewer



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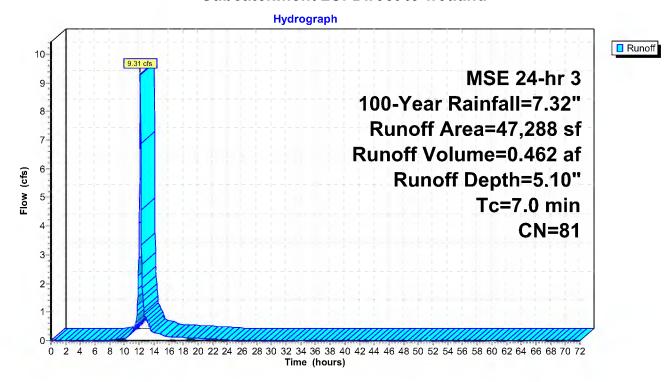
Summary for Subcatchment 2S: Direct to wetland

Runoff = 9.31 cfs @ 12.14 hrs, Volume= 0.462 af, Depth= 5.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| | Area (sf) | CN | Description | | | |
|------|-----------|---------|-----------------------|-------------|---------------|--|
| | 3,064 | 98 | Paved park | ing, HSG E |) | |
| | 44,224 | 80 | >75% Gras | s cover, Go | ood, HSG D | |
| | 47,288 | 81 | Weighted A | verage | | |
| | 44,224 | | 93.52% Pervious Area | | | |
| | 3,064 | | 6.48% Impervious Area | | | |
| _ | | | | | | |
| Te | | Slope | _ | Capacity | Description | |
| (min |) (feet) | (ft/ft) | (ft/sec) | (cfs) | | |
| 7.0 |) | | | | Direct Entry. | |

Subcatchment 2S: Direct to wetland



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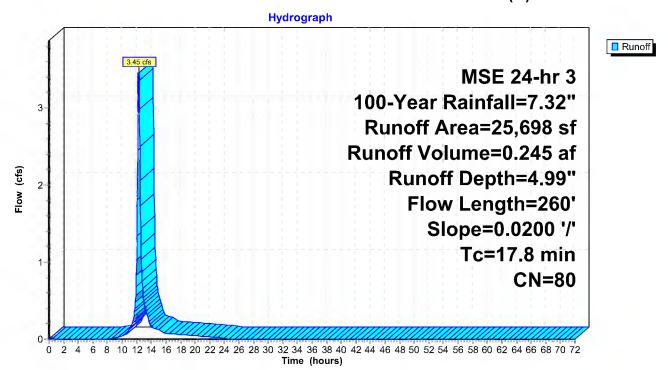
Summary for Subcatchment 3S: Runoff to Offsite Wetland (N)

Runoff = 3.45 cfs @ 12.26 hrs, Volume= 0.245 af, Depth= 4.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN E | Description | | |
|-------|----------|---------|-------------------------|-------------|---------------------------------|
| | 1,286 | 98 F | 98 Paved parking, HSG D | | |
| | 24,412 | 79 V | Voods/gras | ss comb., C | Good, HSG D |
| | 25,698 | 80 V | Veighted A | verage | |
| | 24,412 | S | 5.00% Per | vious Area | |
| | 1,286 | 5 | .00% Impe | ervious Are | a |
| | | | | | |
| Tc | Length | Slope | Velocity | Capacity | Description |
| (min) | (feet) | (ft/ft) | (ft/sec) | (cfs) | |
| 15.1 | 100 | 0.0200 | 0.11 | | Sheet Flow, SWALE |
| | | | | | Grass: Dense n= 0.240 P2= 2.86" |
| 2.7 | 160 | 0.0200 | 0.99 | | Shallow Concentrated Flow, |
| | | | | | Short Grass Pasture Kv= 7.0 fps |
| 17.8 | 260 | Total | | | |

Subcatchment 3S: Runoff to Offsite Wetland (N)



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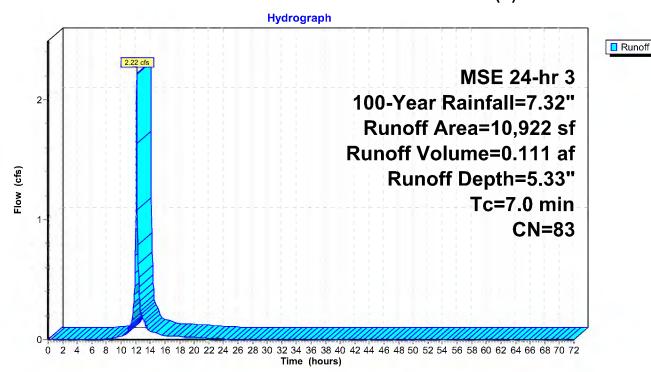
Summary for Subcatchment 4S: Runoff to Wazata Blvd (S)

Runoff = 2.22 cfs @ 12.14 hrs, Volume= 0.111 af, Depth= 5.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN | Description | | |
|-------------|------------------|-----------------|------------------------|-------------------|---------------|
| | 1,777 | 98 | Paved park | ing, HSG E | D |
| | 9,145 | 80 | >75% Gras | s cover, Go | lood, HSG D |
| | 10,922 | 83 | Weighted A | verage | |
| | 9,145 | | 83.73% Pei | vious Area | a |
| | 1,777 | | 16.27% Impervious Area | | |
| Tc (min) | Length (feet) | Slope (ft/ft | • | Capacity (cfs) | · |
| 7.0 | | | | | Direct Entry, |

Subcatchment 4S: Runoff to Wazata Blvd (S)



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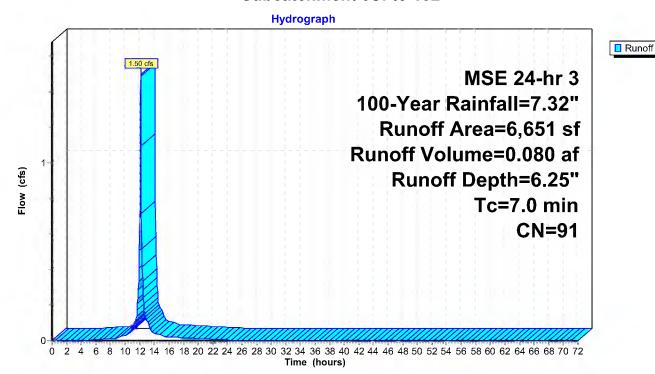
Summary for Subcatchment 5S: to 102

Runoff = 1.50 cfs @ 12.14 hrs, Volume= 0.080 af, Depth= 6.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs MSE 24-hr 3 100-Year Rainfall=7.32"

| A | rea (sf) | CN | Description | | | |
|-------------|------------------|------------------|-------------------------|-------------------|---------------|--|
| | 4,143 | 98 | Paved park | ing, HSG E | | |
| | 2,508 | 80 | >75% Gras | s cover, Go | od, HSG D | |
| | 6,651 | 91 | Weighted A | verage | | |
| | 2,508 | | 37.7 ¹ % Pei | vious Area | | |
| | 4,143 | | 62.29% Impervious Area | | | |
| Tc (min) | Length (feet) | Slope (ft/ft) | - | Capacity (cfs) | Description | |
| 7.0 | (ICCI) | (1010 | (10300) | (013) | Direct Entry, | |

Subcatchment 5S: to 102



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Summary for Reach 3R: total to offsite wetland

[40] Hint: Not Described (Outflow=Inflow)

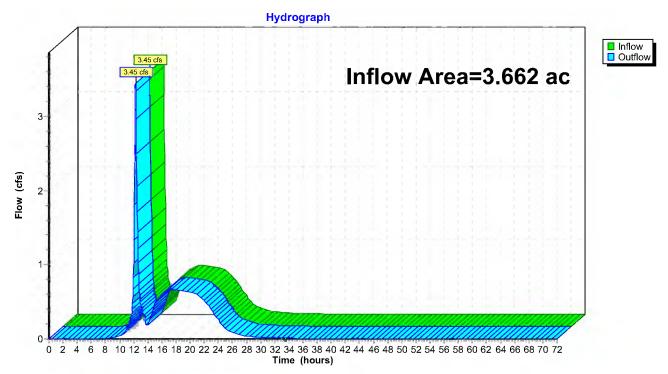
Inflow Area = 3.662 ac, 52.96% Impervious, Inflow Depth = 2.27" for 100-Year event

Inflow = 3.45 cfs @ 12.26 hrs, Volume= 0.692 af

Outflow = 3.45 cfs @ 12.26 hrs, Volume= 0.692 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 3R: total to offsite wetland



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Summary for Reach 4R: total proposed

[40] Hint: Not Described (Outflow=Inflow)

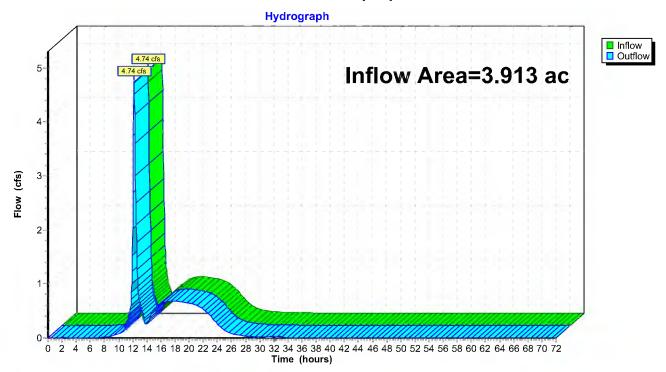
Inflow Area = 3.913 ac, 50.61% Impervious, Inflow Depth = 2.46" for 100-Year event

Inflow = 4.74 cfs @ 12.19 hrs, Volume= 0.803 af

Outflow = 4.74 cfs @ 12.19 hrs, Volume= 0.803 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 4R: total proposed



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Summary for Pond 1P: Underground Detention

[58] Hint: Peaked 1.34' above defined flood level

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

1.834 ac, 95.12% Impervious, Inflow Depth = 6.96" for 100-Year event

Inflow = 18.80 cfs @ 12.14 hrs, Volume= 1.064 af

Outflow 19.45 cfs @ 12.15 hrs, Volume= 1.064 af, Atten= 0%, Lag= 0.5 min

19.45 cfs @ 12.15 hrs, Volume= Primary 1.064 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 928.10' @ 12.15 hrs Surf.Area= 3,839 sf Storage= 9,824 cf

Flood Elev= 926.76' Surf.Area= 3,774 sf Storage= 7,920 cf

Plug-Flow detention time= 84.7 min calculated for 1.063 af (100% of inflow)

Center-of-Mass det. time= 84.7 min (831.3 - 746.6)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1A | 922.50' | 0 cf | 37.00'W x 102.00'L x 6.00'H Field A |
| | | | 22,644 cf Overall - 9,817 cf Embedded = 12,827 cf x 0.0% Voids |
| #2A | 923.00' | 9,817 cf | CMP Round 60 x 25 Inside #1 |
| | | | Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf |
| | | | Overall Size= 60.0"W x 60.0"H x 20.00'L |
| | | | 25 Chambers in 5 Rows |
| #3 | 928.00' | 137 cf | riser storage (Prismatic)Listed below (Recalc) |
| | | | |

9,954 cf Total Available Storage

Storage Group A created with Chamber Wizard

| Elevation | Surf.Area | Inc.Store | Cum.Store |
|-----------|-----------|--------------|--------------|
| (feet) | (sq-ft) | (cubic-feet) | (cubic-feet) |
| 928.00 | 65 | 0 | 0 |
| 930.10 | 65 | 137 | 137 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 920.70' | 24.0" Round device outlet L= 108.0' Ke= 0.900 |
| | • | | Inlet / Outlet Invert= 920.70' / 920.17' S= 0.0049 '/' Cc= 0.900 |
| | | | n= 0.011, Flow Area= 3.14 sf |
| #2 | Device 1 | 923.00' | 0.480 cfs 18" phospho, 14 cartridge |
| #3 | Device 2 | 923.00' | 4.0" Vert. device inlet C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 926.76' | 4.0' long device bypass weir 2 End Contraction(s) |

Primary OutFlow Max=19.16 cfs @ 12.15 hrs HW=928.09' TW=923.93' (Dynamic Tailwater)

-1=device outlet (Passes 19.16 cfs of 24.36 cfs potential flow)

-2=18" phospho, 14 cartridge (Constant Controls 0.48 cfs)

3=device inlet (Passes 0.48 cfs of 0.86 cfs potential flow)

-4=device bypass weir (Weir Controls 18.68 cfs @ 3.77 fps)

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Pond 1P: Underground Detention - Chamber Wizard Field A

Chamber Model = CMP Round 60 (Round Corrugated Metal Pipe)

Effective Size= 60.0"W x 60.0"H => 19.63 sf x 20.00'L = 392.7 cf Overall Size= 60.0"W x 60.0"H x 20.00'L

60.0" Wide + 30.0" Spacing = 90.0" C-C Row Spacing

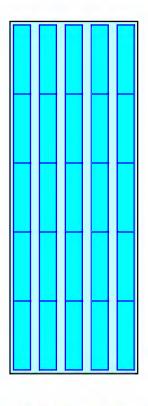
5 Chambers/Row x 20.00' Long = 100.00' Row Length +12.0" End Stone x 2 = 102.00' Base Length 5 Rows x 60.0" Wide + 30.0" Spacing x 4 + 12.0" Side Stone x 2 = 37.00' Base Width 6.0" Stone Base + 60.0" Chamber Height + 6.0" Stone Cover = 6.00' Field Height

25 Chambers x 392.7 cf = 9,817.5 cf Chamber Storage

22,644.0 cf Field - 9,817.5 cf Chambers = 12,826.5 cf Stone x 0.0% Voids = 0.0 cf Stone Storage

Chamber Storage = 9,817.5 cf = 0.225 af Overall Storage Efficiency = 43.4% Overall System Size = 102.00' x 37.00' x 6.00'

25 Chambers 838.7 cy Field 475.1 cy Stone

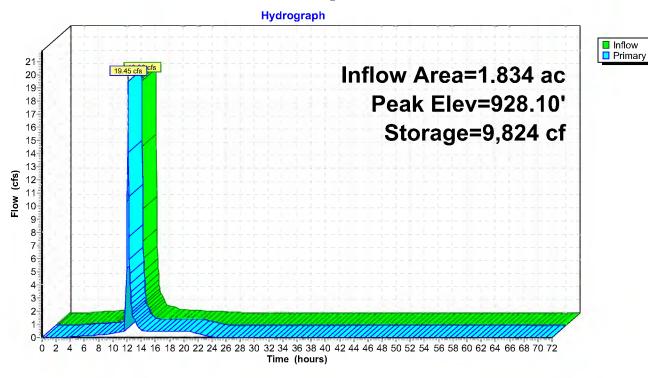




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Pond 1P: Underground Detention



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Stage-Area-Storage for Pond 1P: Underground Detention

| Elevation | Storage | Elevation | Storage |
|-----------|--------------|-----------|--------------|
| (feet) | (cubic-feet) | (feet) | (cubic-feet) |
| 922.50 | Ó | 927.60 | 9,450 |
| 922.60 | 0 | 927.70 | 9,577 |
| 922.70 | ő | 927.80 | 9,686 |
| 922.80 | 0 | 927.90 | 9,770 |
| 922.90 | 0 | | |
| | | 928.00 | 9,817 |
| 923.00 | 0 | 928.10 | 9,824 |
| 923.10 | 47 | 928.20 | 9,830 |
| 923.20 | 132 | 928.30 | 9,837 |
| 923.30 | 240 | 928.40 | 9,843 |
| 923.40 | 368 | 928.50 | 9,850 |
| 923.50 | 511 | 928.60 | 9,856 |
| 923.60 | 667 | 928.70 | 9,863 |
| 923.70 | 835 | 928.80 | 9,869 |
| 923.80 | 1,014 | 928.90 | 9,876 |
| 923.90 | 1,202 | 929.00 | 9,882 |
| 924.00 | 1,398 | 929.10 | 9,889 |
| 924.10 | 1,601 | 929.20 | 9,895 |
| 924.20 | 1,812 | 929.30 | 9,902 |
| 924.30 | 2,028 | 929.40 | 9,908 |
| 924.40 | | | |
| | 2,250 | 929.50 | 9,915 |
| 924.50 | 2,477 | 929.60 | 9,921 |
| 924.60 | 2,708 | 929.70 | 9,928 |
| 924.70 | 2,943 | 929.80 | 9,934 |
| 924.80 | 3,182 | 929.90 | 9,941 |
| 924.90 | 3,423 | 930.00 | 9,947 |
| 925.00 | 3,667 | 930.10 | 9,954 |
| 925.10 | 3,913 | | |
| 925.20 | 4,161 | | |
| 925.30 | 4,409 | | |
| 925.40 | 4,659 | | |
| 925.50 | 4,909 | | |
| 925.60 | 5,159 | | |
| 925.70 | 5,408 | | |
| 925.80 | 5,657 | | |
| 925.90 | 5,904 | | |
| 926.00 | 6,150 | | |
| 926.10 | 6,394 | | |
| 926.20 | 6,636 | | |
| | | | |
| 926.30 | 6,874 | | |
| 926.40 | 7,109 | | |
| 926.50 | 7,340 | | |
| 926.60 | 7,567 | | |
| 926.70 | 7,789 | | |
| 926.80 | 8,006 | | |
| 926.90 | 8,216 | | |
| 927.00 | 8,420 | | |
| 927.10 | 8,616 | | |
| 927.20 | 8,804 | | |
| 927.30 | 8,982 | | |
| 927.40 | 9,150 | | |
| 927.50 | 9,307 | | |
| | | | |
| | | | |

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Summary for Pond 102: stmh 102

[57] Hint: Peaked at 924.00' (Flood elevation advised)

Inflow Area = 1.987 ac, 92.60% Impervious, Inflow Depth = 6.91" for 100-Year event

Inflow = 20.95 cfs @ 12.15 hrs, Volume= 1.143 af

Outflow = 20.95 cfs @ 12.15 hrs, Volume= 1.143 af, Atten= 0%, Lag= 0.0 min

Primary = 20.95 cfs @ 12.15 hrs, Volume= 1.143 af

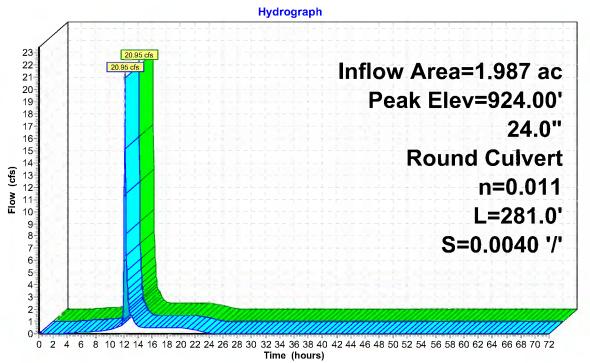
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 924.00' @ 12.15 hrs

| Device | Routing | Invert | Outlet Devices |
|--------|---------|---------|--|
| #1 | Primary | 919.93' | 24.0" Round Culvert L= 281.0' Ke= 0.900 Inlet / Outlet Invert= 919.93' / 918.80' S= 0.0040 '/' Cc= 0.900 n= 0.011, Flow Area= 3.14 sf |

Primary OutFlow Max=20.64 cfs @ 12.15 hrs HW=923.92' TW=917.02' (Dynamic Tailwater) 1=Culvert (Inlet Controls 20.64 cfs @ 6.57 fps)

Pond 102: stmh 102





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Stage-Area-Storage for Pond 102: stmh 102

| - | 0. | l —, | 01 |
|------------------|----------------|------------------|----------------|
| Elevation | Storage | Elevation | Storage |
| (feet) | (acre-feet) | (feet) | (acre-feet) |
| 919.93 | 0.000 | 922.48 | 0.000 |
| 919.98 | 0.000 | 922.53 | 0.000 |
| 920.03 | 0.000 | 922.58 | 0.000 |
| 920.08 | 0.000 | 922.63 922.68 | 0.000 |
| 920.13 920.18 | 0.000 0.000 | 922.73 | 0.000 0.000 |
| 920.18 | 0.000 | 922.73 | 0.000 |
| 920.28 | 0.000 | 922.83 | 0.000 |
| 920.33 | 0.000 | 922.88 | 0.000 |
| 920.38 | 0.000 | 922.93 | 0.000 |
| 920.43 | 0.000 | 922.98 | 0.000 |
| 920.48 | 0.000 | 923.03 | 0.000 |
| 920.53 | 0.000 | 923.08 | 0.000 |
| 920.58 | 0.000 | 923.13 | 0.000 |
| 920.63 | 0.000 | 923.18 | 0.000 |
| 920.68 | 0.000 | 923.23 | 0.000 |
| 920.73 | 0.000 | 923.28 | 0.000 |
| 920.78 | 0.000 | 923.33 | 0.000 |
| 920.83 | 0.000 | 923.38 | 0.000 |
| 920.88 | 0.000 | 923.43 | 0.000 |
| 920.93 | 0.000 | 923.48 | 0.000 |
| 920.98 | 0.000 | 923.53 | 0.000 |
| 921.03 | 0.000 | 923.58 | 0.000 |
| 921.08 | 0.000 | 923.63 | 0.000 |
| 921.13 | 0.000 | 923.68 | 0.000 |
| 921.18 | 0.000 | 923.73 | 0.000 |
| 921.23 921.28 | 0.000 | 923.78 923.83 | 0.000 |
| 921.26 | 0.000 0.000 | 923.88 | 0.000 0.000 |
| 921.38 | 0.000 | 923.88 | 0.000 |
| 921.43 | 0.000 | 923.98 | 0.000 |
| 921.48 | 0.000 | 020.00 | 0.000 |
| 921.53 | 0.000 | | |
| 921.58 | 0.000 | | |
| 921.63 | 0.000 | | |
| 921.68 | 0.000 | | |
| 921.73 | 0.000 | | |
| 921.78 | 0.000 | | |
| 921.83 | 0.000 | | |
| 921.88 | 0.000 | | |
| 921.93 | 0.000 | | |
| 921.98 | 0.000 | | |
| 922.03 | 0.000 | | |
| 922.08 | 0.000 | | |
| 922.13 | 0.000 | | |
| 922.18 922.23 | 0.000 | | |
| 922.23 922.28 | 0.000 0.000 | | |
| 922.26 | 0.000 | | |
| 922.38 | 0.000 | | |
| 922.43 | 0.000 | | |
| | 0.000 | | |

Volume

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Summary for Pond Wtld Prd: Existing Wetland

Inflow Area = 3.072 ac, 62.17% Impervious, Inflow Depth = 6.27" for 100-Year event

Inflow = 30.24 cfs @ 12.15 hrs, Volume= 1.605 af

Outflow = 0.60 cfs @ 18.21 hrs, Volume= 0.446 af, Atten= 98%, Lag= 364.0 min

Primary = 0.60 cfs @ 18.21 hrs, Volume= 0.446 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 918.21 @ 18.21 hrs Surf.Area= 27,515 sf Storage= 53,987 cf

Plug-Flow detention time= 549.0 min calculated for 0.446 af (28% of inflow)

Avail.Storage Storage Description

Center-of-Mass det. time= 383.9 min (1,199.5 - 815.6)

Invert

| VOIGITIC | 111401 | 7 | rage Clorage B | Coonplion | | |
|-----------|----------|---|--------------------|-------------------|-----------------------|-----------|
| #1 | 916.00 | 0' 76,78 | 34 cf Custom S | Stage Data (Pris | smatic)Listed below (| (Recalc) |
| Elevation | on S | Surf.Area | Inc.Store | Cum.Store | | |
| (fee | et) | (sq-ft) | (cubic-feet) | (cubic-feet) | | |
| 916.0 | 00 | 21,538 | 0 | 0 | | |
| 917.0 | 00 | 24,128 | 22,833 | 22,833 | | |
| 918.0 | 00 | 26,828 | 25,478 | 48,311 | | |
| 919.0 | 00 | 30,118 | 28,473 | 76,784 | | |
| Device | Routing | Invert | Outlet Devices | | | |
| #1 | Primary | 916.35' | 15.0" Round o | ocs outlet L= 18 | 3.0' Ke= 0.900 | |
| | • | | Inlet / Outlet Inv | vert= 916.35' / 9 | 16.22' S= 0.0072 '/' | Cc= 0.900 |
| | | | n= 0.010, Flow | / Area= 1.23 sf | | |
| #2 | Device 1 | 918.08' | 4.0' long ocs v | veir wall 2 End | Contraction(s) | |
| #3 | Device 2 | 917.07' | 15.0" Round o | ocs inlet L= 12. | 0' Ke= 0.900 | |
| | | | Inlet / Outlet Inv | vert= 917.07' / 9 | 16.39' S= 0.0567 '/' | Cc= 0.900 |

Primary OutFlow Max=0.60 cfs @ 18.21 hrs HW=918.21' TW=0.00' (Dynamic Tailwater)

n= 0.010, Flow Area= 1.23 sf

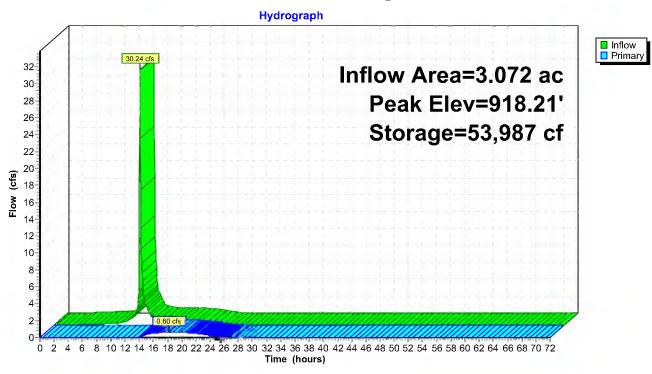
-1=ocs outlet (Passes 0.60 cfs of 5.18 cfs potential flow)
-2=ocs weir wall (Weir Controls 0.60 cfs @ 1.17 fps)

3=ocs inlet (Passes 0.60 cfs of 1.60 cfs potential flow)

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Pond Wtld Prd: Existing Wetland



Storage

63,564

65,000

66,444

67,897

69,357 70,826

72,303 73,789

75,282

76,784

(cubic-feet)

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Stage-Area-Storage for Pond Wtld Prd: Existing Wetland

Elevation

(feet)

918.55

918.60

918.65

918.70

918.75

918.80 918.85

918.90

918.95

919.00

Surface

(sq-ft)

28,637

28,802

28,966

29,131

29,296

29,460

29,625

29,789

29,954

30,118

| Elevation | Surface | Storage |
|------------------|----------------------------|-------------------|
| (feet) 916.00 | (s <u>q</u> -ft) 21,538 | (cubic-feet) 0 |
| 916.05 | 21,667 | 1,080 |
| 916.10 | 21,797 | 2,167 |
| 916.15 916.20 | 21,926 22,056 | 3,260 4,359 |
| 916.25 | 22,030 | 5,465 |
| 916.30 | 22,315 | 6,578 |
| 916.35 | 22,445 | 7,697 |
| 916.40 916.45 | 22,574 22,704 | 8,822 9,954 |
| 916.50 | 22,833 | 11,093 |
| 916.55 | 22,962 | 12,238 |
| 916.60 916.65 | 23,092 23,221 | 13,389 14,547 |
| 916.70 | 23,351 | 15,711 |
| 916.75 | 23,481 | 16,882 |
| 916.80 916.85 | 23,610 23,740 | 18,059 19,243 |
| 916.90 | 23,869 | 20,433 |
| 916.95 | 23,999 | 21,630 |
| 917.00 917.05 | 24,128 | 22,833 24,043 |
| 917.03 | 24,263 24,398 | 25,259 |
| 917.15 | 24,533 | 26,483 |
| 917.20 917.25 | 24,668 24,803 | 27,713 28,949 |
| 917.30 | 24,803 24,938 | 30,193 |
| 917.35 | 25,073 | 31,443 |
| 917.40 | 25,208 | 32,700 |
| 917.45 917.50 | 25,343 25,478 | 33,964 35,235 |
| 917.55 | 25,613 | 36,512 |
| 917.60 | 25,748 | 37,796 |
| 917.65 917.70 | 25,883 26,018 | 39,087 40,384 |
| 917.75 | 26,153 | 41,688 |
| 917.80 | 26,288 | 42,999 |
| 917.85 917.90 | 26,423 26,558 | 44,317 45,642 |
| 917.95 | 26,693 | 46,973 |
| 918.00 | 26,828 | 48,311 |
| 918.05 918.10 | 26,992 27,157 | 49,657 51,010 |
| 918.15 | 27,137 | 52,372 |
| 918.20 | 27,486 | 53,742 |
| 918.25 918.30 | 27,651 27,815 | 55,121 56,507 |
| 918.35 | 27,913 | 57,902 |
| 918.40 | 28,144 | 59,305 |
| 918.45 918.50 | 28,309 28,473 | 60,717 62,136 |
| 910.30 | 20,473 | 02,130 |

APPENDIX C - MIDS MODEL





Project Information

Calculator Version: Version 4: July 2020

Project Name: Marsh Run II
User Name / Company Name: Sambatek
Date: 2/20/2023

Project Description:

Construction Permit?: No

Site Information

Retention Requirement (inches):

Site's Zip Code:

Annual Rainfall (inches):

Phosphorus EMC (mg/l):

TSS EMC (mg/l):

55305

30.4

0.3

TSS EMC (mg/l):

54.5

Total Site Area

| Land Cover | A Soils (acres) | B Soils (acres) | C Soils (acres) | D Soils (acres) | Total (acres) |
|---|--------------------|--------------------|--------------------|--------------------|------------------|
| Forest/Open Space - Undisturbed, protected forest/open space or reforested land | | | | | 0 |
| Managed Turf - disturbed, graded for yards or other turf to be mowed/managed | | | | 1.93 | 1.93 |
| | | Ir | npervious A | rea (acres) | 1.98 |
| | | | Total A | rea (acres) | 3.91 |

Site Areas Routed to BMPs

| Land Cover | A Soils (acres) | B Soils (acres) | C Soils (acres) | D Soils (acres) | Total (acres) |
|---|--------------------|--------------------|--------------------|--------------------|------------------|
| Forest/Open Space - Undisturbed, protected forest/open space or reforested land | | | | | 0 |
| Managed Turf - disturbed, graded for yards or other turf to be mowed/managed | | | | 1.73 | 1.73 |
| | | I | mpervious A | rea (acres) | 1.94 |
| | | | Total A | rea (acres) | 3.67 |

Summary Information

Performance Goal Requirement

| Performance goal volume retention requirement: | 7906 | ft3 |
|--|------|-----|
| Volume removed by BMPs towards performance goal: | 210 | ft³ |
| Percent volume removed towards performance goal | 3 | % |
| | | |

Annual Volume and Pollutant Load Reductions

| Post development annual runoff volume Annual runoff volume removed by BMPs: Percent annual runoff volume removed: | 5.3888 0.0971 | acre-ft acre-ft |
|--|------------------|--------------------|
| Percent annual runoff volume removed: | 2 | % |
| Post development annual particulate P load: | 2.4185 | lbs |
| Annual particulate P removed by BMPs: | 1.851 | lbs |
| Post development annual dissolved P load: | 1.979 | lbs |
| Annual dissolved P removed by BMPs: | 0.929 | lbs |
| Total P removed by BMPs | 2.78 | lbs |
| Percent annual total phosphorus removed: | 63 | % |
| Post development annual TSS load: | 798.8 | lbs |
| Annual TSS removed by BMPs: | 716.2 | lbs |
| Percent annual TSS removed: | 90 | % |

BMP Summary

Performance Goal Summary

| BMP Name | BMP Volume Capacity (ft3) | Volume Recieved (ft3) | Volume Retained (ft3) | Volume Outflow (ft3) | Percent Retained (%) |
|--------------------------|---------------------------------|-----------------------------|-----------------------------|----------------------------|-------------------------|
| Impervious disconnection | 210 | 399 | 210 | 189 | 53 |
| existing wetland | 0 | 7536 | 0 | 7536 | 0 |
| stormfilter + detention | 0 | 6948 | 0 | 6948 | 0 |
| jelllyfish | 0 | 399 | 0 | 399 | 0 |
| sump | 0 | 6948 | 0 | 6948 | 0 |

Annual Volume Summary

| BMP Name | Volume From Direct Watershed (acre-ft) | Volume From Upstream BMPs (acre-ft) | Volume Retained (acre-ft) | Volume outflow (acre-ft) | Percent Retained (%) |
|--------------------------|---|---|---------------------------------|--------------------------------|----------------------------|
| Impervious disconnection | 1.1172 | 0 | 0.0971 | 1.0201 | 9 |
| existing wetland | 0 | 5.0911 | 0 | 5.0911 | 0 |
| stormfilter + detention | 0 | 3.8201 | 0 | 3.8201 | 0 |
| jelllyfish | 0.2508 | 0 | 0 | 0.2508 | 0 |
| sump | 3.8201 | 0 | 0 | 3.8201 | 0 |

Particulate Phosphorus Summary

| BMP Name | Load From Direct Watershed (lbs) | Load From Upstream BMPs (lbs) | Load Retained (lbs) | Outflow Load (lbs) | Percent Retained (%) |
|--------------------------|---|--|---------------------------|--------------------------|-------------------------|
| Impervious disconnection | 0.5014 | 0 | 0.0436 | 0.4578 | 9 |
| existing wetland | 0 | 1.1931 | 0.7159 | 0.4772 | 60 |
| stormfilter + detention | 0 | 1.7145 | 1.0287 | 0.6858 | 60 |
| jelllyfish | 0.1126 | 0 | 0.0631 | 0.0495 | 56 |
| sump | 1.7145 | 0 | 0 | 1.7145 | 0 |

Dissolved Phosphorus Summary

| BMP Name | Load From Direct Watershed (lbs) | Load From Upstream BMPs (lbs) | Load Retained (lbs) | Outflow Load (lbs) | Percent Retained (%) |
|--------------------------|---|--|---------------------------|--------------------------|-------------------------|
| Impervious disconnection | 0.4102 | 0 | 0.0356 | 0.3746 | 9 |
| existing wetland | 0 | 0.9762 | 0 | 0.9762 | 0 |
| stormfilter + detention | 0 | 1.4028 | 0.8417 | 0.5611 | 60 |
| jelllyfish | 0.0921 | 0 | 0.0516 | 0.0405 | 56 |
| sump | 1.4028 | 0 | 0 | 1.4028 | 0 |

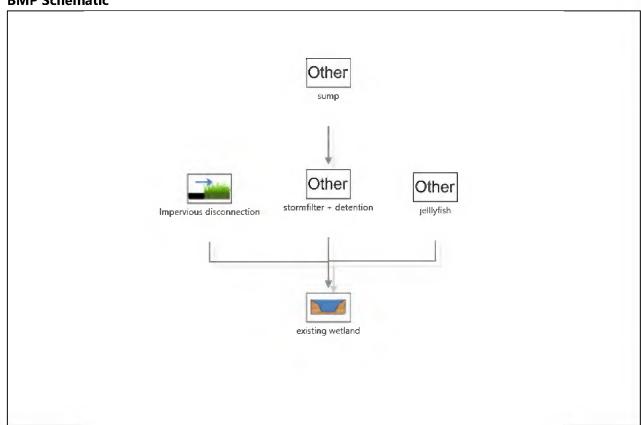
Total Phosphorus Summary

| BMP Name | Load From Direct Watershed (lbs) | Load From Upstream BMPs (lbs) | Load Retained (lbs) | Outflow Load (lbs) | Percent Retained (%) |
|--------------------------|---|--|---------------------------|--------------------------|-------------------------|
| Impervious disconnection | 0.9116 | 0 | 0.0792 | 0.8324 | 9 |
| existing wetland | 0 | 2.1693 | 0.7159 | 1.4534 | 30 |
| stormfilter + detention | 0 | 3.1173 | 1.8704 | 1.2469 | 60 |
| jelllyfish | 0.2047 | 0 | 0.1147 | 0.09 | 56 |
| sump | 3.1173 | 0 | 0 | 3.1173 | 0 |

TSS Summary

| BMP Name | Load From Direct Watershed (lbs) | Load From Upstream BMPs (lbs) | Load Retained (lbs) | Outflow Load (lbs) | Percent Retained (%) |
|--------------------------|---|--|---------------------------|--------------------------|-------------------------|
| Impervious disconnection | 165.61 | 0 | 117.22 | 48.39 | 71 |
| existing wetland | 0 | 132.28 | 79.37 | 52.909999999 | 60 |
| stormfilter + detention | 0 | 509.67 | 433.22 | 76.449999999 | 85 |
| jelllyfish | 37.18 | 0 | 29.74 | 7.44 | 80 |
| sump | 566.3 | 0 | 56.63 | 509.67 | 10 |

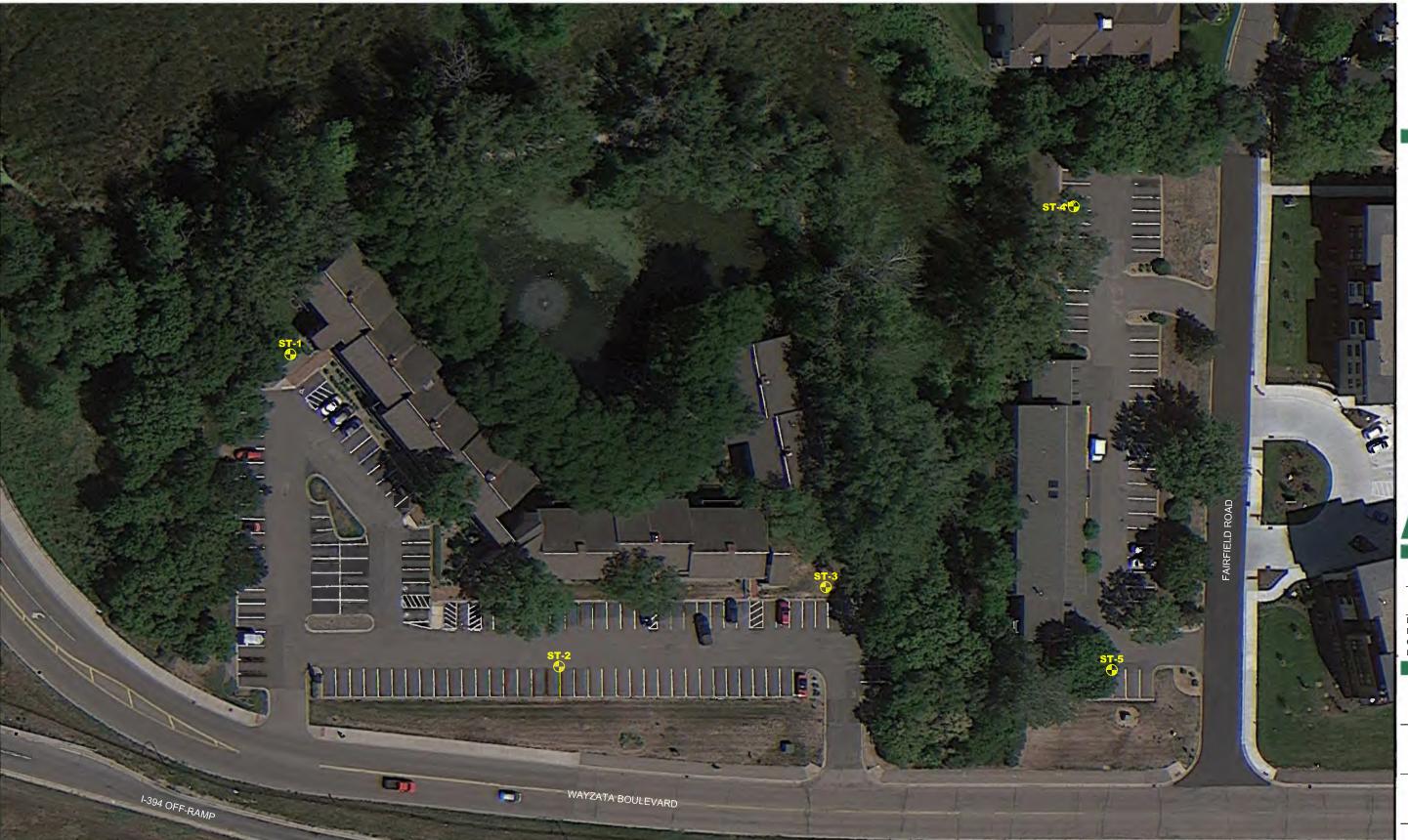
BMP Schematic



APPENDIX D - BORING LOGS







BRAUN
INTERTEC
The Science You Build On.

11001 Hampshire Avenue S Minneapolis, MN 55438 952.995.2000 braunintertec.com

Drawing Information

Project No. B1803638 01

Drawing No: B1803638-01

 Drawn By:
 JAG

 Date Drawn:
 10/12/22

 Checked By:
 JLW

 Last Modified:
 10/20/22

Project Information

Marsh Run - Phase II

Northwest Quadrant of Wayzata Boulevard and Fairfield Road W.

Minnetonka, Minnesota

Soil Boring Location Sketch

DENOTES APPROXIMATE LOCATION OF STANDARD PENETRATION TEST BORING

30' 0 60' SCALE: 1"= 60'



| Project | Number B | 180363 | R 01 | | | BORING: | : Terrinion | ogy sneet | ST-1 | abbieviations |
|--|----------------|-----------------------|---|------------------------------------|------------------|--------------------------------------|-----------------------|-------------|--------------------------------------|---------------|
| | hnical Eva | | J.U 1 | | | LOCATION: | See attac | ched sket | | |
| | Run - Phas | | | | | | | S. IOU ONOU | | |
| NW Qu | adrant of V | Vayzata | Blvd and | Fairfield Ro | W k | DATUM: N | IAD 1983 | HARN Ad | j MN Hennepin (U | S Feet) |
| Minnet | onka, Minn | esota | | | | NORTHING | : 16 | 6000 | EASTING: | 487892 |
| DRILLER: | M. Tal | kada | LOGGED BY: | R. H | luber | START DAT | E: | 10/19/22 | END DATE: | 10/19/22 |
| SURFACE ELEVATION: | 924.9 ft | RIG: 75 | 07 | METHOD: 3 1/4 | 4" HSA | SURFACIN | G: | Grass | WEATHER: | Sun |
| Elev./ Depth ft | Water Level | | scription of Ma 2488 or 2487; 1110-1-2908 | Rock-USACE E | Sample | Blows (N-Value) Recovery | q _p tsf | MC % | Tests or R | emarks |
| - 922.9 - 2.0 | mo FIL | ist | LEAN CLAY (0 | e-grained, black | el, | 3-3-5 (8) 17" 3-3-3 | | | | |
| 917.9 | | AN CLAY ((LUVIUM) | CL), gray, mois | t, medium | 5— | (6) 18" 1-2-3 (5) 17" | | | | |
| 915.9 9.0 - - - - - | /// gra | | , moist, mediui | ace Gravel, gra n to very stiff | y to | 2-3-6 (9) 18" 4-6-9 (15) | | 19 | | |
| - | | 4 | | | 15 | 17" 6-7-11 (18) 18" | | 16 | Switched to mu drilling at 15 fee | |
| - - - - - - | | | 1 | | 20 — | 5-8-11 (19) 15" | | | | |
| 4 | | | | | 25 | 6-11-15 (26) 17" | | | | |
| - 896.9 _ 28.0 _ - - - - | | | D (SC), trace (very stiff (GLA | Gravel, grayish CIAL TILL) | 30 — | 5-8-10 (18*) | | | *Low recovery | |
| | . 2.1.7. | Cor | ntinued on ne | | | | | | | |
| B1803638.01 | | | | Proup Into | rtec Corporation | | Print Date:1 | 1/01/2022 | ST-1 | page 1 of 3 |



See Descriptive Terminology sheet for explanation of abbreviations

| Project | Number E | 21202629 | R N1 | | | 36 | BORING: | remino | ogy sneet | for explanation o | abbreviations |
|---------------------------------------|-------------------------------|----------------------------------|----------------------------------|--------------------------------|-------------------------|---------|--|------------|------------|-------------------|---------------|
| | hnical Eva | | U.U I | | | | LOCATION: | See atta | ched sket | | |
| | Run - Phas | | | | | | 200, 111011. | Joo and | S.IOG GROO | | |
| | adrant of \ | | Blvd and | Fairfield | Rd W | | DATUM: N | AD 1983 | HARN Ad | j MN Hennepin (l | JS Feet) |
| Minnet | onka, Minr | nesota | | | | | NORTHING | 10 | 66000 | EASTING: | 487892 |
| DRILLER: | M. Takada LOGGED BY: R. Huber | | | | | | START DAT | E: | 10/19/22 | END DATE: | 10/19/22 |
| SURFACE ELEVATION: | 924.9 ft | RIG: 75 | 07 | METHOD: 3 | 3 1/4" HSA | | SURFACING | 3 : | Grass | WEATHER: | Sun |
| Elev./ Depth ft | Water Level | E EM | Sample | Blows (N-Value) Recovery | q _թ tsf | MC % | Tests or F | lemarks | | | |
| - 880.9 - 44.0 - 54.0 - 59.0 | SIL trace (GI | TY, CLAYEdium-grainedist, medium | ADED SAND W | edium-grainedium dense | 35— 35— 40— 40— 50— 50— | | 5-11-12 (23) 18" 10-10-17 (27) 18" 11-12-15 (27) 18" 12-15-20 (35) 18" 15-15-15 (30*) | | | *Low recovery | |
| - | | dium dense | n-grained, trace to dense (GL | ACIAL OŪTV | | X | (16) 18" | | | | |
| B1803638.01 | | Cor | ntinued on ne | | ntertec Corpora | tic | - | rint Dete | 11/01/2022 | ST-1 | page 2 of 3 |

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-1 page 2 of 3



See Descriptive Terminology sheet for explanation of abbreviations Project Number B1803638.01 BORING: ST-1 **Geotechnical Evaluation** LOCATION: See attached sketch Marsh Run - Phase II DATUM: NAD 1983 HARN Adj MN Hennepin (US Feet) NW Quadrant of Wayzata Blvd and Fairfield Rd W Minnetonka, Minnesota NORTHING: 166000 EASTING: 487892 DRILLER: M. Takada LOGGED BY: R. Huber START DATE: 10/19/22 END DATE: 10/19/22 SURFACE ELEVATION: 924.9 ft RIG: 7507 METHOD: 3 1/4" HSA SURFACING: WEATHER: Grass Sun **Description of Materials** Blows Elev./ Water Level (Soil-ASTM D2488 or 2487; Rock-USACE EM MC (N-Value) Depth Tests or Remarks 1110-1-2908) tsf % ft Recovery POORLY GRADED SAND with SILT (SP-SM), 17-17-23 fine to medium-grained, trace Gravel, gray, wet, 65; (40)medium dense to dense (GLACIAL OUTWASH) 18" 856.9 SILTY, CLAYEY SAND (SC-SM), fine to 68.0 medium-grained, trace Gravel, reddish brown, 21-24-47 moist, very dense (GLACIAL TILL) 70 (71)18" 850.9 SILTY SAND (SM), fine to medium-grained, 74.0 12-13-15 trace Gravel, brown, moist, medium dense to (28)very dense (GLACIAL TILL) 18" 16-30-20 80 Auger met refusal at 82 feet (50)843.9 12" LIMESTONE, brown, highly weathered 81.0 50/1" 842.9 *Low recovery **END OF BORING** (REF*) 82.0 Water level obscured due to mud rotary drilling. Boring immediately backfilled 85 90. 95

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-1 page 3 of 3



| Project | Number E | 31803638 | 3.01 | | | BORING: | Terrinor | ogy sneet | ST-2 | abbreviations |
|------------------------------|---|---------------------------|-------------------------------|--------------------|---------------|-----------------------|-----------------------|------------------------|------------------|---------------|
| | hnical Eva | | | | | LOCATION: | See atta | ched sket | | |
| | Run - Phas | | | | | | 1 | | | |
| | | | Blvd and | Fairfield Rd | W | | - | 7 | j MN Hennepin (U | S Feet) |
| Minnet | onka, Minr | nesota | | | | NORTHING | : 16 | 55800 | EASTING: | 488063 |
| DRILLER: | M. Ta | kada | LOGGED BY: | R. Hul | ber | START DAT | E: | 10/17/22 END DATE: 10/ | | |
| SURFACE ELEVATION: | 925.1 ft | RIG: 75 | 07 | METHOD: 3 1/4" | HSA | SURFACIN | G: | Asphalt | WEATHER: | Cloudy |
| Elev./ Depth ft | Description of Materials (Soil-ASTM D2488 or 2487; Rock-USACE EM 1110-1-2908) | | | | | | q _բ tsf | MC % | Tests or Ro | emarks |
| | | L: CLAYEY | | vith Gravel, black | A | / | | | | |
| 923.1 | | | | | -47 | 4-4-6 | 7 | | | |
| _ 2.0 _ - | | L: SANDY I wnish gray, | | CL), trace Gravel, | | (10) 15" | | | | |
| - - - | | | | | 5 | 1-2-2 (4) 16" | | | | |
| _ _ _ 916.1 | | | | - | | 2-2-2 (4) 17" | - | | | |
| _ 9.0 _ _ _ | to allo a TC | RGANIC SO PSOIL) | IL (OL), black, | moist (BURIED | 10- | 1-1-2 (3) 16" | | 44 | OC=8% | |
| 913.1 12.0 | | AN CLAY (C LUVIUM) | CL), gray, mois | t, medium to stiff | | 1-2-5 (7) 15" | | | | |
| - - - - - | | 4 | | | 15 | 2-4-6 (10) 13" | | 20 | | |
| 906.1 19.0 - - - | | | CLAY (CL), tra ACIAL TILL) | ace Gravel, gray, | 20 | 6-6-11 (17) 17" | | 31 | | |
| | | | | | 25 | 4-5-8 (13*) | | | *Low recovery | |
| - - - - - - | | - | | | 30 | 4-5-6 (11) 18" | | | | |
| | | Cor | ntinued on ne | | | | | | | |
| B1803638.01 | | | - | Descent Intente | c Corporation | | Print Date: | 14/04/2022 | ST-2 | page 1 of 2 |



See Descriptive Terminology sheet for explanation of abbreviations Project Number B1803638.01 BORING: ST-2 **Geotechnical Evaluation** LOCATION: See attached sketch Marsh Run - Phase II DATUM: NAD 1983 HARN Adj MN Hennepin (US Feet) NW Quadrant of Wayzata Blvd and Fairfield Rd W Minnetonka, Minnesota NORTHING: 165800 EASTING: 488063 DRILLER: M. Takada LOGGED BY: R. Huber START DATE: 10/17/22 END DATE: 10/17/22 SURFACE ELEVATION: 925.1 ft RIG: 7507 METHOD: 3 1/4" HSA SURFACING: Asphalt WEATHER: Cloudy **Description of Materials** Elev./ Blows Water Level (Soil-ASTM D2488 or 2487; Rock-USACE EM MC q_p tsf (N-Value) Tests or Remarks Depth 1110-1-2908) % Recovery ft SANDY LEAN CLAY (CL), trace Gravel, gray, moist, stiff (GLACIAL TILL) 891.1 SILTY SAND (SM), fine to medium-grained, 34.0 4-7-11 brown, moist, medium dense (GLACIAL TILL) (18)14" 8-10-13 ∇ (23)884.1 . 18″ Water observed at 40.0 feet 41.0 **END OF BORING** with 40.0 feet of tooling in the ground while drilling. Boring immediately backfilled Water observed at 35.0 feet at end of drilling. Water not observed to cave-in depth of 30.0 feet immediately after withdrawal of auger. 60.

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-2 page 2 of 2



| Cocottonical Evaluation Name I NW Quadrant of Waystata Blvd and Fairfield Rd W | Project | Number B | 1803638 | R 01 | | - 00 | BORING: | : Terrimon | ogy sneet | ST-3 | abbieviations |
|---|---|---|---------------------------|---------------------------------|----------------------------|------|-------------|------------|-----------|------------------|---------------|
| Marsh Run - Phase I | | | | J.U 1 | | | | See attac | ched sket | | |
| Margin M | | | | | | | | | | | |
| DRILLER: M. Taka LOGGED BY: R. Hubber START DATE 10/18/22 END DATE: 10/18/2 | NW Qu | adrant of V | Vayzata | Blvd and | Fairfield Rd | W | DATUM: N | IAD 1983 | HARN Ad | j MN Hennepin (L | JS Feet) |
| Suppraction 925.0 h Rig 7507 METHOD: 3 1/4* HSA SURFACING: Grass WEATHER: Sun Description of Materials The suppraction of Materials The | Minnete | onka, Minn | esota | | | | NORTHING | s: 16 | 35851 | EASTING: | 488234 |
| Description of Materials Description Description of Materials Descr | DRILLER: | M. Tal | ada | LOGGED BY: | R. Hul | ber | START DAT | E: | 10/18/22 | END DATE: | 10/18/22 |
| Continued on next page Continued on next p | SURFACE ELEVATION: | E 925.0 ft RIG: 7507 METHOD: 3 1/4" HSA | | | | | | G: | Grass | WEATHER: | Sun |
| 923.0 2.0 2.0 2.0 2.0 3.5-5 5 6.0 7.8-8 (16) 17 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (23) 16 7.14-9 (24) 18 7.14-9 (25) 1.1-11 (27) | Depth | Water Level | Sample | (N-Value) | q _₽ tsf | | Tests or R | emarks | | | |
| black and brown, moist 5 | | gra | ined, black, | , moist | | | | | | | |
| 5 (10) 18" 7-14-9 (23) 16" 4-7-8 (15) 10- | - 2.0 - - - | | | | oc), llace Glavel, | | 17" | | | | |
| Continued on next page Continued on next p | - - - | | | | | 5— | (10) 18" | | | | |
| 10- (15°) 1.1-11 (2°) 0" 2-2-2 (4) 18" 20- (3) 17" 27 SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) Continued on next page "Low recovery "No recovery "No recovery 23 Switched to mud rotary drilling at 15 feet 27 27 27 SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) Continued on next page | - - - | | | | 1 | | (23) 16" | | | | |
| 911.0 14.0 LEAN CLAY (CL), gray, wet, soft (ALLUVIUM) 15- 22-2-2 (4) 18" 23 Switched to mud rotary drilling at 15 feet 20- 21-2 (3) 17" 27 SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) 27 SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) Continued on next page | | | | | | 10 | | | | *Low recovery | |
| LEAN CLAY (CL), gray, wet, soft (ALLUVIUM) 15— 22-2-2 (4) 18" 23 Switched to mud rotary drilling at 15 feet 20— 21-2 (3) 17" 25— 25— 25— 27 30— 30— 30— 30— Continued on next page | - - - 911.0 | | | A | , | | (2*) | | | *No recovery | |
| 20— (3) 17" 25— (4) 18" SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) 2-3-5 (8) 18" Continued on next page | | LE/ | AN CLAY (C | CL), gray, wet, | soft (ALLUVIUM) | | (4) | | 23 | | |
| 25— (4) 18" SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) 23— 27.0 SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) 2-3-5 (8) 18" Continued on next page | - - - - - | | | 1 | | 20- | | | 27 | | |
| SANDY LEAN CLAY (CL), trace Gravel, gray, moist, soft to stiff (GLACIAL TILL) 2-3-5 (8) 18" Continued on next page | - - - - - - - - - - - - - - - - - - - | | | | | 25 | | | | | |
| 30 (8) 18" Continued on next page | 27.0 | SA mo | NDY LEAN st, soft to s | CLAY (CL), tra tiff (GLACIAL | ace Gravel, gray, TILL) | | | | | | |
| | - - - | | | | | 30 | (8) | | | | |
| | D40000000 | | Cor | ntinued on ne | | | | D: 15 : : | 4/04/2225 | 2= - | page 1 of 3 |



| Project | Number | B180363 | 8.01 | | | | BORING: | | 37 | for explanation o | |
|-----------------------|-----------------------|-----------|--|----------------|------------------|--------|---|-----------------------|------------|-------------------|---------------|
| Geotecl | hnical E | valuation | | | | | LOCATION: | See atta | ched sket | ch | |
| | Run - Ph | | Dhad and | F = ! = £! = ! | l Dal W | | DATUM: N | AD 1092 | НАВИ АА | j MN Hennepin (l | IS Foot) |
| | adrant o onka, Mil | | Blvd and | rairtield | ı Ka W | | NORTHING | - | 65851 | EASTING: | 488234 |
| | | | LOCOED DV | | Dillinhan | | - | | | | |
| DRILLER: | | Takada | LOGGED BY: | | R. Huber | | START DAT | | 10/18/22 | | 10/18/22 |
| SURFACE ELEVATION: | 925.0 f | | 507 | | 3 1/4" HSA | | SURFACING | 3 : | Grass | WEATHER: | Sun |
| Elev./ Depth ft | Water Level | | escription of Ma 2488 or 2487; 1110-1-2908 | Rock-USA | CE EM | Sample | Blows (N-Value) Recovery | q _բ tsf | MC % | Tests or F | Remarks |
| 871.0 | | POORLY GR | ADED SAND (S Gravel, gray, w | TILL) | 40- | | 4-4-7 (11) 18" 4-7-8 (15) 15" 4-6-8 (14) 18" 5-5-9 (14) 17" 6-3-3 (6*) 0" | | | *No recovery | |
| B1803638.01 | | Co | ntinued on ne | ext page | n Intertec Corpo | | | | 11/01/2022 | ST-3 | B page 2 of 3 |



See Descriptive Terminology sheet for explanation of abbreviations

| Project | Number B1803638.01 | BORING: ST-3 |
|--|---|--|
| Geotec | nnical Evaluation | LOCATION: See attached sketch |
| 1 | Run - Phase II | |
| 1 | adrant of Wayzata Blvd and Fairfield Rd W | DATUM: NAD 1983 HARN Adj MN Hennepin (US Feet) |
| Minneto | onka, Minnesota | NORTHING: 165851 EASTING: 488234 |
| DRILLER: | M. Takada LOGGED BY: R. Huber | START DATE: 10/18/22 END DATE: 10/18/22 |
| SURFACE ELEVATION: | 925.0 ft RIG: 7507 METHOD: 3 1/4" HSA | SURFACING: Grass WEATHER: Sun |
| Elev./ Depth ft | Description of Materials ਭ ਲ (Soil-ASTM D2488 or 2487; Rock-USACE EM 1110-1-2908) | Blows (N-Value) Recovery qp MC tsf MC % |
| | POORLY GRADED SAND (SP), fine to coarsegrained, with Gravel, gray, wet, loose 65—(GLACIAL OUTWASH) | 9-4-5 (9) 18" |
| 69.0 - 69.0 | SILTY SAND (SM), fine to medium-grained, with Gravel, gray, wet, medium dense 70— (GLACIAL TILL) | 7-10-15 (25) 18" |
| - 852.0 - 73.0 | SILTY, CLAYEY SAND (SC-SM), fine to medium-grained, with Gravel, reddish brown, moist, very dense (GLACIAL TILL) 75 | 11-30-46 (76) 17" |
| 846.0 79.0 - - - - - - - - - - - - - - - - - - - | SILTY SAND (SM), fine to medium-grained, with Gravel, brown, moist, dense (GLACIAL 80 — TILL) LIMESTONE, brown, highly weathered END OF BORING | 15-22-19 (41) 18" 25-50/1" (REF*) *Low recovery Water level obscured due |
| - 82.5 | Boring immediately backfilled 85— 90— | to mud rotary drilling. |
| | 95— | |

page 3 of 3 B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-3



| Project | Number E | 3180363 | 8.01 | | | BORING: | | .ogy | ST-4 | |
|---|----------------|-----------------------|---|-----------------|--------------------|--------------------------------|-----------------------|------------|------------------|---------------|
| | hnical Eva | | | | | LOCATION | l: See atta | ched sket | | |
| Marsh | Run - Pha | se II | | | | | 1 | | | |
| | | | Blvd and | Fairfield | Rd W | DATUM: 1 | | - | j MN Hennepin (l | JS Feet) |
| Minnet | onka, Mini | nesota | Q | | | NORTHING | G: 1 | 66094 | EASTING: | 488393 |
| DRILLER: | | | | | | | TE: | 10/17/22 | END DATE: | 10/17/22 |
| SURFACE ELEVATION: | 920.7 ft | RIG: 7 | 507 | METHOD: 3 | 1/4" HSA | SURFACIN | IG: | Asphalt | WEATHER: | Cloudy |
| Elev./ Depth ft | Water Level | | escription of Ma 12488 or 2487; 1110-1-2908 | Rock-USACE | Sample | Blows (N-Value) Recovery | q _₽ tsf | MC % | Tests or F | Remarks |
| - - 918.7 - 2.0 | mo FII | oist L: SANDY | Y SAND (SC), I LEAN CLAY (0 | | -4 | 2-3-4 (7) | 1 | | | |
| — 916.7 | bla | ck, moist | | | $\neg \triangle$ | 15" | | | | |
| _ 4.0 _ - _ | to site of TC | RGANIC SO PSOIL) | OIL (OL), black, | moist (BURI | ED 5 | 2-3-3 (6) 12" | | | | |
| 913.7 7.0 | LE | AN CLAY (| CL), gray, wet, | soft (ALLUVI | UM) | 1-1-1 (2) 16" | 1 | 40 | LL=37, PL=16, | , PI=21 |
| - - - - | | | | | 10 | 1-1-2 (3) 18" | | 32 | | |
| _ _ _ 906.7 | | | A | | | 1-1-2 (3) 18" | | 37 | LL=41, PL=19, | PI=22 |
| _ 14.0 _ - - - - - - | | | Ñ CLAY (CL), w n to stiff (GLAC | | 15— | 2-4-4 (8) 18" | | | | |
| | | | | | 20 | 2-4-5 (9) 18" | | 18 | | |
| | • | | | | 25 | 7 1-4-6 (10) 3 17" | | | | |
| | | AYEY SAN f (GLACIA | ID (SC), trace (L TILL) | Gravel, gray, ı | moist, 30 | , 2-4-5 (9) 18" | | | | |
| 888.7 32.0 | ! Z:V: A | Co | ntinued on ne | ext page | | | | | | |
| B1803638.01 | | | | | ntertec Corporatio | n | Drint Date: | 11/01/2022 | ST- | 1 page 1 of 2 |



See Descriptive Terminology sheet for explanation of abbreviations Project Number B1803638.01 BORING: ST-4 **Geotechnical Evaluation** LOCATION: See attached sketch Marsh Run - Phase II DATUM: NAD 1983 HARN Adj MN Hennepin (US Feet) NW Quadrant of Wayzata Blvd and Fairfield Rd W Minnetonka, Minnesota NORTHING: 166094 EASTING: 488393 DRILLER: M. Takada LOGGED BY: START DATE: END DATE: R. Huber 10/17/22 10/17/22 SURFACE ELEVATION: 920.7 ft RIG: 7507 METHOD: 3 1/4" HSA SURFACING: **Asphalt** WEATHER: Cloudy **Description of Materials** Elev./ Blows Water Level (Soil-ASTM D2488 or 2487; Rock-USACE EM MC q_p tsf Depth (N-Value) Tests or Remarks 1110-1-2908) % ft Recovery SANDY LEAN CLAY (CL), trace Gravel, gray, moist, very stiff (GLACIAL TILL) 5-7-9 (16)18" 4-7-10 (17)879.7 . 18″ Water observed at 25.0 feet 41.0 **END OF BORING** at end of drilling. Boring immediately backfilled 50 55 60-

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-4 page 2 of 2



See Descriptive Terminology sheet for explanation of abbreviations

| Project | Number | B180363 | 8.01 | | | 00 | BORING: | Termino | ogy sneet | ST-5 | I ADDIEVIALIONS |
|-------------------------------------|------------------|------------------------------|--------------------------------------|-----------------------|------------------|------------|----------------------|-------------------------------|------------|------------------|-----------------|
| | hnical Ev | | | | | | LOCATION: | See atta | ched sket | | |
| | Run - Pha | | | | | | | 1 | | | |
| NW Qu | adrant of | Wayzata | Blvd and | Fairfield | Rd W | | DATUM: N | AD 1983 | HARN Ad | j MN Hennepin (l | JS Feet) |
| Minnet | onka, Min | nesota | | | | | NORTHING | 10 | 55798 | EASTING: | 488417 |
| DRILLER: | M. T | akada | LOGGED BY: | | R. Huber | | START DAT | RT DATE: 10/17/22 END DATE: 1 | | | 10/17/22 |
| SURFACE ELEVATION: | 922.5 ft | RIG: 75 | 07 | METHOD: 3 | 3 1/4" HSA | | SURFACING | G: | Asphalt | WEATHER: | Cloudy |
| Elev./ Depth ft | Water Level | Sample | Blows (N-Value) Recovery | q _p tsf | MC % | Tests or F | Remarks | | | | |
| 920.5 | | | LAYEY SAND h brown, moist | | ace | | | - | | | |
| 2.0 - 918.5 | | LL: SANDY ack, moist | LEAN CLAY (0 | CL), gray and | | X | 4-5-5 (10) 17" | | | | |
| _ 4.0 _ _ _ | FI | LL: ORGAN | IC SOIL (OL), | black, moist | 5— | | 3-3-4 (7) 16" | | | | |
| 915.5 | | LL: CLAYEY ay, moist | SAND (SC), t | prown and da | ark | X | 2-1-1 (2) 14" | 1 | P | | |
| 913.5 _ 9.0 _ - | LE | EAN CLAY (0 oft to medium | CL), with Silt le n (ALLUVIUM) | nses, gray, v | wet, | | 4-3-1 (4) 18" | | | | |
| - - - - | | | A | | K | X | 1-1-4 (5) 18" | | | | |
| - - - - - 904.5 | | 4 | | 4 | 15 | X | 1-1-1 (2) 18" | | 32 | LL=33, PL=20, | PI=13 |
| 904.5 _ 18.0 _ - - - | S _i m | ANDY LEAN oist, medium | CLAY (CL), transition to stiff (GLAC | ace Gravel, (| gray, | X | 2-2-4 (6) 18" | | | | |
| 4 | | | 1 | | _ _ _ | | 2-3-5 | | | | |
| | | | | | 25 — — | X | (8) 18" | | | | |
| | | | | | 30 — | X | 3-4-9 (13) 16" | | | | |
| Ē_ | 1/// | Coi | ntinued on ne | xt page | | | | | | | |
| B1803638.01 | | | | | Intertec Corpora | tion | | Print Date: | 11/01/2022 | ST-5 | page 1 of 2 |

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-5 page 1 of 2



See Descriptive Terminology sheet for explanation of abbreviations Project Number B1803638.01 BORING: ST-5 **Geotechnical Evaluation** LOCATION: See attached sketch Marsh Run - Phase II DATUM: NAD 1983 HARN Adj MN Hennepin (US Feet) NW Quadrant of Wayzata Blvd and Fairfield Rd W Minnetonka, Minnesota NORTHING: 165798 EASTING: 488417 DRILLER: M. Takada LOGGED BY: END DATE: R. Huber START DATE: 10/17/22 10/17/22 SURFACE ELEVATION: 922.5 ft RIG: 7507 METHOD: 3 1/4" HSA SURFACING: **Asphalt** WEATHER: Cloudy **Description of Materials** Elev./ Blows Water Level (Soil-ASTM D2488 or 2487; Rock-USACE EM MC Depth (N-Value) Tests or Remarks 1110-1-2908) tsf % ft Recovery SANDY LEAN CLAY (CL), trace Gravel, gray, 889.5 moist, medium to stiff (GLACIAL TILL) 33.0 SANDY LEAN CLAY (CL), trace Gravel, with Sand seams, gray, moist, stiff to very stiff 4-5-5 (GLACIAL TILL) (10)18" 8-17-10 *Low recovery (27*)881.5 Water observed at 12.5 feet 41.0 **END OF BORING** while drilling. Boring immediately backfilled 50 55 60-

B1803638.01 Braun Intertec Corporation Print Date:11/01/2022 ST-5 page 2 of 2



Schedule of Events

City of Minnetonka Hennepin County, Minnesota

For the proposed Modification to the Development Program for Development District No. 1 & the proposed establishment of Marsh Run II Tax Increment Financing District (a redevelopment district)

Draft as of February 16, 2023

March 20, 2023 Letter received by County Commissioner giving notice of potential

redevelopment TIF district (at least 30 days prior to publication of public

hearing notice). [Ehlers will distribute.]

March 24, 2023 Project information, property identification numbers, fiscal impacts and maps

sent to Ehlers for drafting documentation.

Ehlers confirms whether building permits have been issued on the property to

be included in the TIF District.

Ehlers conducts internal review of Plans. By March 29, 2023

March 31, 2023 Fiscal/economic implications received by School Board Clerk and County

> Auditor (at least 30 days prior to public hearing) and County receives information for review of county road impacts. [Ehlers will distribute.]

*The County Board, by law, has 45 days to review the TIF Plan to determine if any county roads will be impacted by the development. Because City staff believes that the proposed TIF district will not require unplanned county road improvements, the TIF Plan was not forwarded to the County Board 45 days prior to the public hearing. Please be aware the County Board could claim that tax increment should be used for county roads, even after the public hearing.

April 20, 2023 Publication of hearing notice and map in the Minnetonka Deephaven Excelsion

> Shorewood Chanhassen Tonka Bay Eden Prairie Sun Sailor (at least 10 days but not more than 30 days prior to hearing). [Ehlers will submit notice, map

and instructions. Publication deadline: April 12, 2023.]

April 27, 2023 EDAC meets at 6:00 PM to considers the Plans, resolution adopting the Plans

in connection with the TIF District. [Attorney provides resolution by April 19,

2023.]

May 1, 2023 City Council holds public hearing at 6:30 PM on the modification to the

Development Program for Development District No. 1 and the proposed

Establishment of Marsh Run II Tax Increment Financing District and considers









a resolution approving the Plans. [Ehlers and attorney provide packet information April 24, 2023.]

EDA considers a resolution approving the modification to the Development Program for Development District No. 1 and the proposed Establishment of Marsh Run II Tax Increment Financing District.

EDA considers an Interfund Loan resolution in connection with the TIF District.

May 2, 2023 City may issue building permits.

Before June 30, 2023 Ehlers files the Plans with the MN Department of Revenue, Office of the State

Auditor, and requests certification of the TIF District with the County.

An action under subdivision 1, paragraph (a), contesting the validity of a determination by an authority under section 469.175, subdivision 3, must be commenced within the later of:

(1) 180 days after the municipality's approval under section 469.175, subdivision 3; or

(2) 90 days after the request for certification of the district is filed with the county auditor under section 469.177, subdivision 1.

